

CALIFORNIA INSTITUTE OF TECHNOLOGY

EARTHQUAKE ENGINEERING RESEARCH LABORATORY

STRONG MOTION EARTHQUAKE ACCELEROGRAMS

DIGITIZED AND PLOTTED DATA

VOLUME II - CORRECTED ACCELEROGRAMS AND INTEGRATED
GROUND VELOCITY AND DISPLACEMENT CURVES

PART A - ACCCELEROGRAMS IIA001 THROUGH IIA020

EERL 71-50

A REPORT ON RESEARCH CONDUCTED UNDER A
GRANT FROM THE NATIONAL SCIENCE FOUNDATION

PASADENA, CALIFORNIA

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PREFACE TO THE SERIES

In 1969 the first volume of a series appeared which presented "uncorrected" digitized and plotted strong-motion earthquake accelerograph data. Since that time several additional volumes of such uncorrected data have been issued, and the whole project of supplying such basic information for all recorded earthquakes is well along towards completion.

The San Fernando earthquake of February 9, 1971 gave an added significance to the project by supplying a very large number of important accelerograms, which in effect multiplied the total amount of available data on past earthquakes by about three. Because of the special importance of these San Fernando records for current studies in earthquake engineering, they are being given top priority in the scheduling of the data processing.

The idea behind the issuance of the so-called "uncorrected" data was to place in the hands of all investigators the basic data in the form corresponding as nearly as possible to the information contained on the original film records. It was recognized that for various purposes different investigators would want to treat these basic data in different ways, and that there would be several points of view with respect to the types of "corrections" appropriate.

The purpose of the second volume is to present integrated ground velocity and displacement curves in as accurate a form and over as wide a frequency range as is compatible with the original data. In addition, the modified data is believed to be the most accurate form of the input data for structural response calculations, and for response spectrum determinations, that is feasible to produce from the original record.

The basic corrections of the original data fall into two main classes. The first accounts for long-period distortions which are usually referred to as a "baseline" correction. These adjustments are necessary in order that the double-integrated displacement curves preserve a meaningful form. The second class involves high-frequency corrections to account for the fall-off of basic transducer response in the accelerograph. These corrections will be required if the high-frequency portion of the response or a spectrum is of importance for particular applications. The whole process has also involved a detailed study of the accuracies involved in digitizing the various forms of the original paper and film records, so that the final result is compatible with all limitations and potentialities of the whole instrumentation system. The theory and details of these corrections have been discussed in a series of reports referred to in the body of this report.

The present report initiates the second phase of a data processing project which has been made possible by the long range support of the National Science Foundation. The cooperative efforts of many people are necessary for such undertaking, and we have been unusually fortunate in the quality and devotion of many persons who have played a significant role in the success of the venture. More specific acknowledgments will be found in the separate sections and in the detailed reports. The continued support received from the Earthquake Research Affiliates program of the California Institute of Technology is also much appreciated.

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INTRODUCTION TO VOLUME II

A transducer measuring relative response of a single-degree-of-freedom oscillator, with 60 to 70 percent critical damping, is normally used to record ground acceleration. For older instruments the natural frequency of such a transducer is close to 10 cps and it approaches 30 cps for more modern accelerographs (Trifunac and Hudson, 1970). The direct output of an accelerograph thus accurately approximates absolute acceleration of the instrument base in a frequency range from 0 cps to about 5 to 15 cps. Since the output of most accelerograph transducers comes in analog form, the analog records must be digitized before they can be used for further analysis.

Digitization of strong-motion accelerograms can be semiautomatic, or automatic. Semiautomatic digitization, frequently referred to as "optical-mechanical digitization," is, at the present time, still the most widely used system in earthquake engineering and strong-motion seismology studies. It involves a mechanical cross-hair which is manually set on the point to be digitized, and an analog to digital conversion system, which transforms the analog position coordinates of the cross-hair into a digital output. Automatic digitization involves either, firstly, digitizing a transparent analog record by a flying spot scanner, a cathode ray tube, or equivalent or, secondly, a direct electronic analog to digital conversion of an analog signal from a magnetic tape. An automatic digitization process using newly developed high precision cathode ray tubes has great potential value for future accelerogram processing.

The exact absolute acceleration of the instrument support undergoes two major alterations before it is available in the form of a so-called "uncorrected accelerogram" (Figure 1). The first alteration takes place in the accelerograph transducer, where the exact acceleration is converted to an analog record of instrument response $R(t)$, while the second alteration takes place during the digitization of the instrument response. The effect of each conversion is to modify the frequency content of an input. To show the nature of these changes, let us assume that an input acceleration has a constant Fourier amplitude spectrum in the frequency band from 0 cps to f_i cps, with $f_i \gg f_n$; where f_n is the natural frequency of an ideal accelerograph transducer represented by a viscously damped, single-degree-of-freedom oscillator. In Figure 1 the $F\{\cdot\}$ indicates the Fourier amplitude spectrum functional. The effect of the above-mentioned modifications on the Fourier amplitude spectrum of the exact input acceleration is shown in Figure 1. Transfer function properties of both an acceleration transducer and the digitization process are basically equivalent to a low-pass filter.

Modern applications of structural vibration theory to design earthquake-resistant structures and research in strong-motion seismology require accurate acceleration data over a wide frequency band. It thus becomes necessary to perform several corrections of the "uncorrected accelerograms." Before these corrections can be performed, it is necessary to study in detail the properties of each processing step and the errors associated with it. A detailed account of long period errors and baseline corrections of strong-motion accelerograms (Trifunac, 1970) and a study of the high frequency errors and instrument corrections

MODIFICATION OF EXACT ABSOLUTE ACCELERATION THROUGH RECORDING AND DIGITIZATION

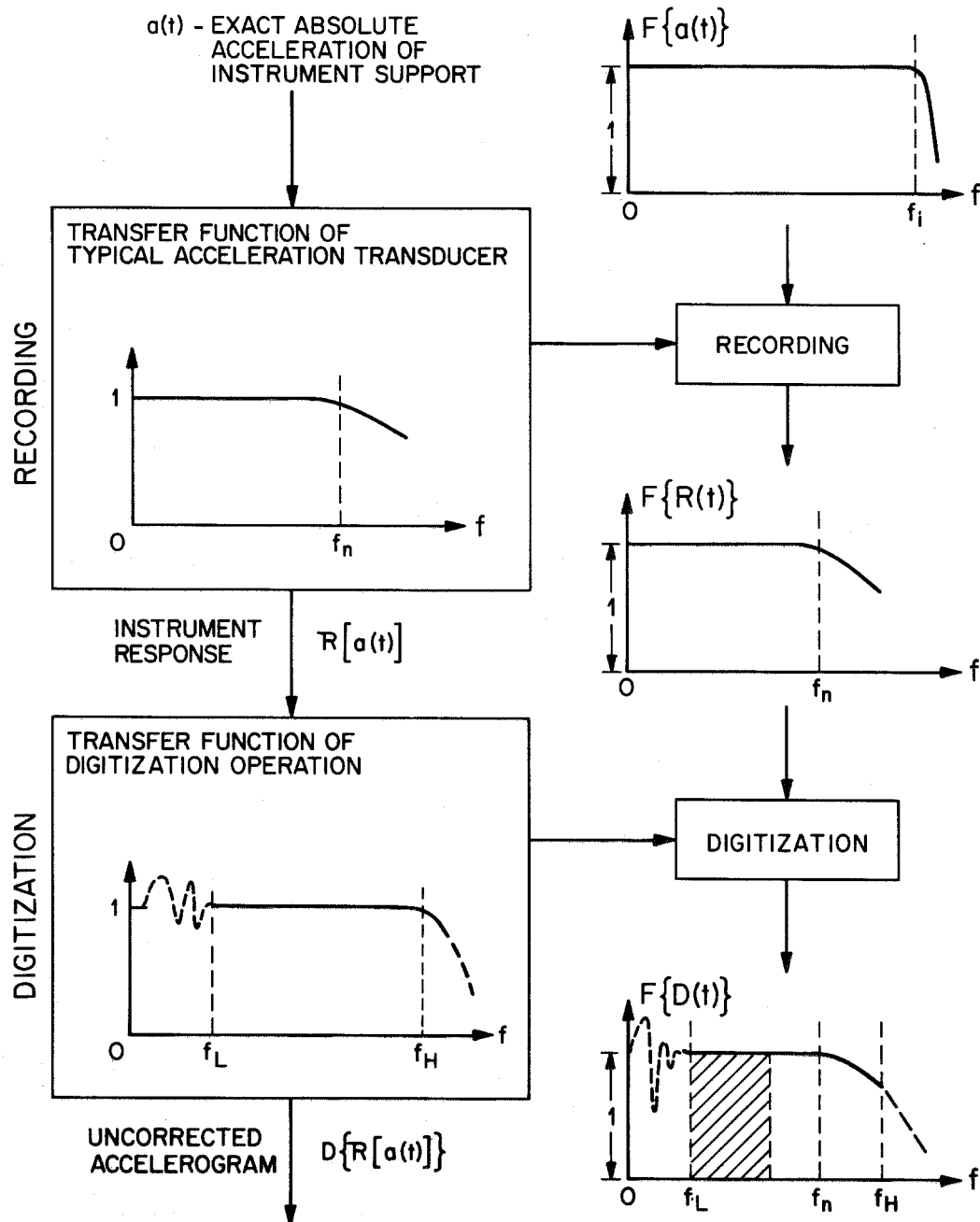


Fig. 1

(Trifunac et al., 1971) may be found in previous reports. Briefly summarized here are some of the main results from these reports which are of immediate importance for standard processing of uncorrected accelerograms.

Uncorrected Accelerograms

Original accelerograms recorded on photographic paper and more recently on 70 mm and 35 mm film are kept in the Washington office of the National Oceanic and Atmospheric Administration (formerly U.S. Coast and Geodetic Survey). From the original records, full-size contact film negatives are prepared by the staff of the Seismological Field Survey (NOAA) in San Francisco. Using these negatives, contact prints are made on translucent, Mylar-based film, which is mechanically strong, dimensionally stable and gives excellent optical contrast for automatic digitization or for accurate setting of the cross-hair during semi-automatic hand digitization.

Digitization of translucent film copies of paper records is performed on a Benson-Lehner 099D data reducer. 312 digital counts per centimeter is the maximum resolution of this unit, while its table length of 60 cm can accommodate about 30 seconds of record, at the usual recording speeds. Acceleration records are digitized with unequally spaced data points in time with an average of from 10 to 40 points per second. The density of digitization depends on the frequency content of the record (Trifunac et al., 1971).

Most records have "fixed traces" recorded by a light beam reflected from fixed mirrors attached to the accelerograph frame.

These fixed traces often depart from a straight line because of paper distortion and transverse motions in the paper drive mechanism. By digitizing the fixed traces at intervals of about two points per second, or more, the long period errors that are introduced into the digitized accelerogram are, for the most part, eliminated. Digitized data of fixed traces are first smoothed by a running average scheme using coefficients slightly different from the usual $\frac{1}{4}$, $\frac{1}{2}$, $\frac{1}{4}$ for equi-spaced data, by altering the weighting values according to the distance of the point from the mid-point. The smoothed fixed trace is then subtracted from the accelerogram trace. Time marks are also digitized and smoothed by $\frac{1}{4}$, $\frac{1}{2}$, $\frac{1}{4}$ to form basic time coordinates.

As a final step in processing the "uncorrected data," the zero axis is translated to make the integral of the digitized acceleration curve zero. This is physically equivalent to making the change in ground velocity, from the beginning to the end of a record, equal to zero. This assumption is not exactly correct, because the true beginning and end of the earthquake are not indicated on the accelerogram. This procedure results in a simple and reproducible method of accurately defining a zero line.

The above described digitization and processing techniques do not in any way distort the original accelerogram in the frequency domain of interest.

Recording and Digitizing Errors at Long and Short Periods

Recording and digitizing errors, present in uncorrected accelerograms, are associated with the frequencies f_L and f_H as shown in Figure 1. Once these frequencies are known, the uncorrected accelerograms can be corrected to represent accurately ground acceleration in the frequency domain between f_L and f_H . Ideally the frequency f_L should be greater than all frequencies associated with long period recording and digitizing errors, whose spectral amplitudes and phases cannot be corrected, while the frequency f_H should be smaller than all frequencies representing high frequency recording and digitizing errors. These frequencies change from one instrument to another and depend on the instrument recording speed and sensitivity (Trifunac, 1970). For the standard accelerogram correction, f_L and f_H are chosen to represent the average for all records.

The principal sources of long period errors can be divided into several groups:

- L1. Errors caused by the transverse play of the recording paper or film in the drive mechanism.
- L2. Errors due to the warping of records, caused by aging, and errors introduced by photographic processing of contact negatives and Mylar translucent copies.
- L3. Errors caused by optical enlargement of 70 mm and 35 mm film negatives.

- L4. Systematic errors due to imperfect mechanical traverse mechanisms of the cross-hair system on the digitizing table.
- L5. Random errors generated during the digitization process.

The main sources of high frequency errors are:

- H1. Modification of harmonic amplitudes and shift of phases caused by the finite, natural frequency ω_0 of the accelerograph transducer.
- H2. Errors resulting from the imperfections in transducer design.
- H3. Random digitization errors.
- H4. Errors caused by inadequate resolution of digitizing equipment.
- H5. Low-pass filtering effects in the optical-mechanical digitization process.

The above errors will not be discussed in detail, but the most prominent ones influencing the choice of f_L and f_H in standard accelerogram processing will be pointed out. The analysis of the above errors, their relative significance and methods of correcting them are outlined in previous reports (Hudson et al., 1969; Trifunac, 1970; Trifunac et al., 1971).

From the point of view of accelerogram correction, the above errors fall into three groups. The first group consists of L1, L2 and L4 and is a set of well defined errors. All information necessary to correct them is available during the digitization process. Corrections for the transverse play of recording paper or film, warping of records and systematic errors in the mechanical system of the digitizer table can all be performed during processing of "uncorrected accelerograms."

The second group of errors is represented by H1 and H2. These are more difficult to correct exactly because they require extensive computational procedures not suitable for routine data processing. Errors resulting from excitation of higher modes are, for example, neglected in our standard processing. These errors restrict the frequency f_H which must be chosen to be smaller than the frequency of the second transducer mode.

The final group, represented by L5, H3, H4 and H5, is the most complex. This group has the strongest influence on the choice of the f_L and f_H frequencies. Typically, the nature of these errors is such that they cannot be corrected, but have to be eliminated from the uncorrected accelerograms.

Long period acceleration waves have amplitudes which decrease as ω^2 when $\omega \rightarrow 0$, and may become smaller than long period digitization noise. Several tests were performed (Trifunac, 1970) to find the longest periods, equal to $\frac{1}{f_L}$, for which ground motion can be accurately retrieved from digitized accelerograms. One of the tests consisted of finding the Fourier amplitude spectrum of long period digitization noise. In another test ground displacement curves, as measured by

an accurate laboratory displacement meter, were compared with displacement curves calculated, by double integration from an accelerograph record. From these tests it was concluded (Trifunac, 1970) that, for a typical accelerogram, the average of the longest periods that can be reproduced accurately is about 16 seconds. This corresponds to $f_L = 0.06$ cps. Typical average errors in the Fourier amplitudes of ground displacements at this frequency are of the order of several millimeters.

The choice of $f_L = 0.06$ cps is a delicate problem. It depends on the expected use of an accelerogram, and in particular, on the required accuracy of the computed ground motion. If long period ground displacements of several meters were expected, errors of several centimeters would certainly be acceptable in computed ground displacements, and it would be possible to extend the validity of the twice-integrated accelerograms to perhaps 30 or even 50 seconds. For the present processing of the corrected accelerograms, a cut-off period of 16 seconds was selected. Whenever longer period motions are required one can always go back to the original uncorrected accelerogram data and, if possible, extend the information beyond 16 seconds according to the needs of that particular study.

Analysis of high-frequency digitization errors (Trifunac et al., 1971) shows that the highest frequency resolved by optical mechanical digitization, in a short segment of digitized record, is substantially above the frequency 25 cps. Fundamental frequencies of most instruments fall between 10 and 30 cps and recorded signals with frequencies higher than 30 cps would either have a very low signal-to-noise ratio, be distorted

by higher modes of vibration of the instrument transducer, or both. From this it was concluded (Trifunac et al., 1971) that $f_H = 25$ cps is the highest frequency that can be extracted with accuracy from hand-digitized paper records. This high frequency limit is, of course, the consequence of presently available and practical means of hand-digitization and processing of paper records. With future improvements in instrument design and technology of data processing, this frequency will no doubt be further increased.

Instrument Correction

To accurately recover frequencies from about $\frac{1}{2}f_n$ up to f_H (Figure 1), a correction for the transducer response is performed.

For standard correction of "uncorrected accelerograms" (Trifunac et al., 1971), the differential equation describing the behaviour of the viscously damped, single-degree-of-freedom oscillator is used,

$$\ddot{x} + 2\omega_o \zeta_o \dot{x} + \omega_o^2 x = -a(t). \quad (1)$$

In this equation

- x = relative motion of the transducer mass
- ω_o = natural frequency of the transducer ($\omega_o = 2\pi f_o$)
- ζ_o = fraction of critical damping
- $a(t)$ = absolute ground acceleration

For an accelerometer, ω_o is a large number (normally about 100 and larger), so that the term $\omega_o^2 x$ dominates the left-hand side of Equation (1). Therefore the terms \ddot{x} and $2\omega_o \zeta_o \dot{x}$ are frequently neglected. This approximation is adequate as long as recorded frequencies are significantly smaller than ω_o , and in that case ground acceleration $a(t)$ is approximately

given by

$$a(t) \approx -\omega_0^2 x. \quad (2)$$

In order to extend information about ground acceleration to higher frequencies, all terms on the left-hand side of Equation (1) have to be considered, requiring differentiation of the recorded instrument response x . As is well known, this may lead to serious difficulties because such a process would amplify high-frequency digitization errors. In a recent study (Trifunac et al., 1971) it was demonstrated that such difficulties may be avoided if digitization errors are filtered out prior to the differentiation process. This is, of course, based on the assumption that high-frequency digitization errors are well above recorded high-frequency components of ground motion, or if not, that the filtering of some of the real high-frequency components of ground motion does not seriously affect the quality of the digital data.

Baseline Correction

Baseline correction of uncorrected accelerograms is performed in such a way that most real signals are preserved, while long period noise, introduced into uncorrected accelerograms by digitization is eliminated. It would be easy to achieve separation of long-period digitization errors, if they were contained in a well defined frequency band. Although sharp boundaries cannot be unequivocally determined, analysis of long period errors (Trifunac, 1970) shows that for periods longer than about 16 seconds digitization noise may give excessively large displacement amplitudes. In the decision process of determining this cut-off period, the preference is to filter out some possibly realistic seismic signals, rather than

contaminate baseline corrected data with processing errors.

The standard procedure for baseline correction is summarized in the flow chart in Figure 2. A more detailed description of the processing steps may be found in the previous report (Trifunac, 1970).

To eliminate distortions caused by photographic enlargement of film negatives, a straight zero acceleration baseline is least square fitted to the uncorrected accelerogram $a(t)$, and the result is $a^0(t)$ (Figure 2). In step 2, the ground velocity $v(t)$ is first calculated assuming $v(0) = 0$. A straight zero velocity baseline is next least square fitted to the velocity $v(t)$ to get $v^0(t)$ (Figure 2). This fitting is designed to estimate the initial velocity v_0 and remove the linear trend a_0 . This trend a_0 is caused by an unknown mean value of ground acceleration which has been, up to this point, assumed to be zero. After the mean of acceleration $a^0(t)$ is changed by adding a constant a_0 , acceleration $a^1(t)$ is high-pass filtered by using an Ormsby filter which has the cut-off frequency $f_c = 0.07$ cps and the roll-off termination frequency $f_T = 0.05$ cps.

Because long periods have been filtered out, the constants v_0 and a_0 as calculated from an uncorrected accelerogram are slightly changed. To correct for this small change, the high-pass filtered accelerogram is processed again through steps 2 and 3, now designated 5 and 6.

The accelerogram to be baseline corrected is specified in the time interval from 0 to T and is undefined outside of that interval. It may be assumed that an instrument is triggered by one of the first arrivals of earthquake waves so that only a short portion of the accelerogram is lost. Prior to any arrival of seismic waves and long after an earthquake, there is no motion and the accelerogram is zero. For high-pass filtering with an Ormsby filter it is necessary to extend the accelerogram $T_w / 2$

FLOW CHART FOR BASELINE CORRECTION

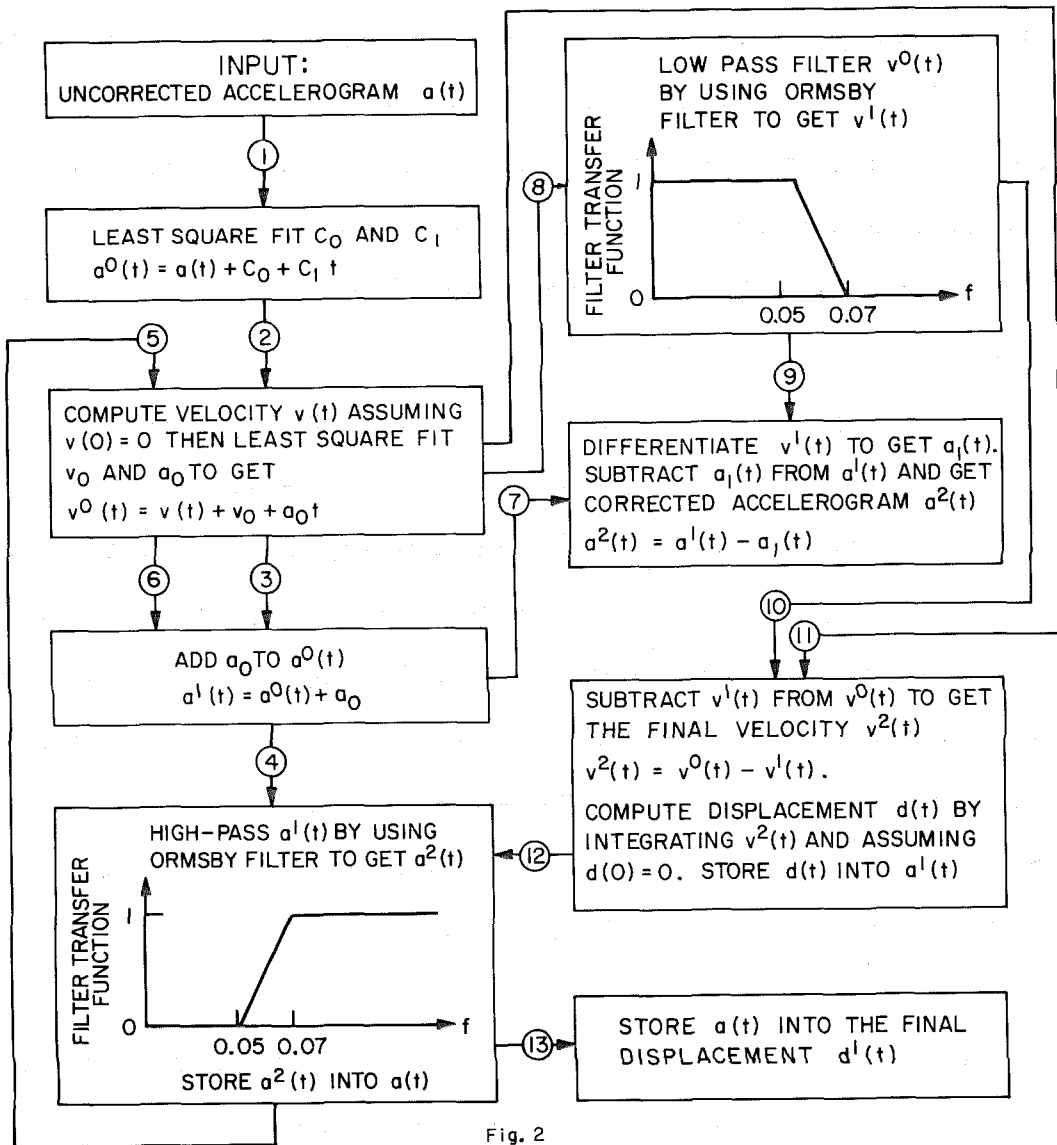


Fig. 2

time units to the left of 0 and $T_{\omega}/2$ to the right of T if the window over which the filtering is performed is designated by T_{ω} . In previous work (Trifunac, 1970) the accelerogram was extended by assuming that it is zero outside the time interval 0 to T . The position of this zero relative to the accelerogram was fixed by steps 1, 2 and 3. The accuracy of this zero position influences the accuracy of long period components in a high-pass filtered accelerogram near the beginning and near the end of the record. For a typical accelerogram, these effects are smaller than the least significant figure in uncorrected accelerogram data which is 0.1 cm/sec.^2

Recent experiments have shown that the small uncertainties in extending an accelerogram by zero outside the interval 0 to T , based on the fitted straight line $C_0 + C_1 t$ (step 1 in Figure 2), and the uncertainties resulting from small errors in estimating v_0 and a_0 (step 2 in Figure 2), may lead to small, but undesirable, long period components in the computed ground displacement, which are entirely the result of data processing procedures. These uncertainties are a consequence of the choice of a fitting criterion, the least square method, which is, from the point of view of the physical nature of accelerograms, only a mathematical fiction.

If these small errors resulting from the non physical estimation process of the constants C_0 and C_1 are designated by ΔC_0 and ΔC_1 , the error added to an accelerogram $a^0(t)$ during operation 1 (Figure 2) of the standard baseline correction can be represented by a function $f(t)$ given by

$$f(t) = \begin{cases} 0 & ; t < 0 \\ \Delta C_0 + \Delta C_1 t & ; 0 < t < T \\ 0 & ; t > T \end{cases}$$

Since $f(t)$ has a jump at $t = 0$ and $t = T$, it introduces small but undesirable effects in the integrated velocity and displacement curves, predominantly near the beginning and the end of a record. In order to eliminate these effects, a new refinement has been added to the standard baseline correction procedures (Trifunac, 1970), which consists of extending the accelerogram $a(t)$ as an even function outside the interval 0 to T , as follows

$$\begin{aligned} a(-\tau) &= a(\tau) ; -T < \tau < 0 \\ a(T + \tau) &= a(T - \tau) ; T < \tau < 2T \end{aligned}$$

An accelerogram thus extended is then used to generate the baseline corrected accelerogram as outlined in Figure 2. It is clear that the error $f(t)$ now becomes

$$f_s(t) = \begin{cases} \Delta C_0 - \Delta C_1 t & ; -T < t < 0 \\ \Delta C_0 + \Delta C_1 t & ; 0 < t < T \\ \Delta C_0 + 2\Delta C_1 T - \Delta C_1 t & ; T < t < 2T \end{cases}$$

Since $f_s(t)$ is continuous at $t = 0$ and $t = T$, the effect of jumps is thus eliminated. Although the accelerogram is extended in a way that cannot be physically justified, the effect of this even extension on intermediate and short periods is much smaller than the effects resulting from the jumps at $t = 0$ and $t = T$ in $f(t)$, and can be justified on that basis.

When a straight line $v_0 + a_0 t$ is fitted to the velocity $v(t)$ (step 2

in Figure 2) small errors Δv_0 and Δa_0 are introduced in the estimates of v_0 and a_0 . When velocity is integrated, errors Δv_0 , Δa_0 and the error Δd_0 (assuming that the ground displacement was zero at $t = 0$), introduce an error

$$\Delta d_0 + \Delta v_0 t + \frac{1}{2} \Delta a_0 t^2$$

in the computed ground displacement. These errors possess periods longer than 16 seconds, which are entirely a result of data processing steps 1 and 2 (Figure 2). Therefore, the second refinement added to the standard baseline correction procedures (Trifunac, 1970) consists of high-pass filtering the ground velocity and displacement curves (steps 8, 10 and 12, Figure 2), computed by assuming the initial conditions $v(t = 0)$ and $D(t = 0)$ to be zero. This filtering is again performed by using the same Ormsby filter as in step 4 in Figure 2. Prior to filtering, the velocity and displacement curves are extended outside the interval 0 to T as follows

$$\begin{aligned} v(-\tau) &= v(\tau) & ; & & -T < \tau < 0 & \text{ and } d(\tau) = \frac{d(T) - d(0)}{T} \tau; \tau < 0 \text{ and } \tau > T \\ v(T + \tau) &= v(T - \tau) & ; & & T < \tau < 2T \end{aligned}$$

The reasons for such extensions are similar to as those mentioned above for even extension of an accelerogram.

The above two additional refinements of standard baseline correction procedures (Trifunac, 1970) and calculations of ground velocity and displacement curves are believed to be adequate for routine, standard data processing of strong-motion accelerograms. For specific research applications when greater accuracy is required for computed ground

velocity and displacement curves, specific improvements may be called for. It may be feasible to apply these only to the particular accelerogram in question. In such cases uncorrected accelerograms can be used as a starting point in the analysis.

Corrected Accelerograms

Standard processing of corrected accelerograms involves first instrument correction and then baseline correction. From uncorrected accelerograms, digitized at unequally spaced intervals, equally spaced data with 50 points per second are interpolated. To improve accuracy, this interpolation is performed in the following way. First, 100 equally spaced points per second are interpolated from the uncorrected data, assuming a straight line between points. The equally spaced data are then low-pass filtered using the Ormsby filter which has the cut-off frequency $f_c = 25$ cps and the roll-off termination frequency $f_T = 27$ cps (Figures 3 and 4). Subsequent to low-pass filtering the data are decimated by keeping every second point. The resulting sequence has 50 points per second which corresponds to the Nyquist frequency of 25 cps.

Instrument correction is performed by using Equation (1) and the instrument constants ω_0 and ζ_0 , determined from calibration tests of each accelerograph component (Figure 3). Differentiation of the instrument response x is performed by the central difference scheme.

Accelerograms corrected for instrument response are next baseline corrected by high-pass filtering with an Ormsby filter (Figure 2). The output of this operation is the corrected accelerogram, which

FLOW CHART FOR INSTRUMENT AND BASELINE CORRECTION OF ACCELEROGRAMS

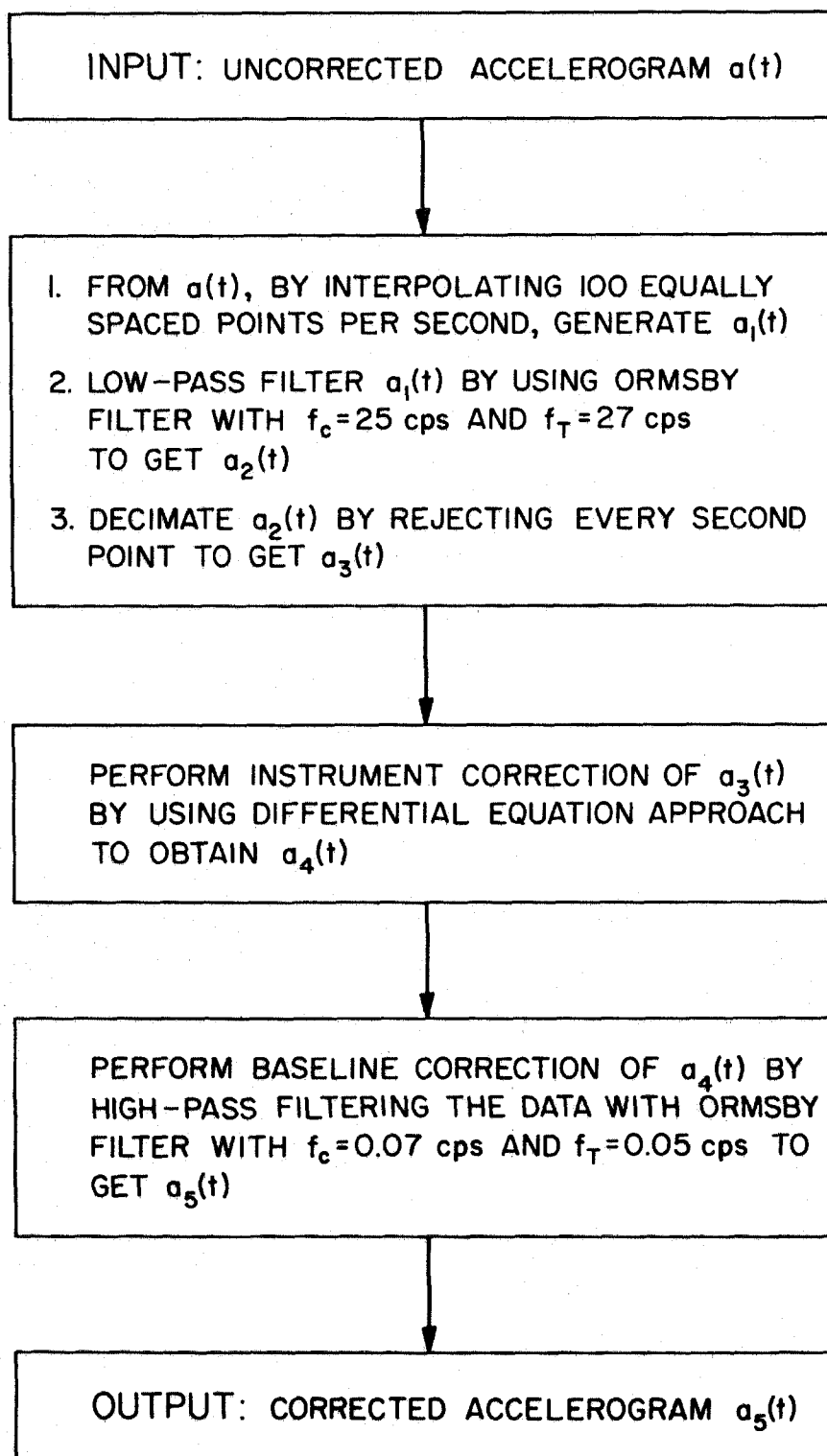


Fig. 3

TRANSFER FUNCTION FOR INSTRUMENT AND BASELINE CORRECTION OF STRONG MOTION ACCELEROGRAMS

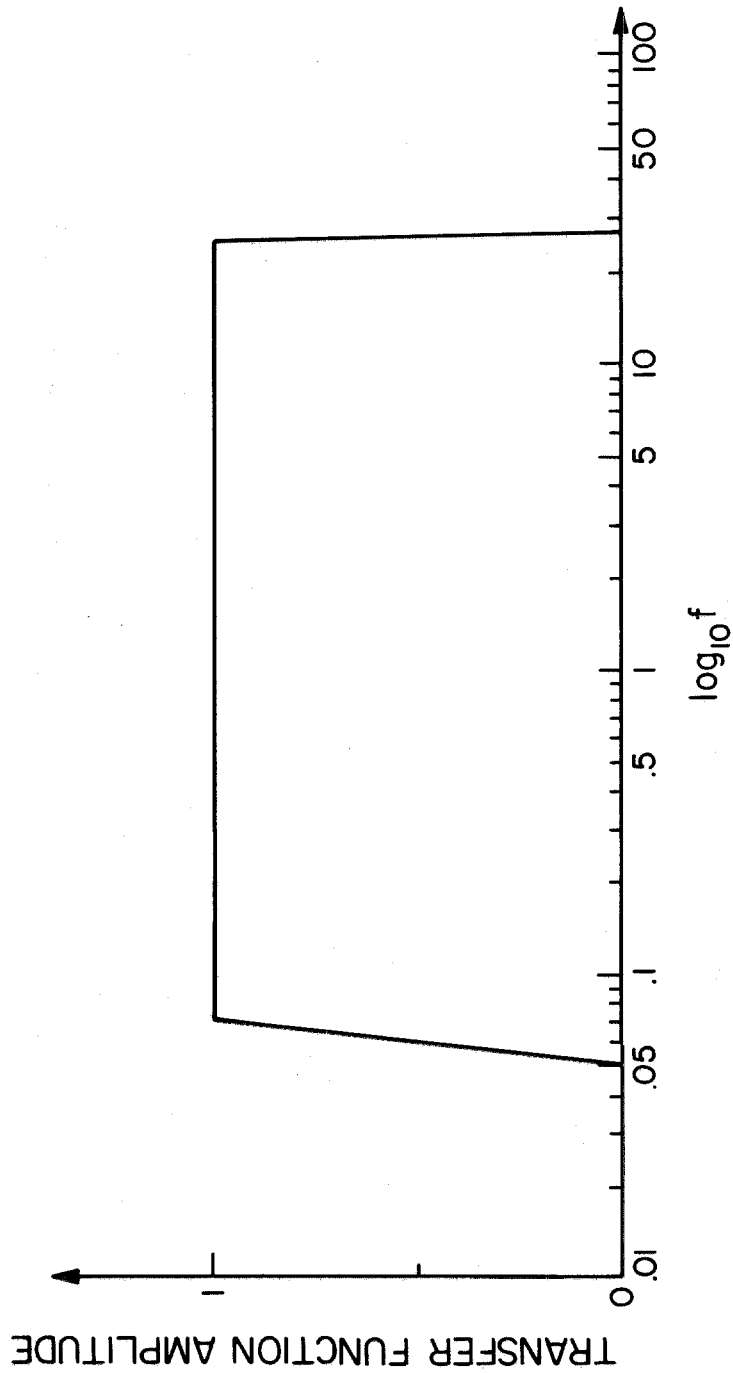


Fig. 4

accurately represents the exact absolute acceleration of the instrument support in the frequency band between 0.07 cps and 25 cps, as shown in Figure 4.

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PRINT-OUTS OF CORRECTED ACCELEROGRAMS AND THE PLOTS OF ACCELERATION, VELOCITY AND DISPLACEMENT CURVES

The scaled, uncorrected accelerogram data, obtained from the first stage of processing and published in several parts of Volume I (Hudson et al., 1969; Brady and Hudson, 1970) are retrieved from magnetic tape storage and corrected for baseline adjustment and instrument frequency response as outlined earlier in this report. This section deals with the format of presentation of the results at the end of this second stage of data processing.

The corrected accelerogram, velocity and displacement for each component of an earthquake record are plotted to appropriate scales; however the accelerogram only is printed out. Details concerning identification and the peak values of acceleration, velocity and displacement, are given at the top of each plot. The first line gives the name, date and time of occurrence of the earthquake; the second line is comprised of two labels, the observation station and component processed. The Roman numeral "II" in the first identification label indicates that the results pertain to the second stage of data processing, i. e., Volume II of corrected accelerogram records. The letter "A" following the Roman numerals implies that the processed record belongs to Part A of Volume II. In fact, it is so arranged that Volume II, Part A consists of the corrected acceleration data for the same records for which the uncorrected data have been published in Volume I, Part A (Hudson et al., 1969). This is valid for all succeeding parts also. The three digit number completing the first label is the Caltech Reference Number for the given earthquake record in Volume I, right-adjusted in a three-digit numerical field. In short IIA013 and IA13 consist of the

corrected and uncorrected acceleration data respectively for the earthquake record with the Caltech Reference Number 13 given in Volume I, Part A. The record label (for instance 57.002.2) is a string of three numbers separated by periods; the first number gives the year in which the earthquake occurred. The second is the serial number of the record as it was received at the Caltech Earthquake Engineering Research Laboratory during that year. The last number indicates whether it was a main event or an aftershock, sequentially numbered, the main event starting from zero.

It will be observed that contrary to general practice, the y-axis is marked positive downwards. Since the accelerograph registers the negative of the true acceleration it is necessary either to invert the recorded accelerogram about the x-axis or change the positive direction of the y-axis. Since investigators are often familiar with typical accelerograms in the form as registered by instrument, it is preferred to label the y-axis suitably and retain the familiar pattern of the accelerograms.

The corrected accelerogram is printed out at equal time intervals of 0.02 seconds. For each component in a record, the identification labels are given in the first line; for convenience the latitude and longitude of the epicenter are printed out also. In the second line, the station number* of the observation station is given as well as its longitude and latitude for the convenience of those who would like to work on seismic waves. The accelerograph characteristics used for instrument correction are also given in each case.

The data are printed out in integer form, with units of mm/sec^2 so as to utilize the printing space more efficiently. There are 20 successive

* Permanent Identification Number in Annual List of Stations issued by Seismological Field Survey, NOAA.

values of acceleration at 0.02 sec intervals printed along each row with some blank spaces after every set of 5 entries for easy reading. Similarly at the end of 10 lines, one row is skipped before printing the succeeding values.

Since the initial values of velocity and displacement are given, with the corresponding acceleration data, it is possible to compute the velocity and displacement curves if numerical values are desired. However, it must be remembered that the integral curves so obtained might need further filtering to eliminate very minor long period errors resulting from small errors in the initial values. This has already been discussed in the previous section.

So that the long period components of the displacements would be clearly revealed, some of the accelerograms have been plotted at a time scale which makes it difficult to see detail in the early portion of the record. In such cases the more extended accelerograms of Volume IA may be referred to, since at the scales involved the eye would not detect significant differences in the uncorrected and corrected accelerograms.

The corrected accelerogram and displacement data are stored on punched cards and on magnetic tapes, copies of which can be supplied at cost from the National Information Service for Earthquake Engineering at the California Institute of Technology.

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Technology

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INSTRUMENT CHARACTERISTICS

<u>Record No.</u>	<u>Location Date & Time</u>	<u>Direction</u>	<u>Instr. No.</u>	<u>Period, T_o (sec)</u>	<u>Sens.* cm/g</u>	<u>Damp* ratio ε</u>	<u>Damp* % crit.</u>
IIA001	El Centro 5-18-40, 2037PST	South West Vert	L56 T57 V55	.099 .100 .095	26.9 26.4 24.3	8 7 9	55.2 52.8 57.4
IIA002	Ferndale 10-7-51, 2011PST	S44W N46W V	L248 T249 V247	.066 .065 .066	14.5 12.6 13.4	9 10 12	57.4 59.2 62.1
IIA003	Pasadena 7-21-52, 9453PDT	S W V	L326 T327 V325	.080 .081 .082	19.2 19.8 20.6	8 8 9	55.2 55.2 57.4
IIA004	Taft 7-21-52, 0453PDT	N21E S69E V	L299 T300 V298	.081 .082 .080	19.8 20.2 18.2	9 8 8	57.4 55.2 55.2
IIA005	Santa Barbara 7-21-52, 0453PDT	N42E S48E V	L260 T261 V259	.064 .066 .066	13.2 13.6 13.7	6 7 7	49.5 52.8 52.8
IIA006	Hollywood Storage Basement 7-21-52, 0453PDT	S E V	T215 L216 V217	.064 .066 .065	12.7 13.7 13.3	9 8 12	57.4 55.2 62.1
IIA007	Hollywood Storage PE Lot 7-21-52, 0453PDT	S E V	T212 L213 V214	.066 .066 .065	13.3 13.2 13.2	9 9 8	57.4 57.4 55.2

* See footnotes at end of table.

INSTRUMENT CHARACTERISTICS (continued)

<u>Record No.</u>	<u>Location Date & Time</u>	<u>Direction</u>	<u>Instr. No.</u>	<u>Period T_o(sec)</u>	<u>Sens.* cm/g</u>	<u>Damp* ratio ε</u>	<u>Damp* % crit.</u>
IIA008	Eureka 12-21-54, 1156PST	N11W N79E V	T252 L251 V250	.067 .066 .066	13.5 13.3 12.7	12 10 7	62.1 59.2 52.8
IIA009	Ferndale 12-21-54, 1156PST	N44E N46W V	L248 T249 V247	.066 .064 .066	13.5 12.6 13.2	9 12 13	57.4 62.1 63.2
IIA010	San Jose B of A Bsmt. 9-4-55, 1801PST	N31W N59E V	200 201 202	.066 .066 .066	12.7 12.7 12.9	10 7 9	59.2 52.8 57.4
IIA011	El Centro 2-9-56, 0633PST	S W V	L206 T207 V208	.0661 .0655 .0646	13.55 12.88 12.52	12 12 10	62.1 62.1 59.2
IIA012	El Centro 2-9-56, 0725PST	See 11 El Centro above.					
IIA013	San Francisco SP Bldg Bsmt. 3-22-57, 1144PST	N45E N45W V	194 195 196	.0668 .0665 .0669	13.0 13.1 13.1	10 10 10	59.2 59.2 59.2
IIA014	San Francisco Alex Bldg Bsmt. 3-22-57, 1144PST	N09W N81E V	198 197 199	.0650 .0639 .0635	12.7 12.6 12.0	10 8 7	59.2 55.2 52.8

* See footnotes at end of table.

INSTRUMENT CHARACTERISTICS (continued)

Record No.	Location Date & Time	Direction	Instr. No.	Period, T _o (sec)	Sens.* cm/g	Damp.* ratio ε	Damp.* % crit.
IIA015	San Francisco	N10E	305	.0754	17.1	8	55.2
	Golden Gate Pk.	S80E **	306	.0779	18.1	10	59.2
	3-22-57, 1144PST	V	304	.0764	17.2	8	55.2
IIA016	San Francisco	S09E **	233	.0658	13.2	10	59.2
	State Bldg.	S81W **	234	.0650	12.8	9	57.4
	3-22-57, 1144PST	V	232	.0648	12.6	9	57.4
IIA017	Oakland City	N26E	236	.0662	12.5	9	57.4
	Hall Bsmt.	S64E **	237	.0673	13.2	10	59.2
	3-22-57, 1144PST	V	235	.0668	13.0	11	60.7
IIA018	Hollister	S01W	239	.0660	13.4	9	57.4
	4-8-61, 2323PST	N89W	240	.0659	13.2	9	57.4
		V	238	.0671	13.7	10	59.2
IIA019	El Centro	S	206	.069	14.7	7.6	54.2
	4-8-68, 1830PST	W	207	.067	13.5	8.8	57.0
		V	208	.067	13.5	8.5	56.3
IIA020	San Diego	S	324	.080	20.0	9	57.4
	Light & Power	E	323	.072	19.0	11	60.7
	4-8-68, 1830PST	V	322	.081	20.0	9	57.4

* Static magnification, $V_s = \omega_n^2 \cdot \text{sensitivity} = \left(\frac{2\pi}{T_o(\text{sec})} \right)^2 \cdot \frac{\text{sensitivity (cm/g)}}{980 \text{ cm/sec}^2}$

Damping ratio, $\epsilon = \exp [\pi n / \sqrt{(1 - n^2)}]$ where n is the fraction of critical damping.

** Revised from the corresponding entry in Volume 1.

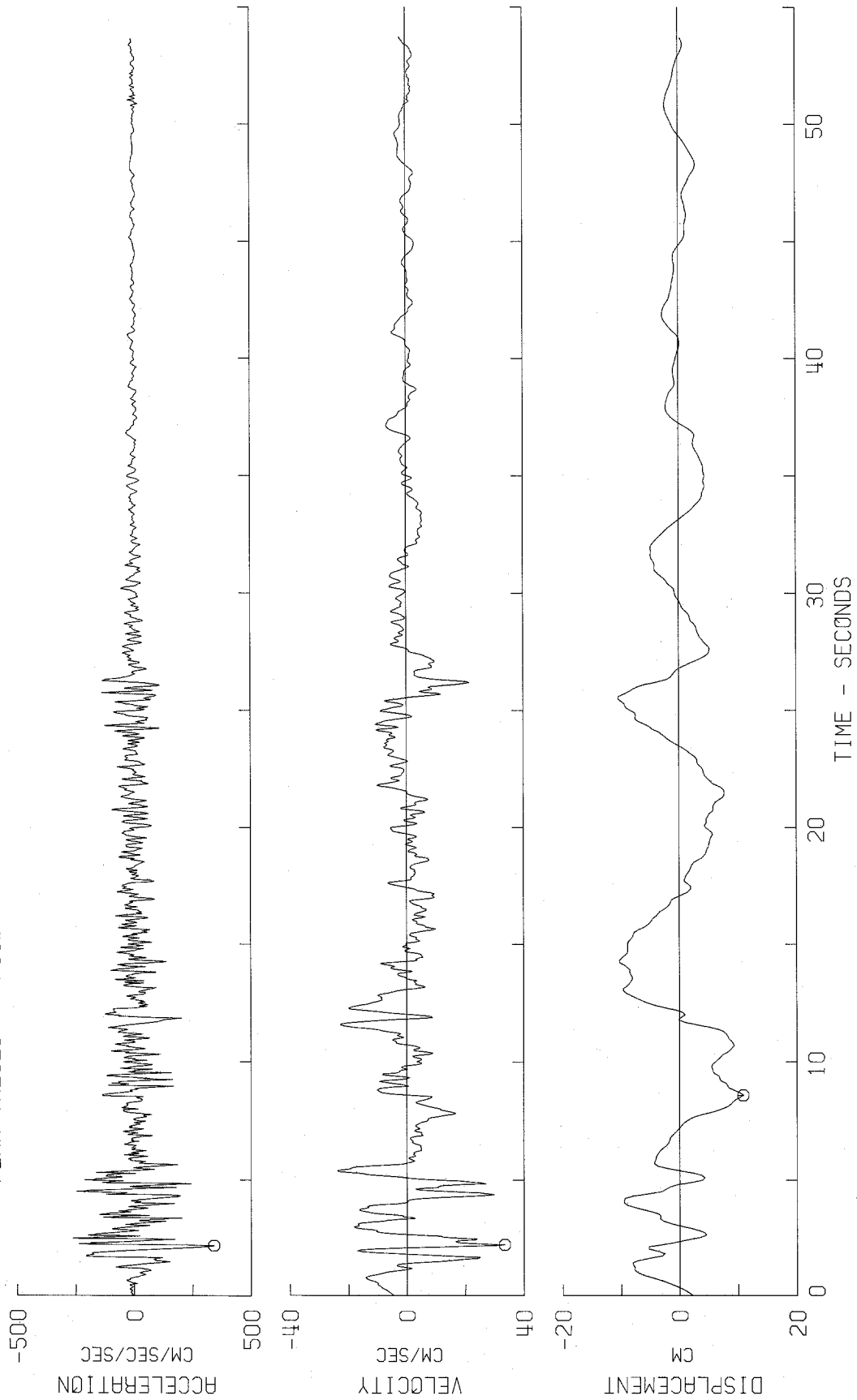
EARTHQUAKE DATA

<u>Date & Time</u>	<u>Location</u>	<u>Epicenter</u>	<u>Max. Intensity</u>	<u>Mag.</u>	<u>References (See Below)</u>
May 18, 1940, 2037PST	Imperial Valley	32°44'N, 115°27'W	X	6.3	1, 2, 3
Oct. 7, 1951, 2011PST	Northwest Calif.	40°17'N, 124°48'W	VII		
July 21, 1952, 9453PDT	Kern County	35°00'N, 119°02'W	XI	7.7	4, 5
Mar. 22, 1957, 1144PST	San Francisco	37°40'N, 122°29'W	VII	5.3	6
Apr. 8, 1961, 2323PST	Hollister	36°40'N, 121°18'W	VII	5.6	
Apr. 8, 1968, 1830PST	Borrego Mtn.	33°09'N, 116°08'W	VII	6.5	7, 8

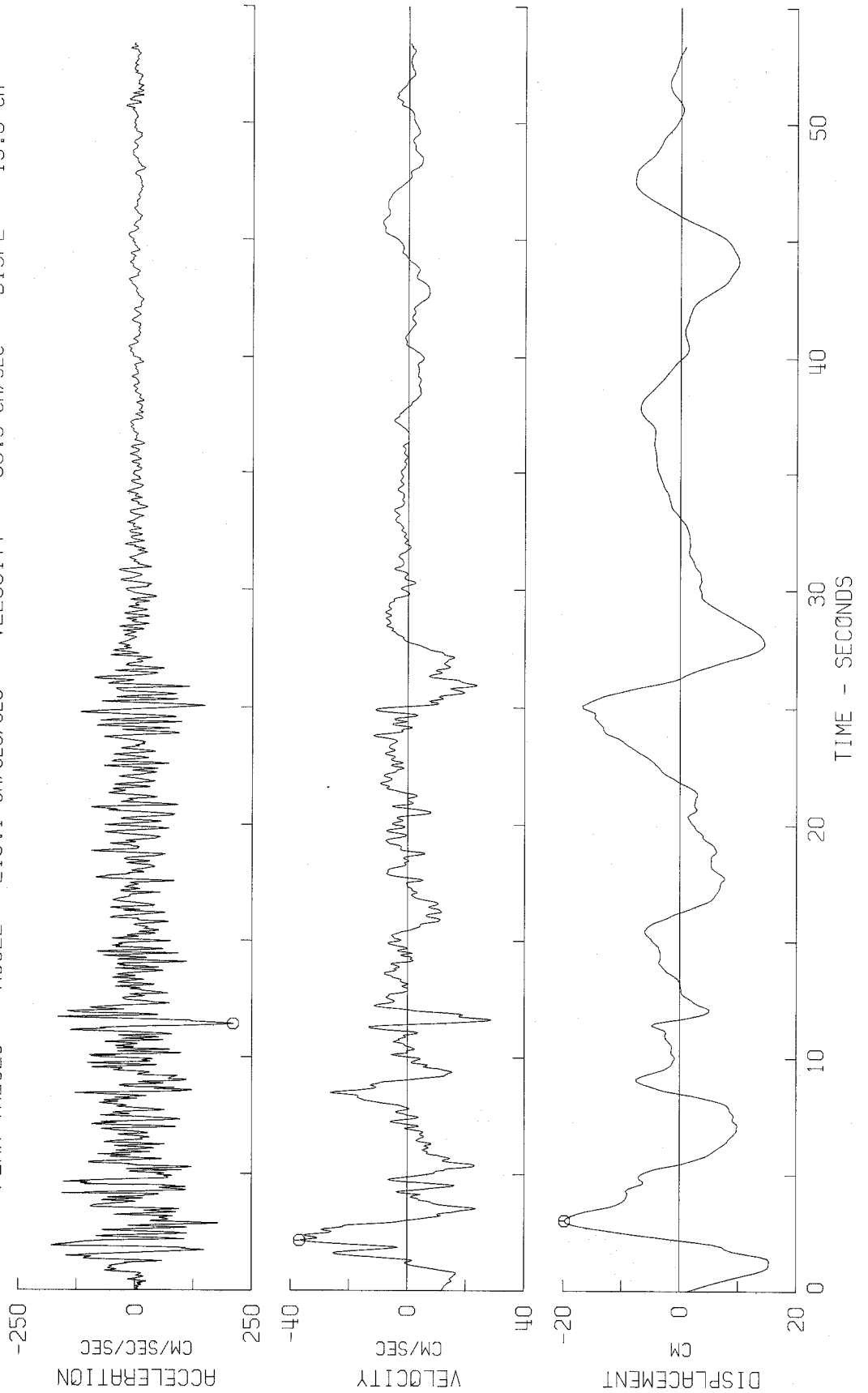
1. Ulrich, F. P., "The Imperial Valley Earthquakes of 1940," BSSA, v. 31, n. 1, January 1941, p. 13-31.
2. Trifunac, M. D. and Brune, J. N., "Complexity of Energy Release During the Imperial Valley, California Earthquake of 1940," BSSA, v. 60, n. 1, February 1970, p. 137-160.
3. Trifunac, M. D., "Response Envelope Spectrum and Interpretation of Strong Earthquake Ground Motion," BSSA, v. 61, n. 2, April 1971, p. 343-356.
4. Steinbrugge, K. V. and Moran, D. F., "An Engineering Study of the Southern California Earthquake of July 21, 1952 and Its Aftershocks," BSSA, v. 44, n. 2B, April 1954.
5. "Earthquakes in Kern County, California During 1952," California Department of Natural Resources, Division of Mines, San Francisco, Bulletin 171, November 1955.

6. "San Francisco Earthquakes of March, 1957," California Division of Mines, Special Report 57, 1959.
7. "Strong Motion Instrument Data on the Borrego Mountain Earthquake of 9 April 1968," Joint Report by the Seismological Field Survey, USCGS, Environmental Science Services Administration, US Department of Commerce, and the Earthquake Engineering Research Laboratory, California Institute of Technology, August 1968.
8. Allen, C. R., et al., "The Borrego Mountain, California, Earthquake of 9 April 1968: A Preliminary Report," BSSA, v. 58, n. 3, June 1968.

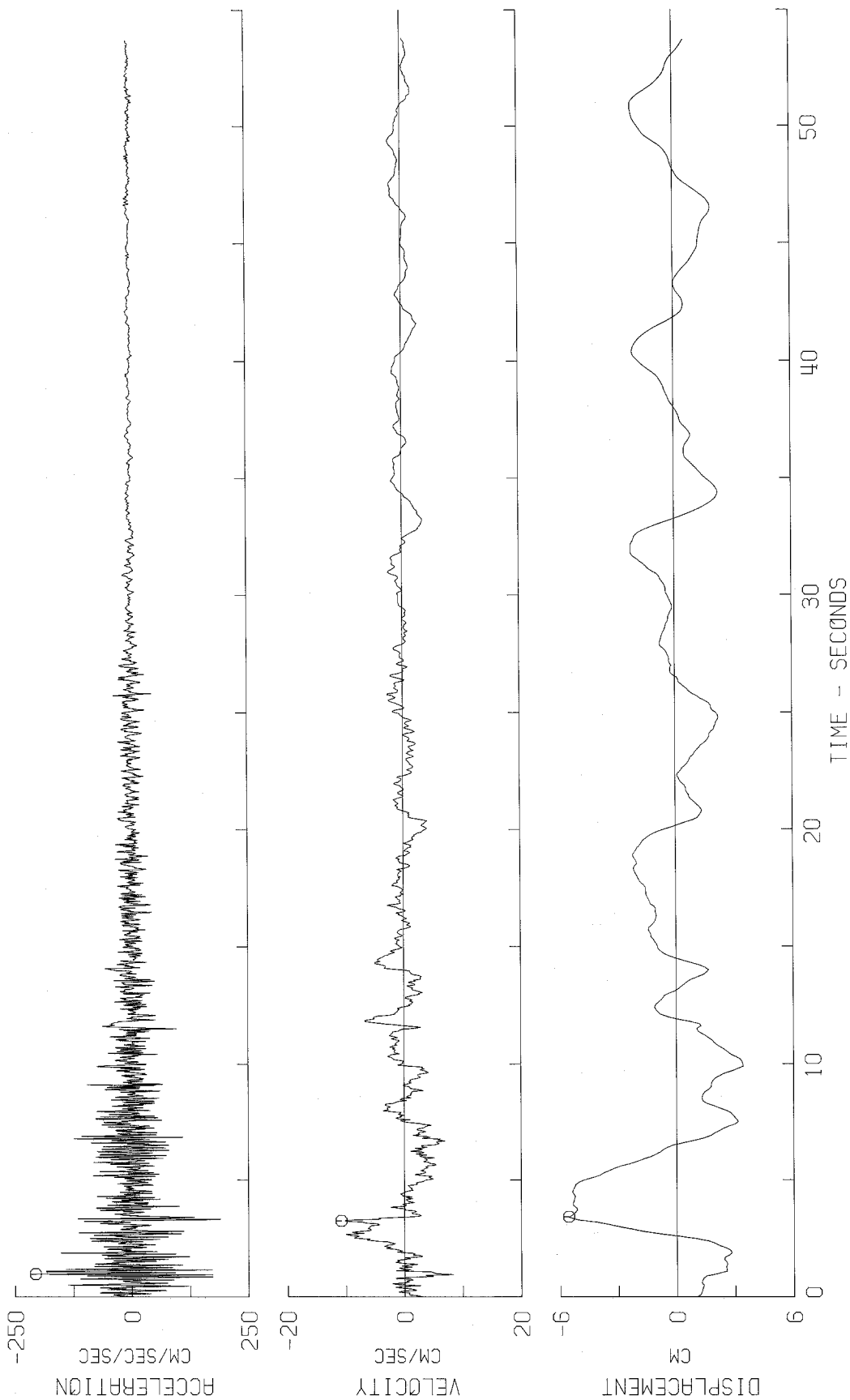
IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST
IIA001 40.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S00E
PEAK VALUES : ACCEL = 341.7 CM/SEC/SEC VELOCITY = 33.4 CM/SEC DISPL = 10.9 CM



IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST
IIA001 40.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S90W
PEAK VALUES : ACCEL = 210.1 CM/SEC/SEC VELOCITY = -36.9 CM/SEC DISPL = -19.8 CM



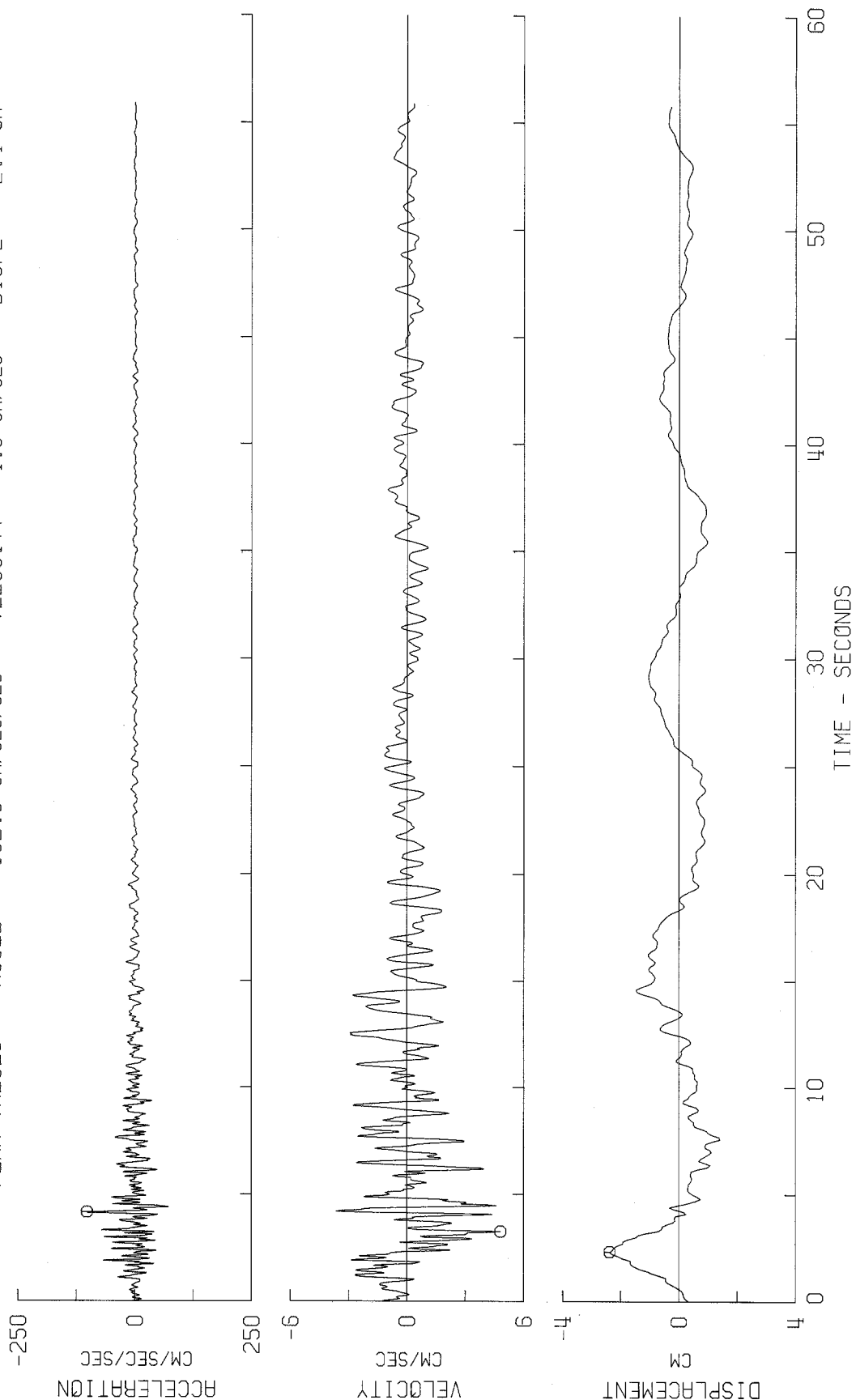
IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST
IIA001 40.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT
PEAK VALUES: ACCEL = -206.3 CM/SEC/SEC VELOCITY = -10.8 CM/SEC DISPL = -5.6 CM



NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST

IIA002 51.001.0 FERNDAL CITY HALL COMP S44W

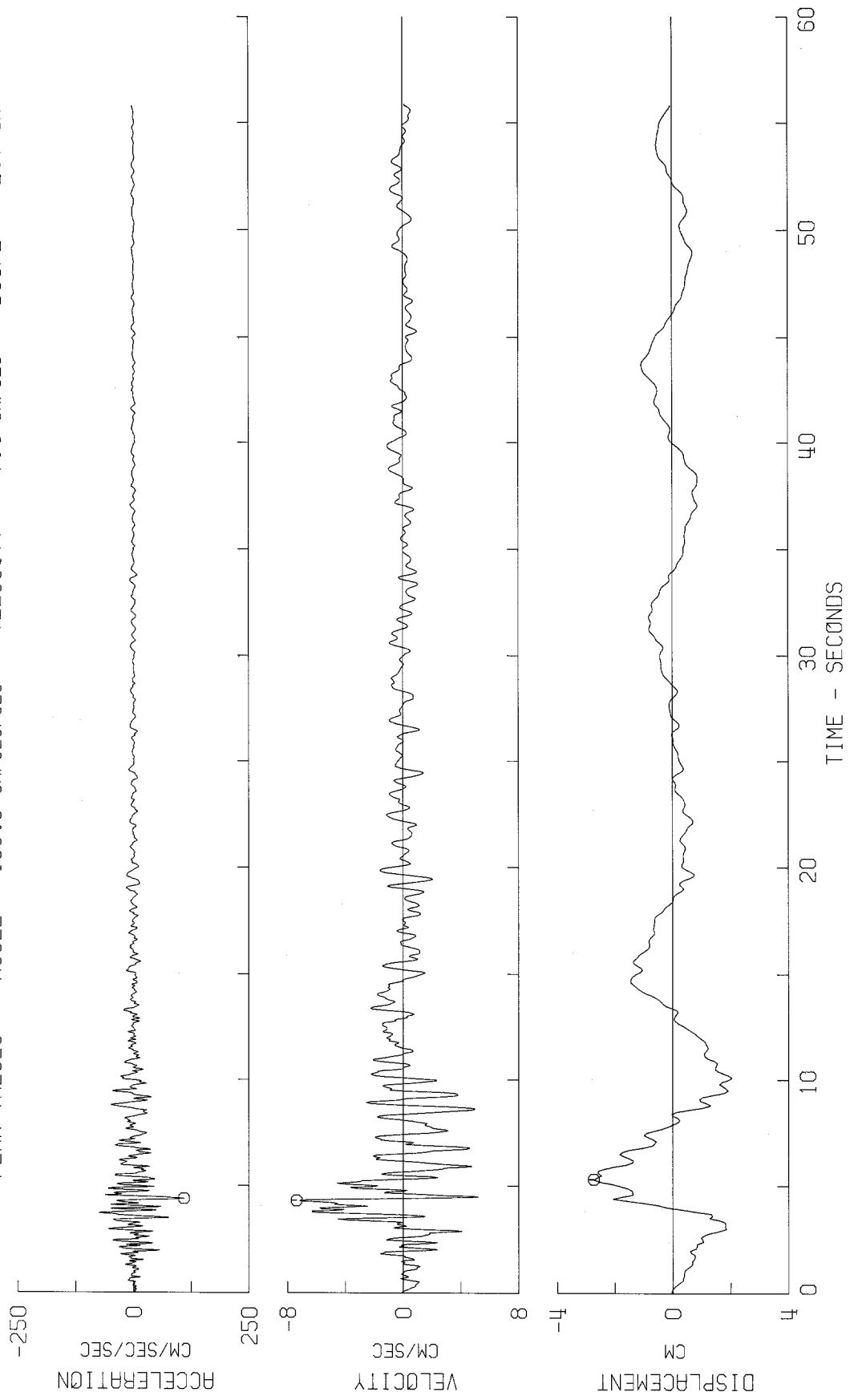
PEAK VALUES : ACCEL = -102.0 CM/SEC/SEC VELOCITY = 4.8 CM/SEC DISPL = -2.4 CM



NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST

IIA002 51.001.0 FERNDAL CITY HALL COMP N46W

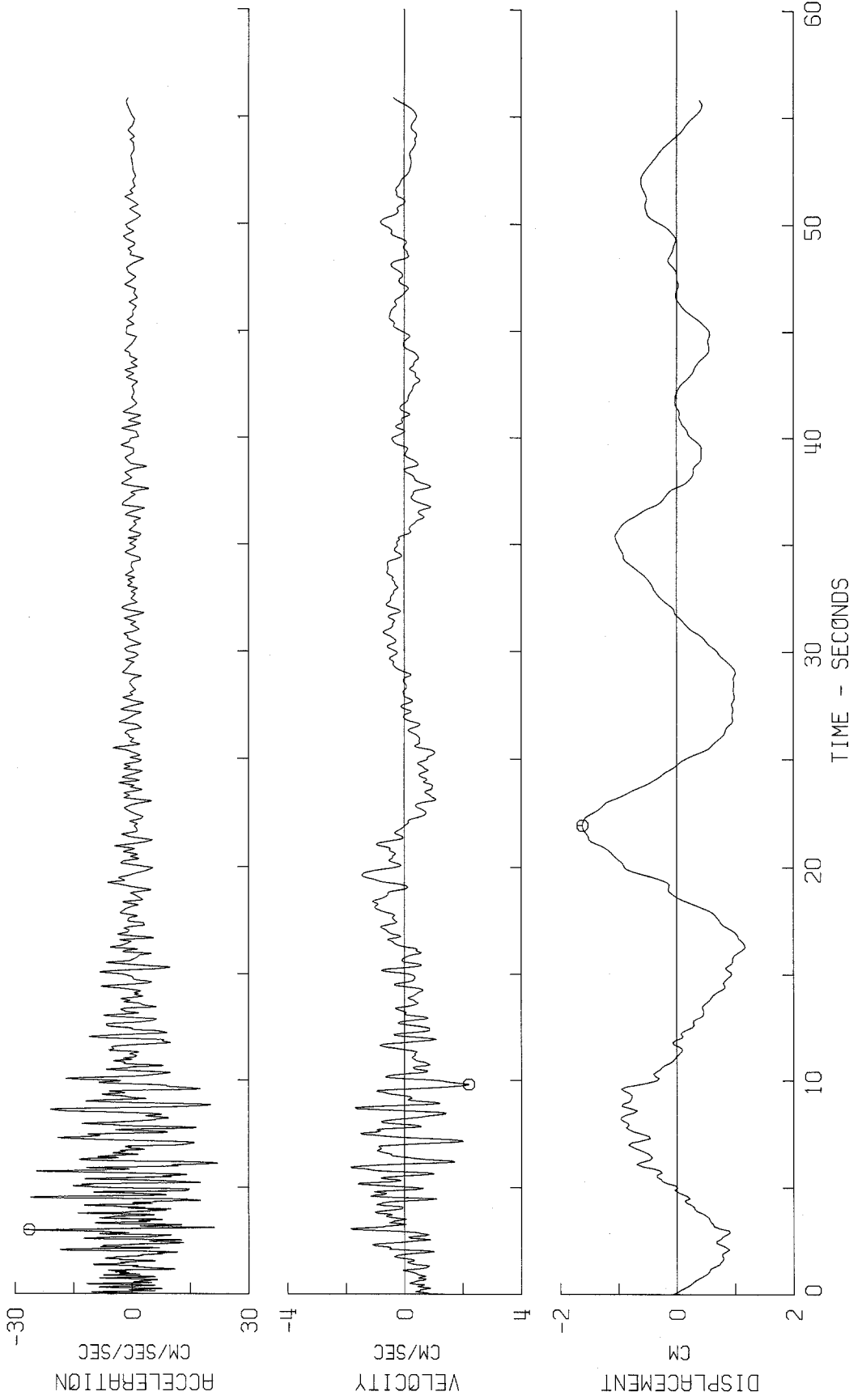
PEAK VALUES : ACCEL = 109.5 CM/SEC/SEC VELOCITY = -7.4 CM/SEC DISPL = -2.7 CM



NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST

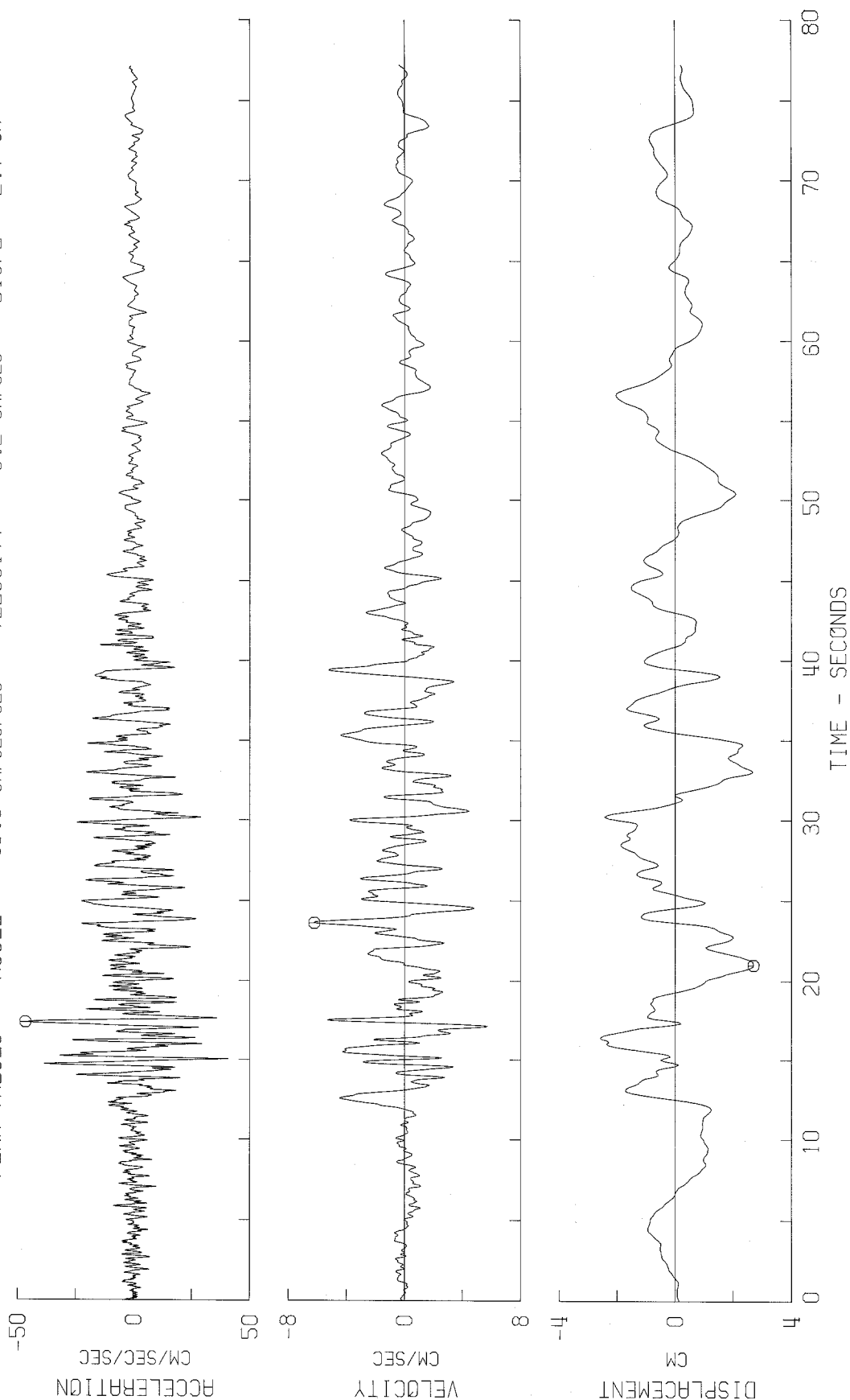
IIA002 51.001.0 FERNDALE CITY HALL COMP VERT

PEAK VALUES : ACCEL = -26.4 CM/SEC/SEC VELOCITY = 2.2 CM/SEC DISPL = -1.6 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
 IIA003 52.001.0 PASADENA - CALTECH ATHENAEUM COMP S00E

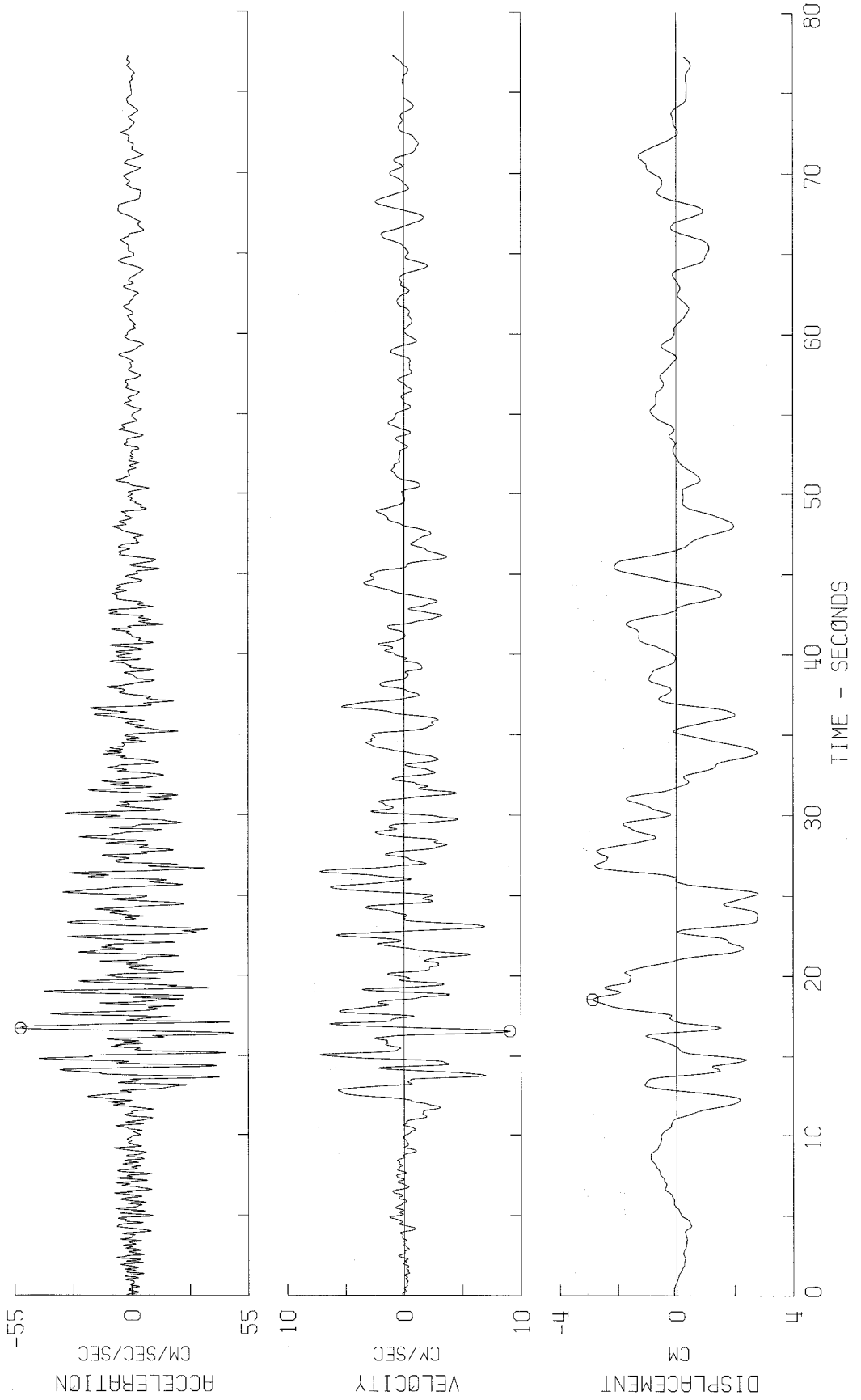
⊙ PEAK VALUES : ACCEL = -46.5 CM/SEC/SEC VELOCITY = -6.2 CM/SEC DISPL = 2.7 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

IIA003 52.001.0 PASADENA - CALTECH ATHENAEUM COMP S90W

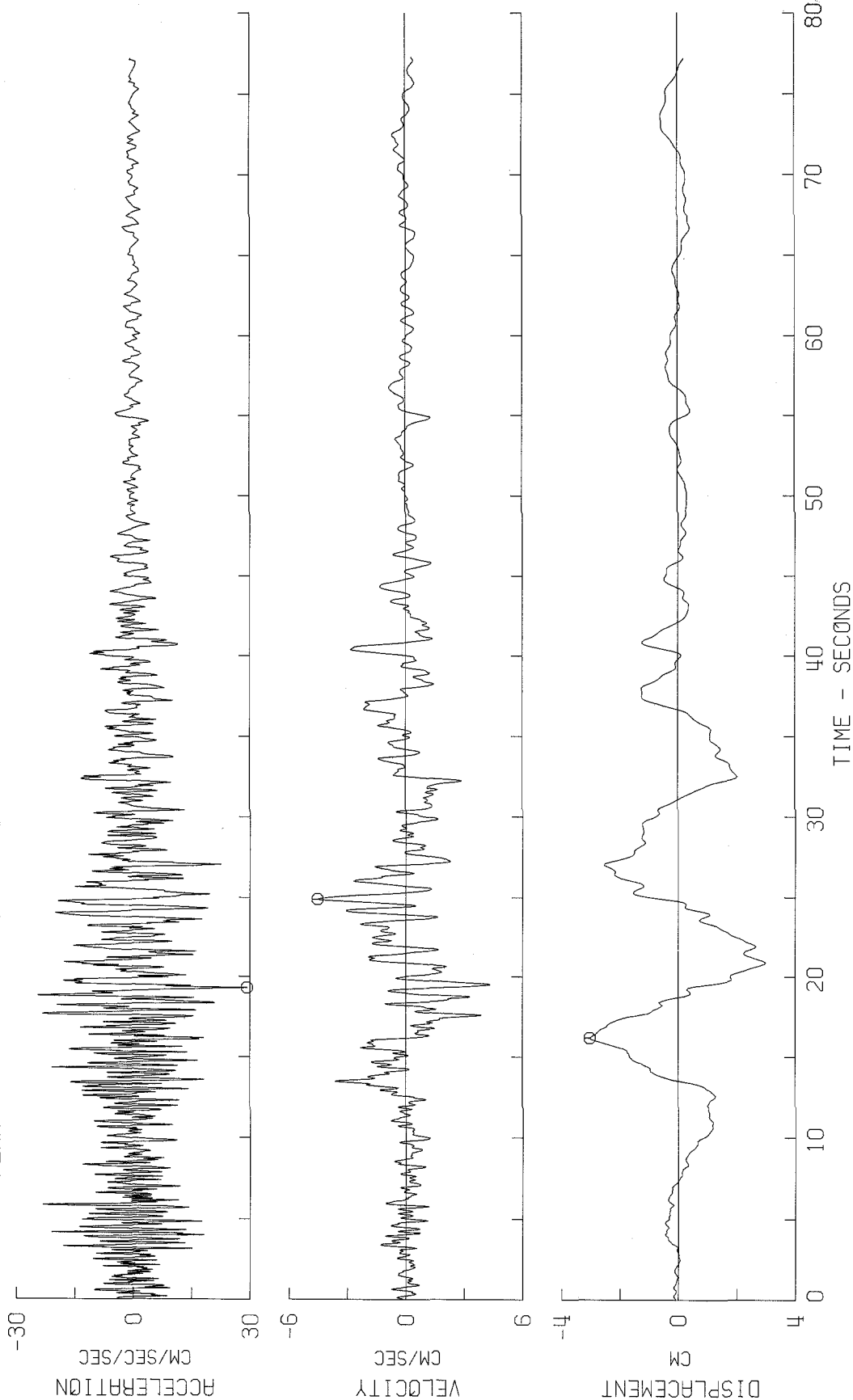
○ PEAK VALUES : ACCEL = -52.1 CM/SEC/SEC VELOCITY = 9.1 CM/SEC DISPL = -2.9 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

IIR003 52.001.0 PASADENA - CALTECH ATHENAEUM COMP VERT

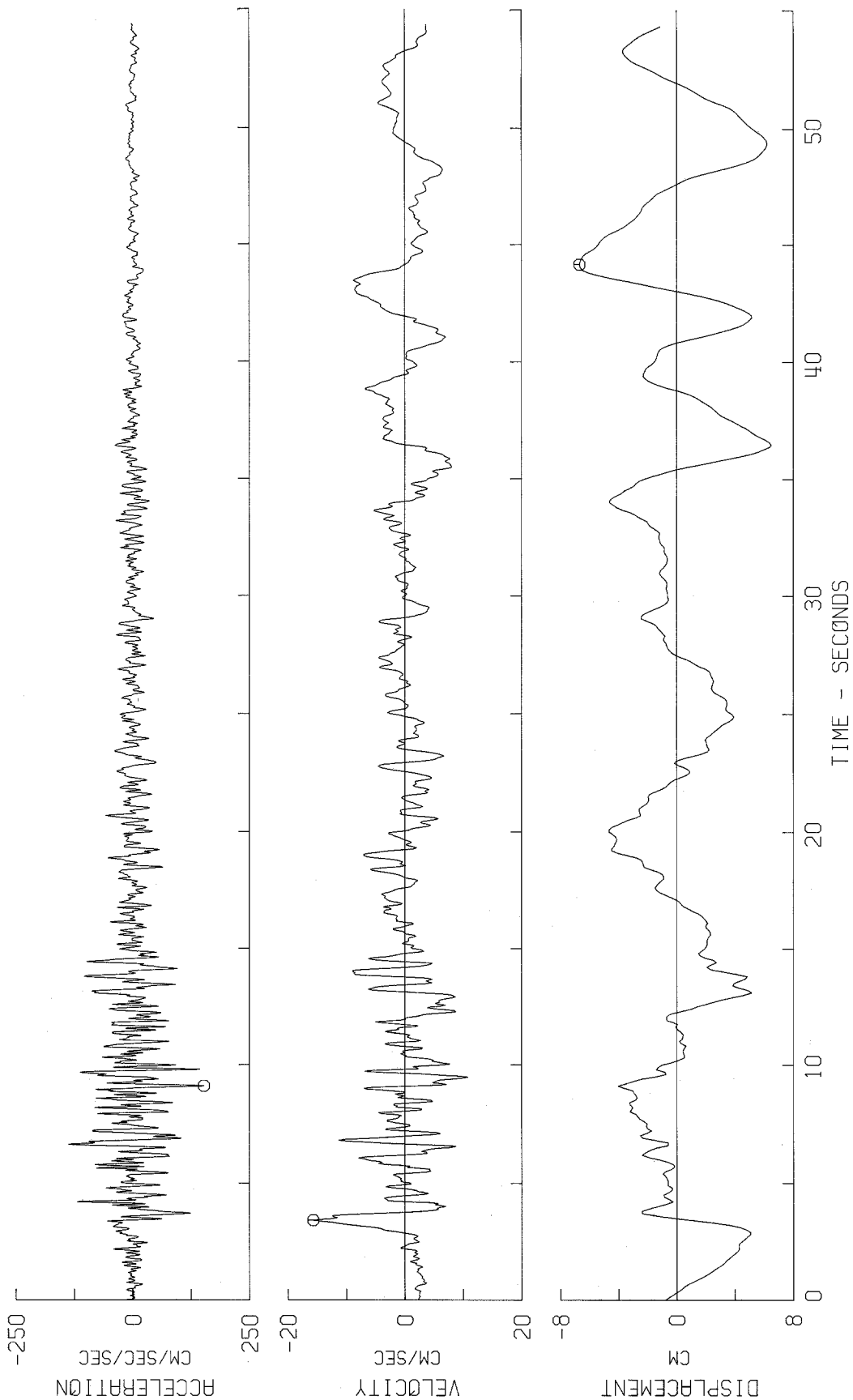
⊙ PEAK VALUES : ACCEL = 29.3 CM/SEC/SEC VELOCITY = -4.5 CM/SEC DISPL = -3.0 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

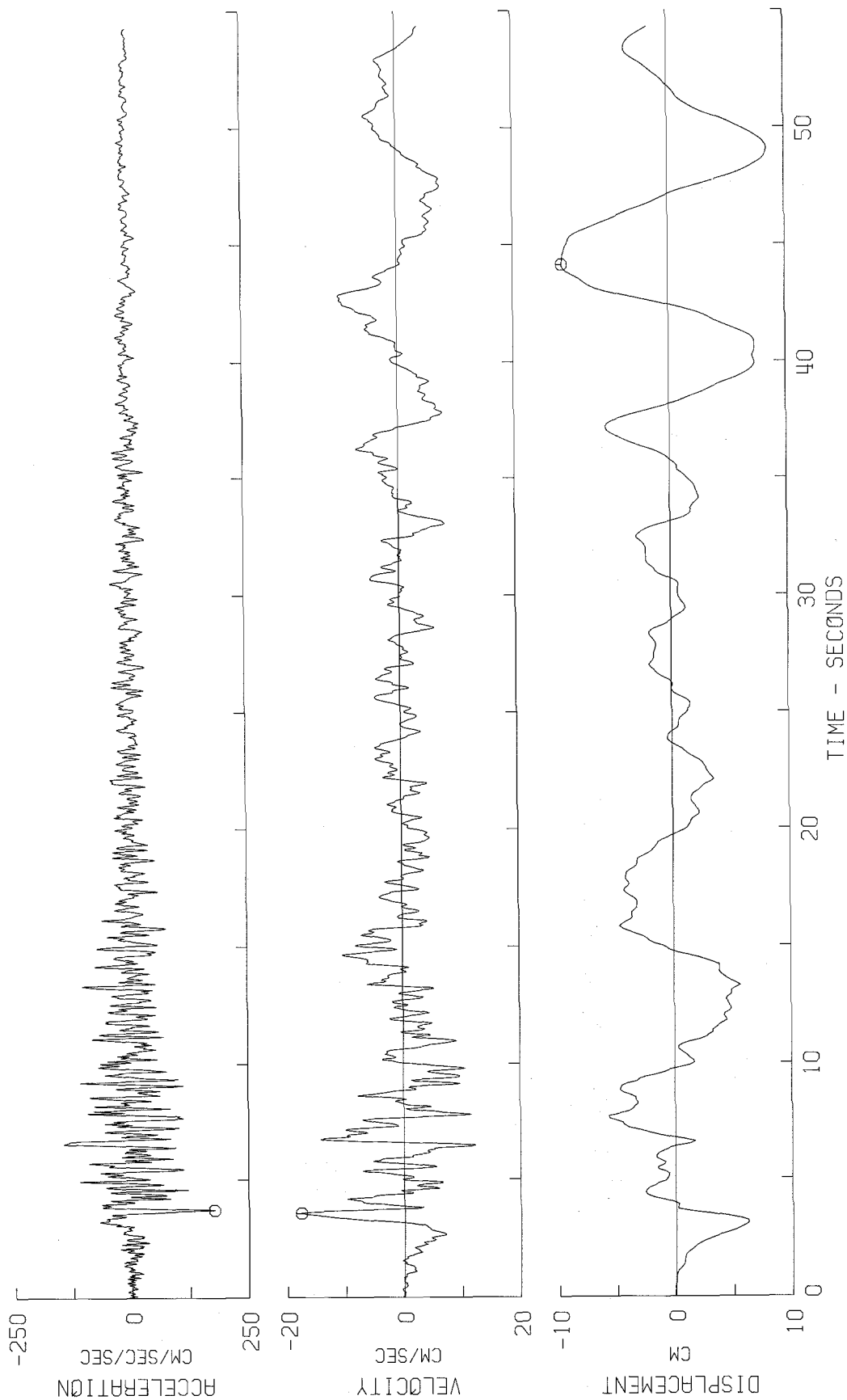
IIA004 52.002.0 TAFT LINCOLN SCHOOL TUNNEL COMP N21E

⊙ PEAK VALUES : ACCEL = 152.7 CM/SEC/SEC VELOCITY = -15.7 CM/SEC DISPL = -6.7 CM



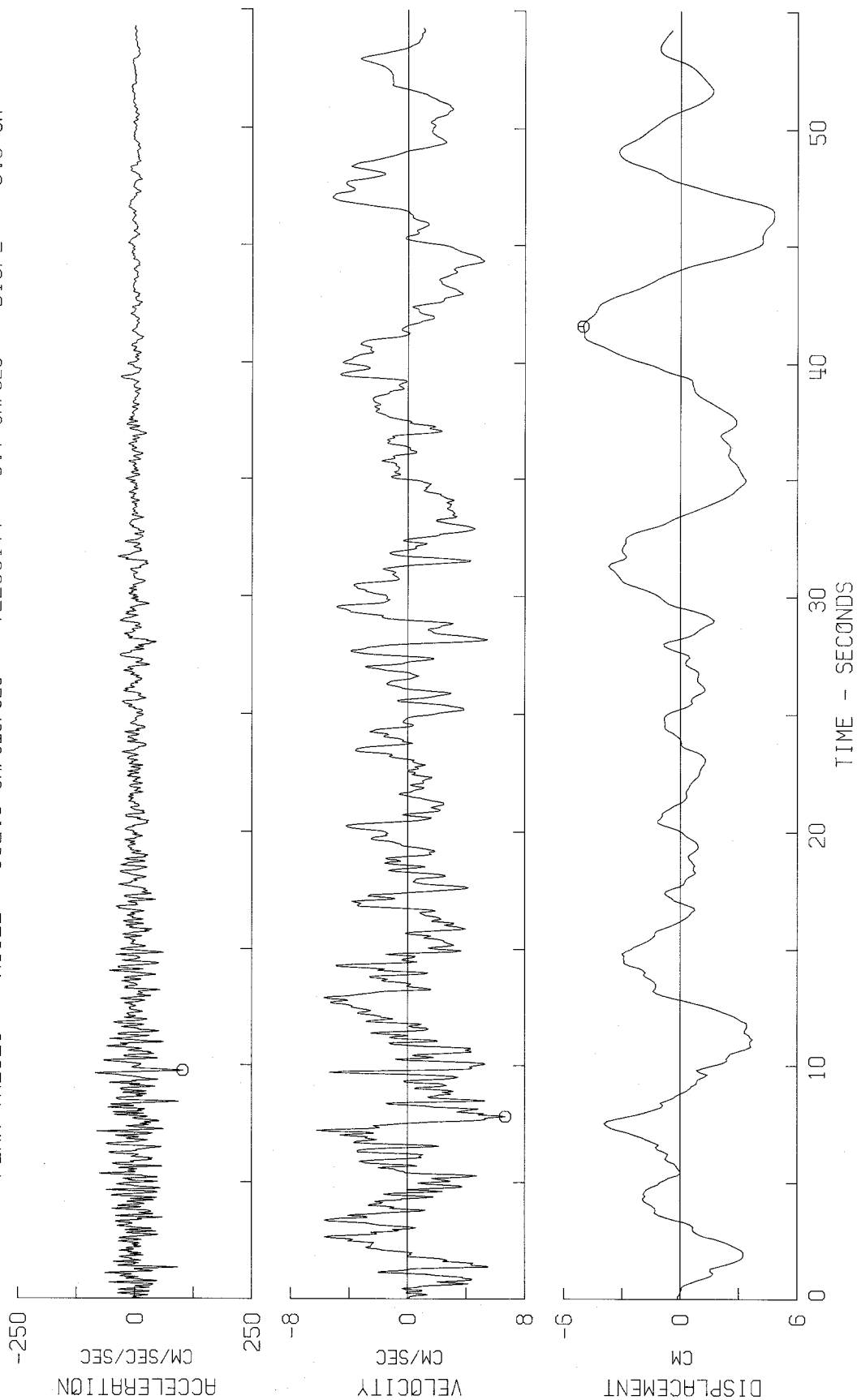
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA004 52.002.0 TAFT LINCOLN SCHOOL TUNNEL COMP S69E

PEAK VALUES : ACCEL = 175.9 CM/SEC/SEC VELOCITY = -17.7 CM/SEC DISPL = -9.2 CM



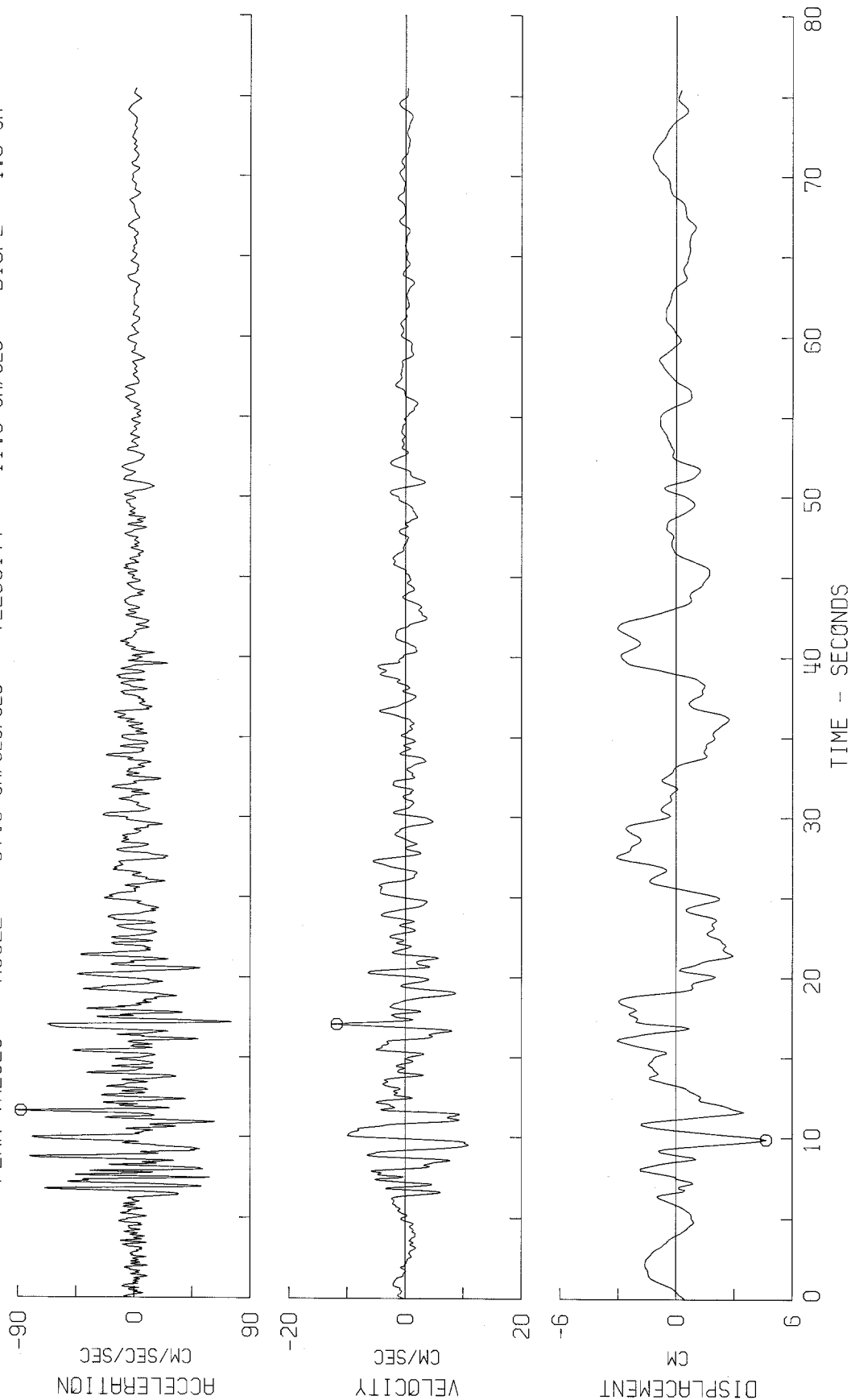
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA004 52.002.0 TAFT LINCOLN SCHOOL TUNNEL COMP VERT

⊙ PEAK VALUES : ACCEL = 102.9 CM/SEC/SEC VELOCITY = 6.7 CM/SEC DISPL = -5.0 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA005 52.003.0 SANTA BARBARA COURTHOUSE COMP N42E

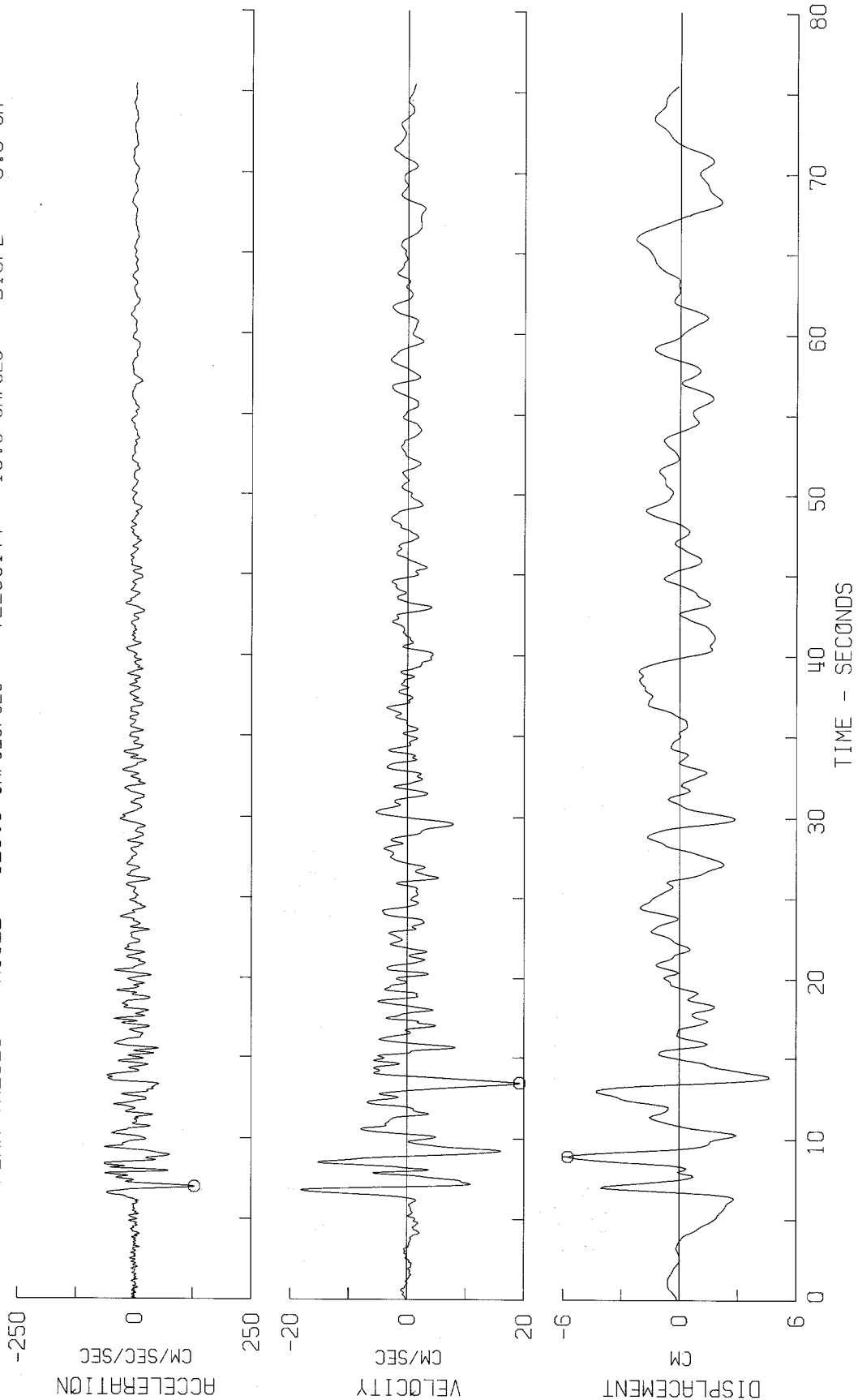
○ PEAK VALUES : ACCEL = -87.8 CM/SEC/SEC VELOCITY = -11.8 CM/SEC DISPL = 4.6 CM



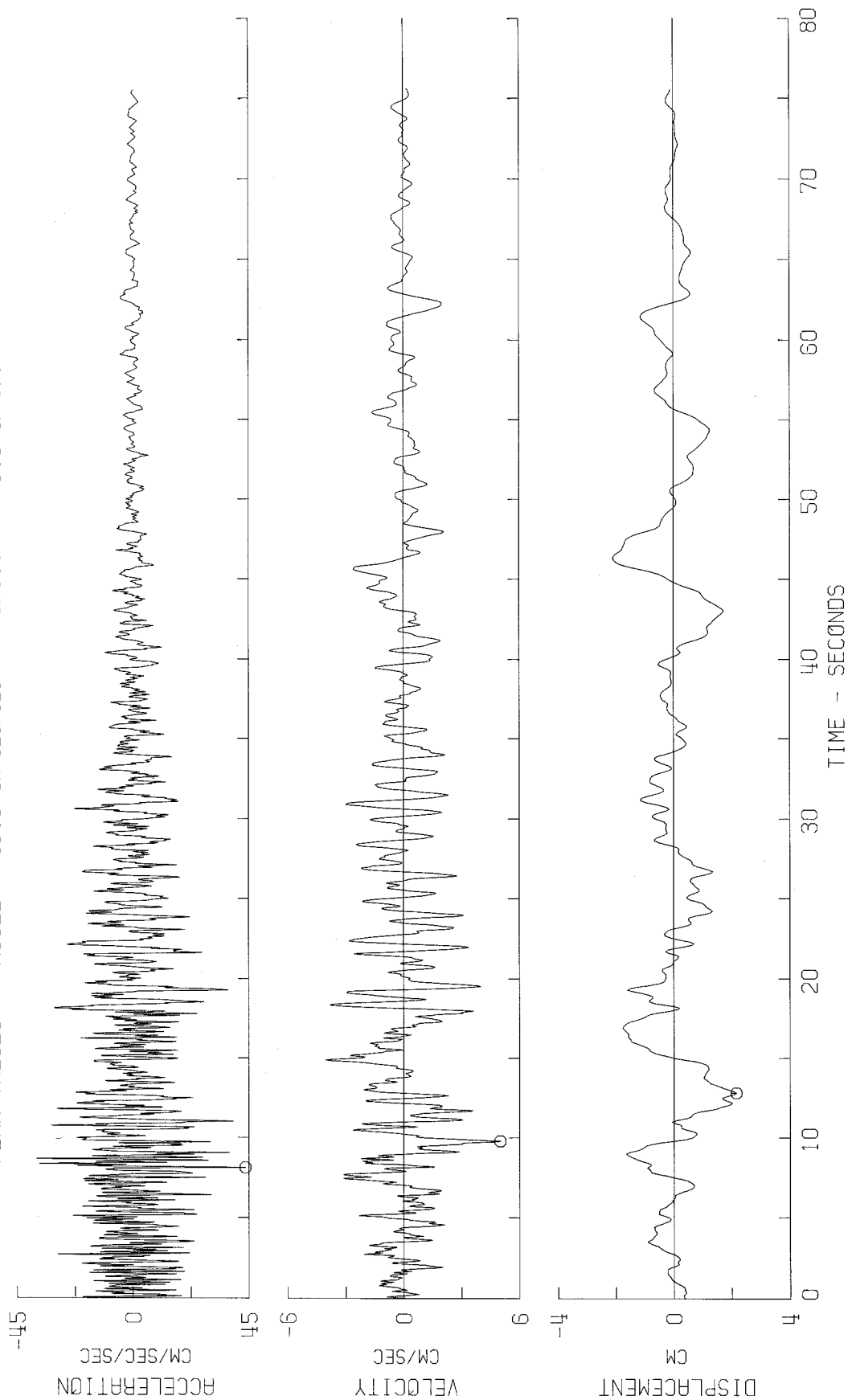
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

IIA005 52.003.0 SANTA BARBARA COURTHOUSE COMP S48E

⊙ PEAK VALUES : ACCEL = 128.6 CM/SEC/SEC VELOCITY = 19.3 CM/SEC DISPL = -5.8 CM



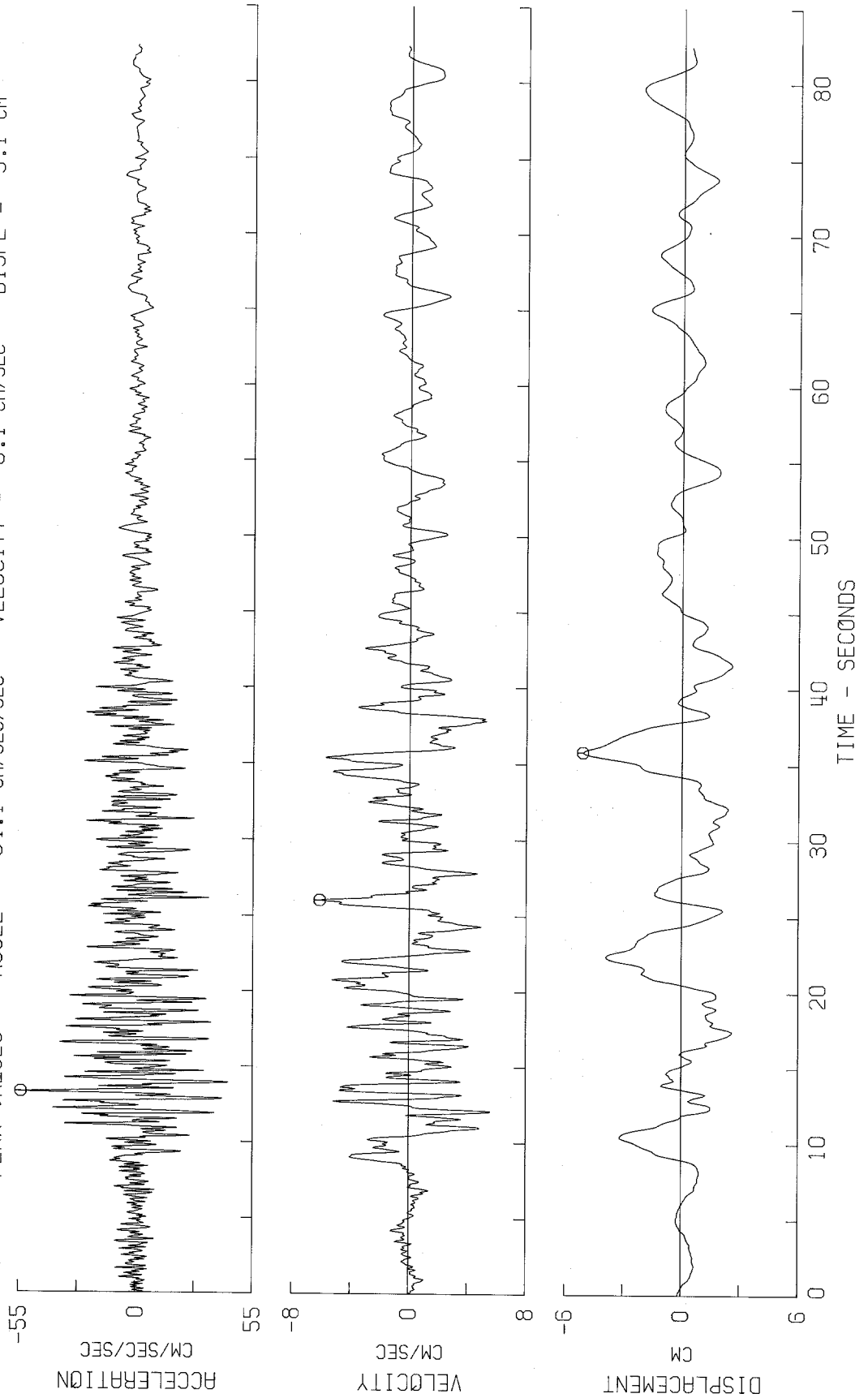
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 -- 0453 PDT
 IIA005 52.003.0 SANTA BARBARA COURT HOUSE COMP VERT
 ○ PEAK VALUES: ACCEL = 43.6 CM/SEC/SEC VELOCITY = 5.0 CM/SEC DISPL = 2.2 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

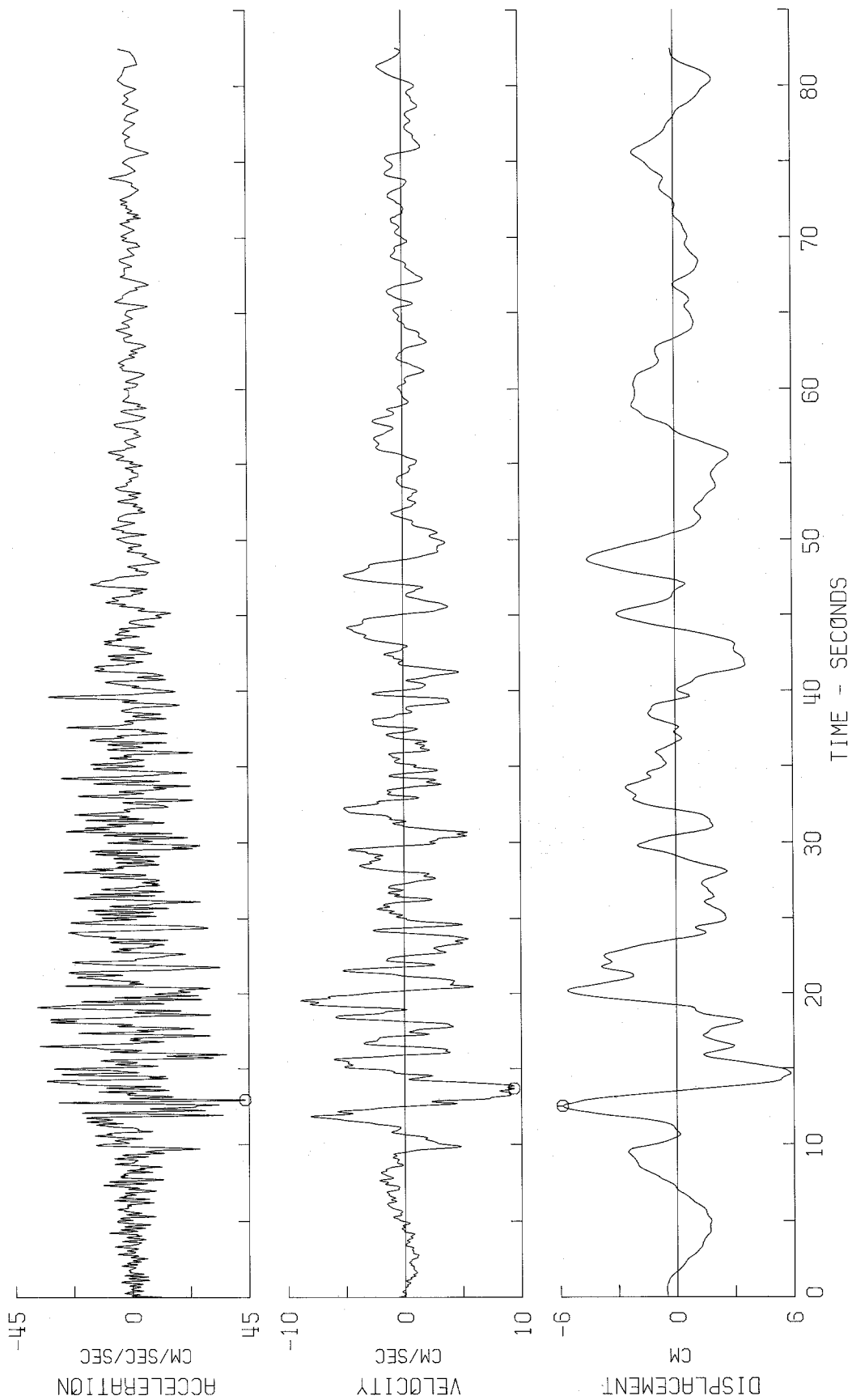
IIA006 52.005.0 HOLLYWOOD STORAGE BASEMENT COMP S00W

Ø PEAK VALUES : ACCEL = -54.1 CM/SEC/SEC VELOCITY = -6.1 CM/SEC DISPL = -5.1 CM

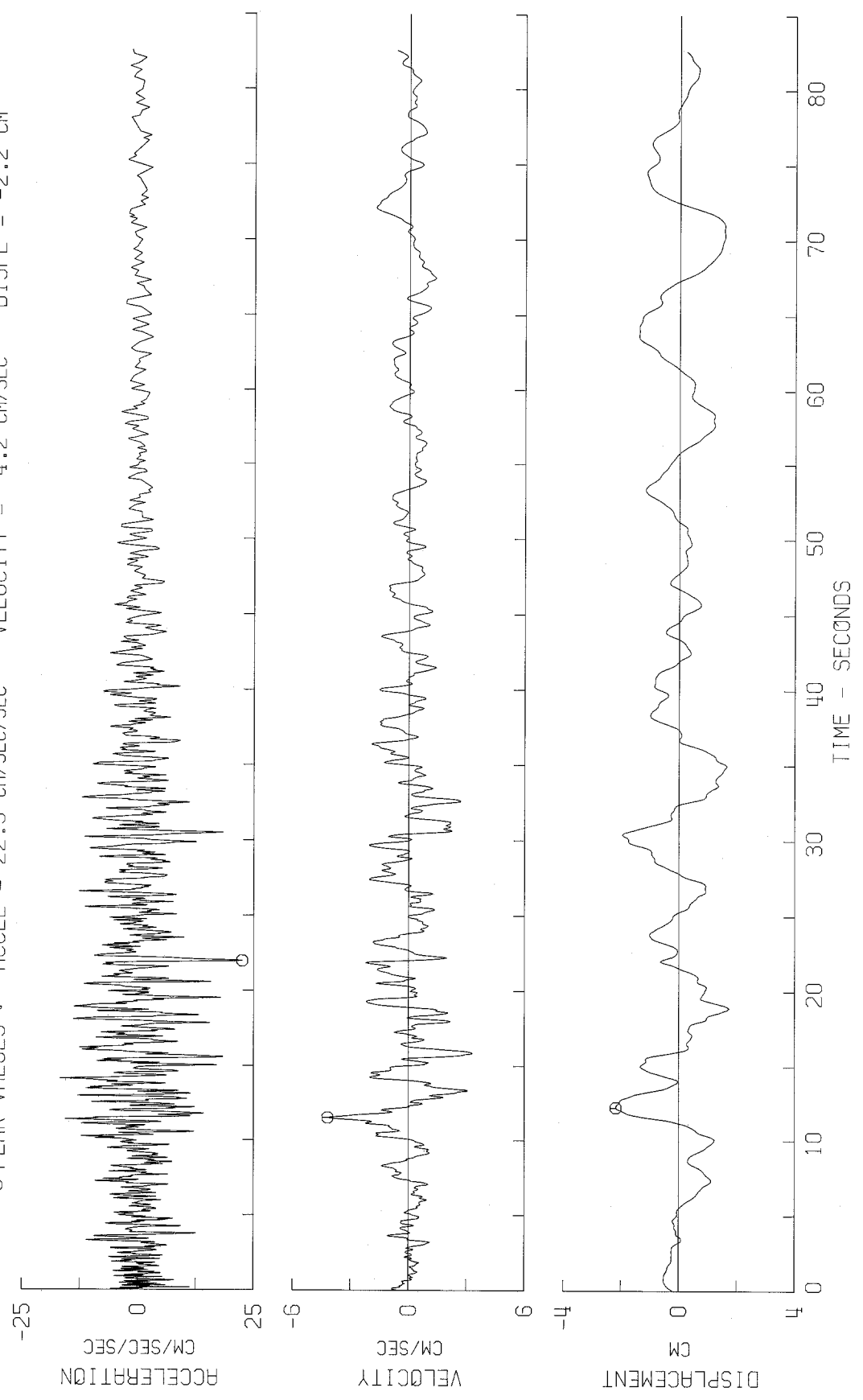


KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA006 52.005.0 HOLLYWOOD STORAGE BASEMENT COMP N90E

PEAK VALUES : ACCEL = 43.5 CM/SEC/SEC VELOCITY = 9.4 CM/SEC DISPL = -5.9 CM



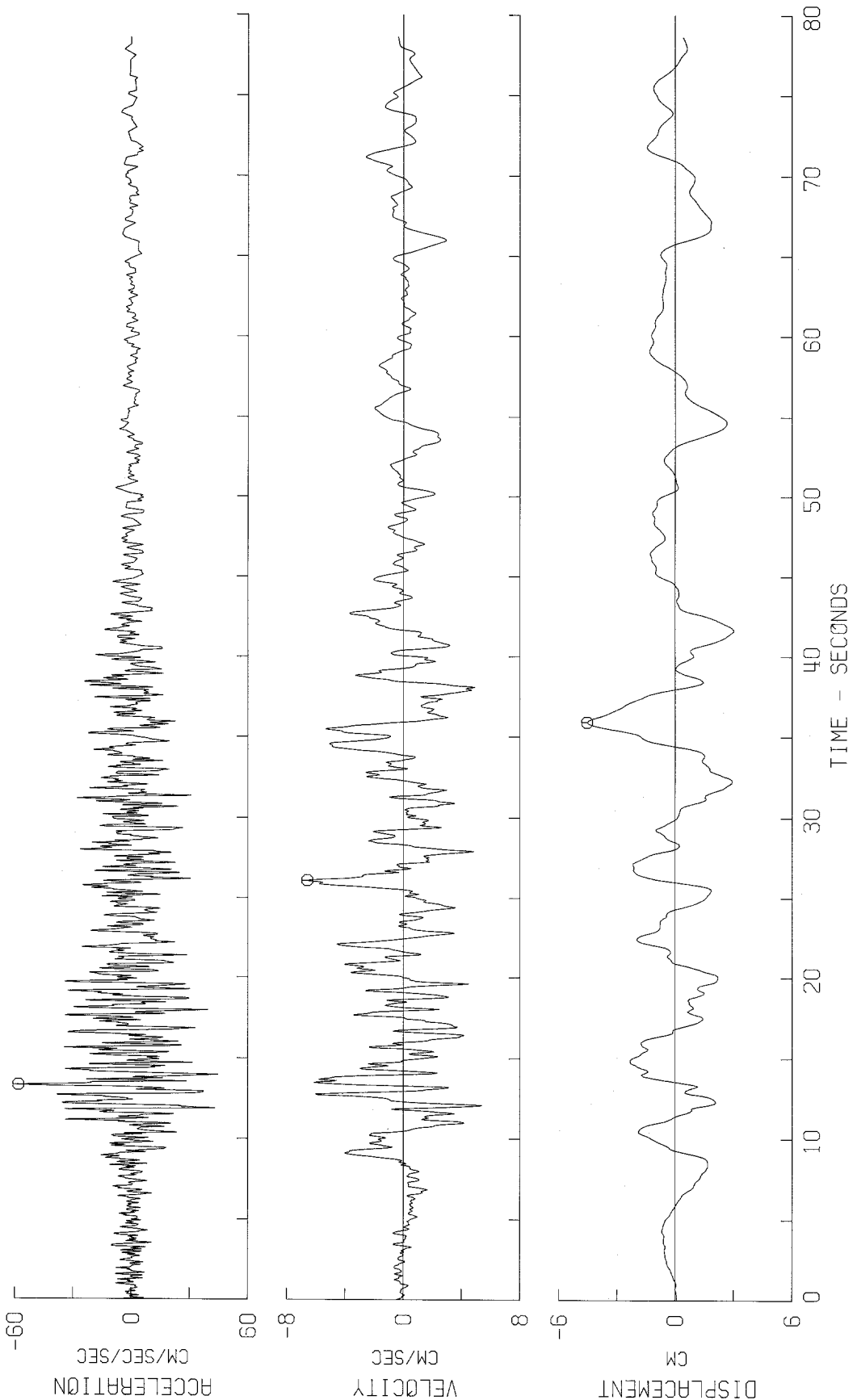
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA006 52.005.0 HOLLYWOOD STORAGE BASEMENT COMP VERT
PEAK VALUES : ACCEL = 22.5 CM/SEC/SEC VELOCITY = -4.2 CM/SEC DISPL = -2.2 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

IIA007 52.006.0 HOLLYWOOD STORAGE P.E. LOT COMP S00W

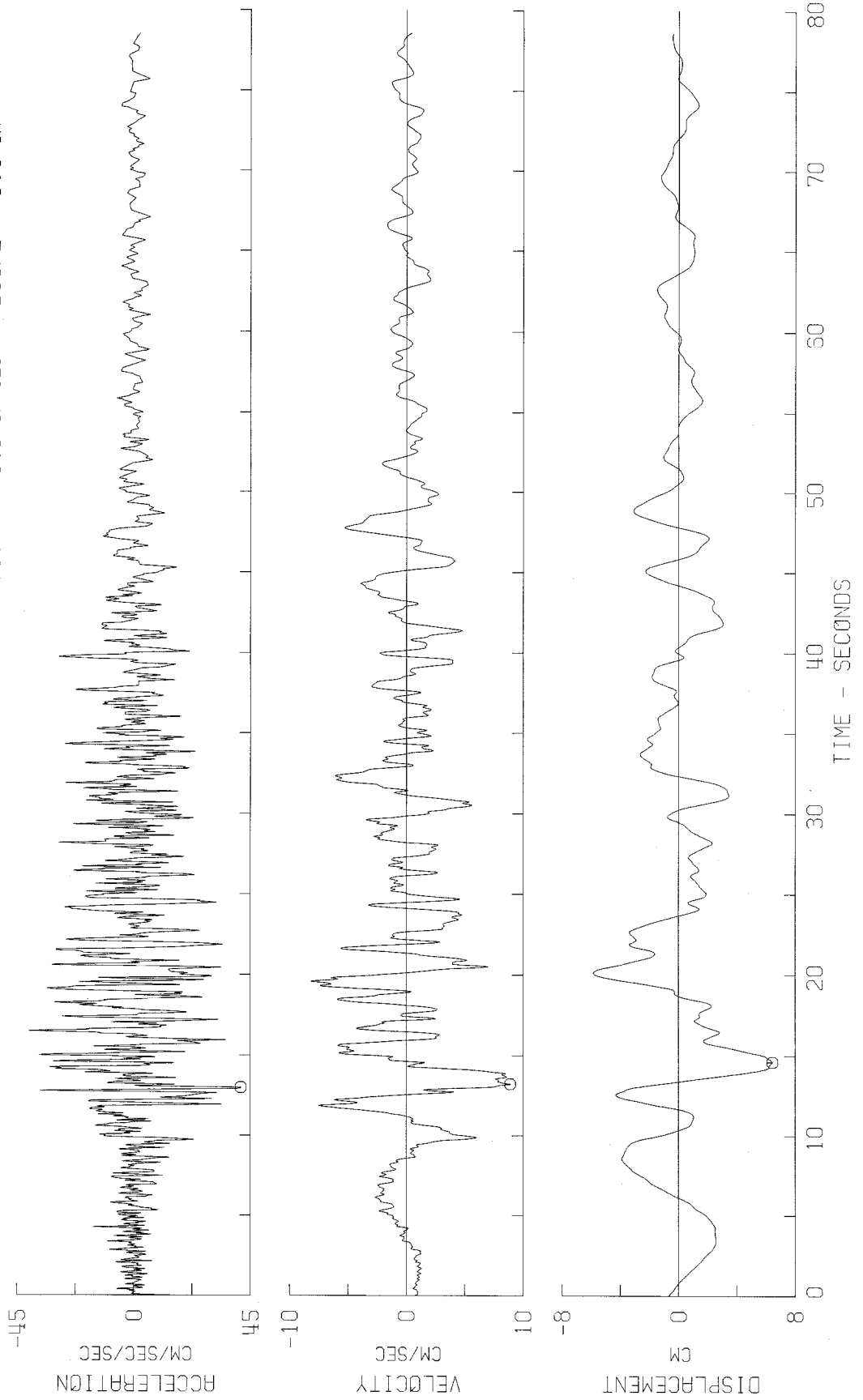
PEAK VALUES : ACCEL = -58.1 CM/SEC/SEC VELOCITY = -6.6 CM/SEC DISPL = -4.5 CM



KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT

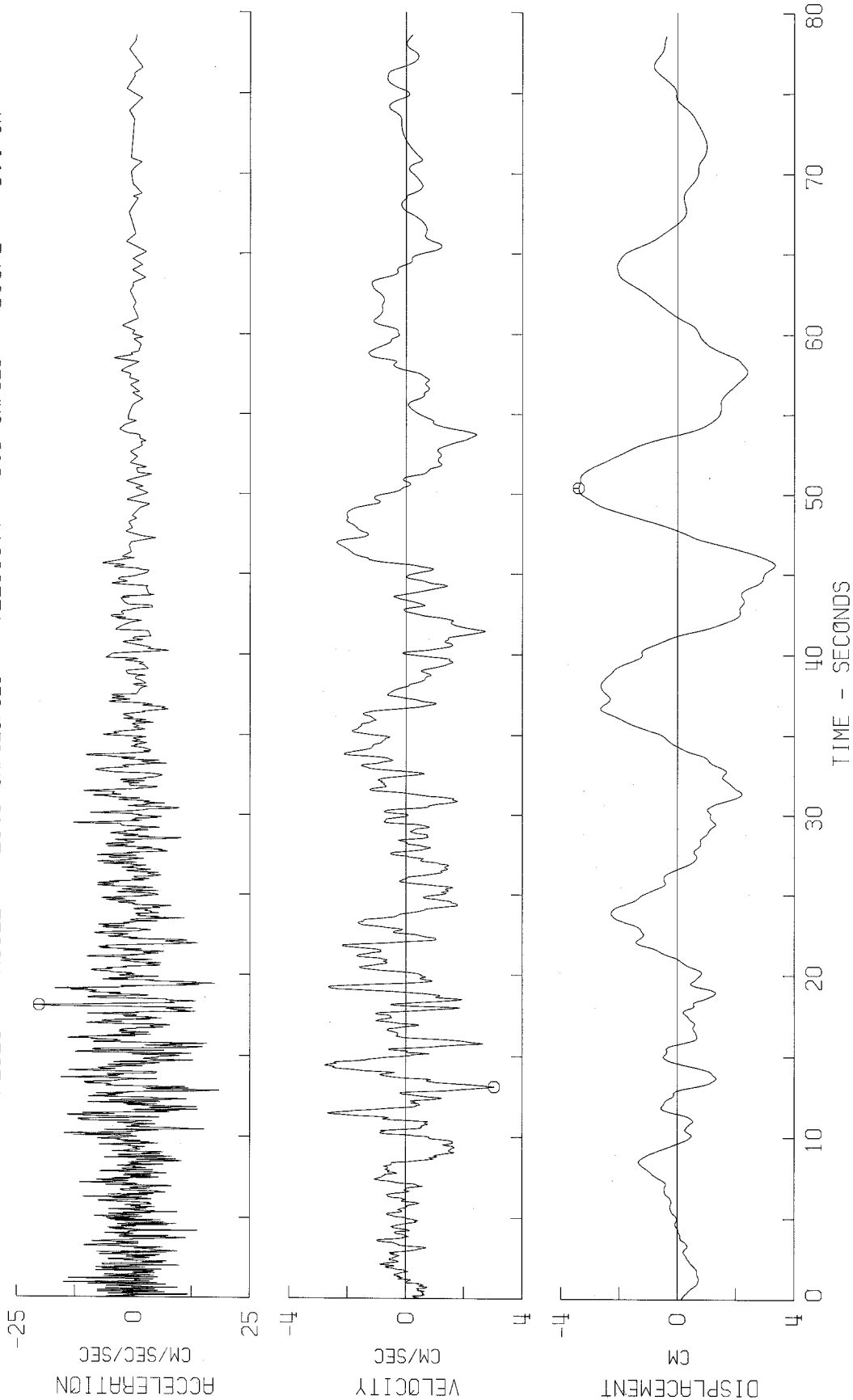
IIA007 52.006.0 HOLLYWOOD STORAGE P.E. LOT COMP N90E

PEAK VALUES : ACCEL = 41.2 CM/SEC/SEC VELOCITY = 8.9 CM/SEC DISPL = 6.4 CM



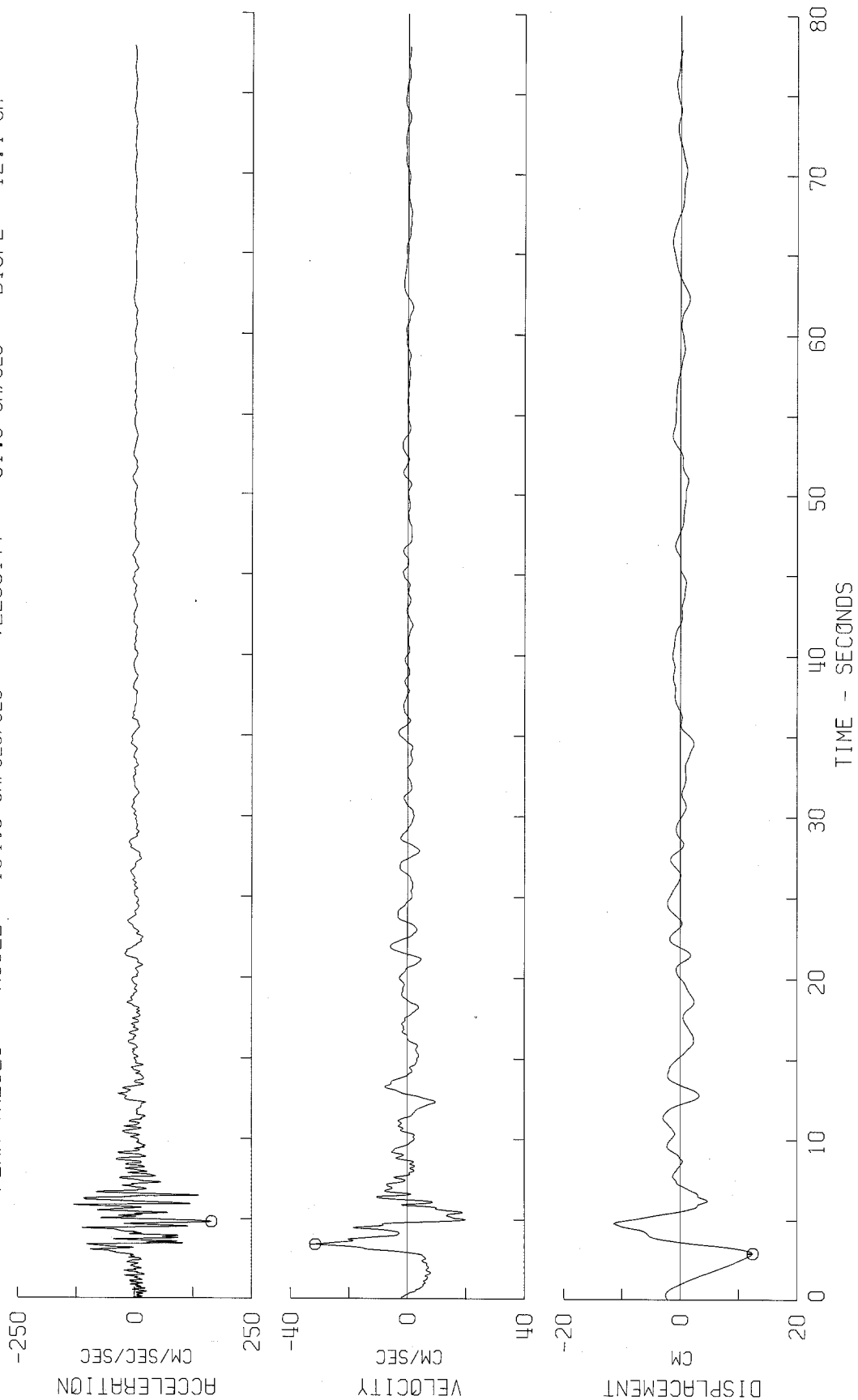
KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
IIA097 52.006.0 HOLLYWOOD STORAGE P.E. LOT COMP VERT

PEAK VALUES: ACCEL = -20.3 CM/SEC/SEC VELOCITY = 3.0 CM/SEC DISPL = -3.4 CM



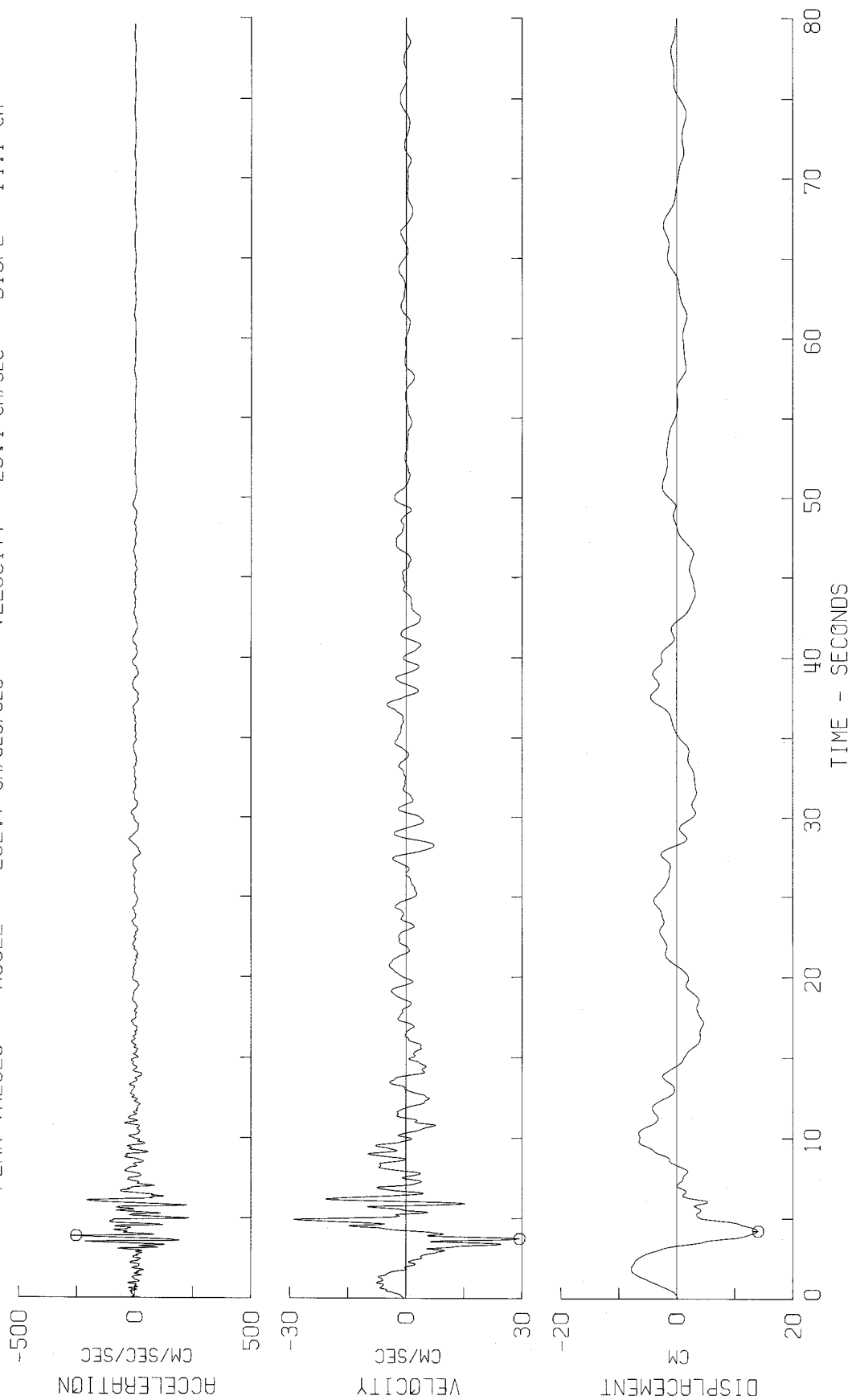
EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST
IIA008 54.003.0 EUREKA FEDERAL BLDG COMP N11W

PEAK VALUES : ACCEL = 164.5 CM/SEC/SEC VELOCITY = -31.6 CM/SEC DISPL = 12.4 CM



EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST
IIA008 54.003.0 EUREKA FEDERAL BLDG COMP N79E

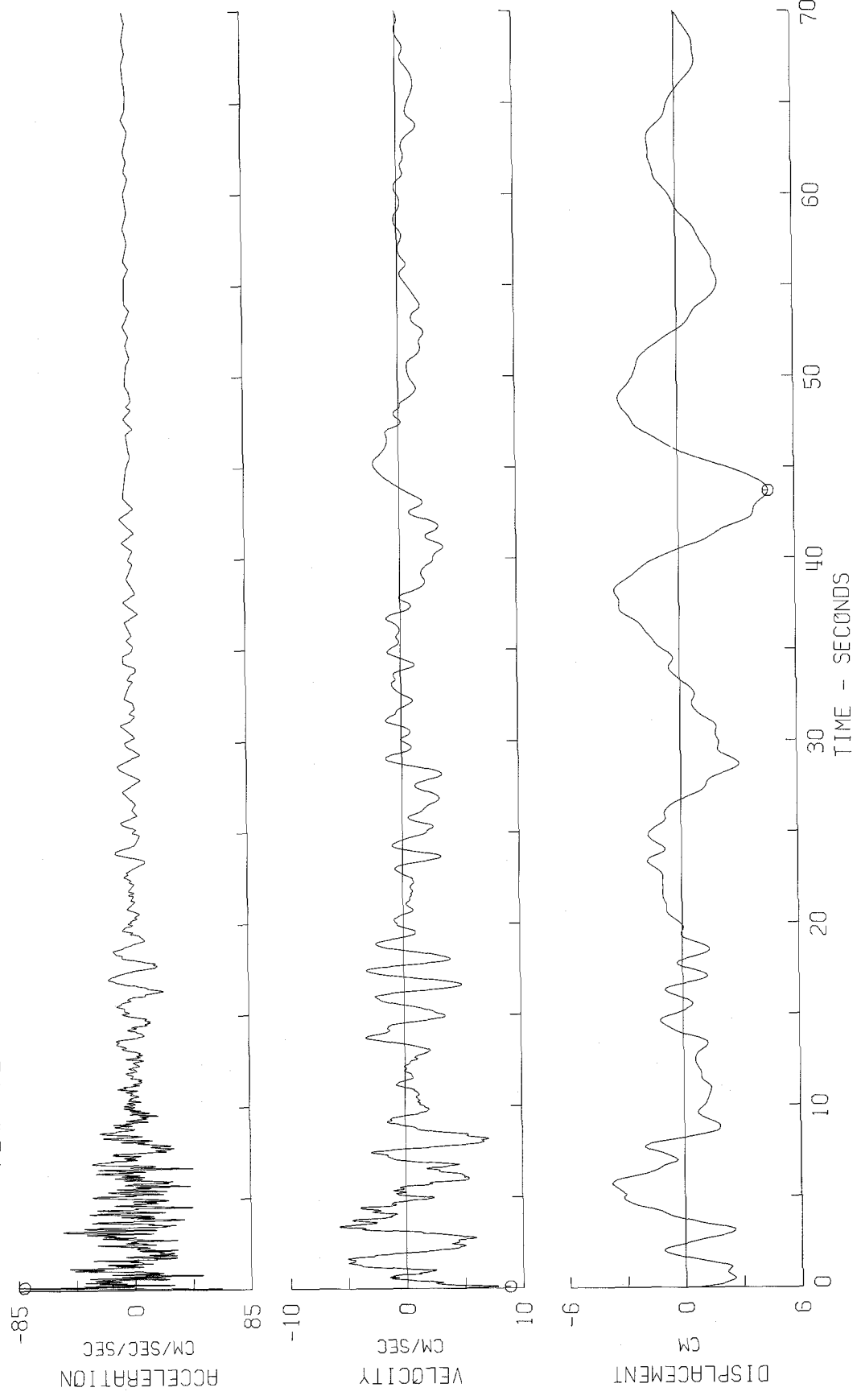
PEAK VALUES : ACCEL = -252.7 CM/SEC/SEC VELOCITY = 29.4 CM/SEC DISPL = 14.1 CM



EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST

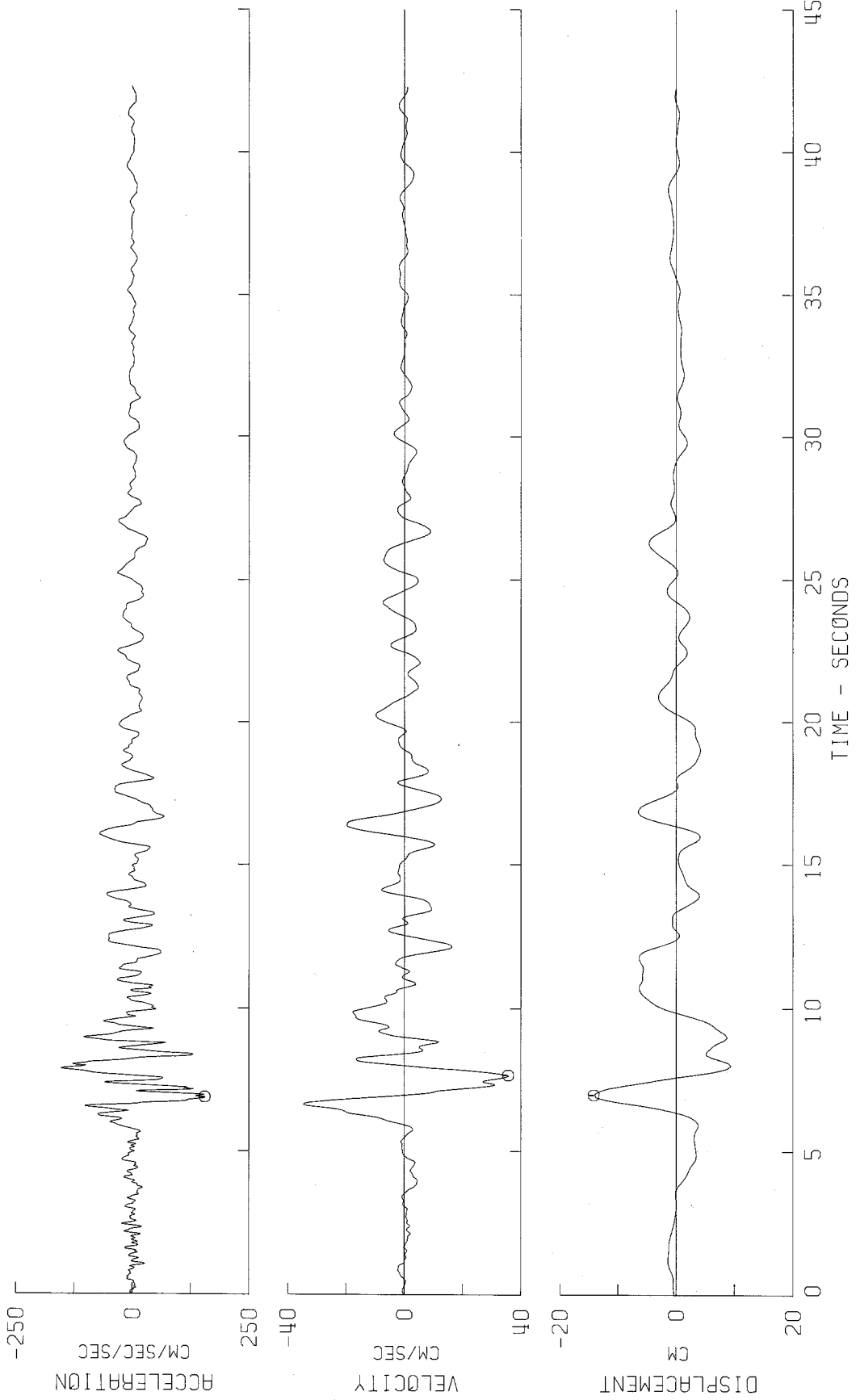
ITIA008 54.003.0 EUREKA FEDERAL BLDG COMP VERT

PEAK VALUES : ACCEL = -81.3 CM/SEC/SEC VELOCITY = 8.2 CM/SEC DISPL = 4.7 CM



EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST
IIA009 54.004.0 FERDALE CITY HALL COMP N44E

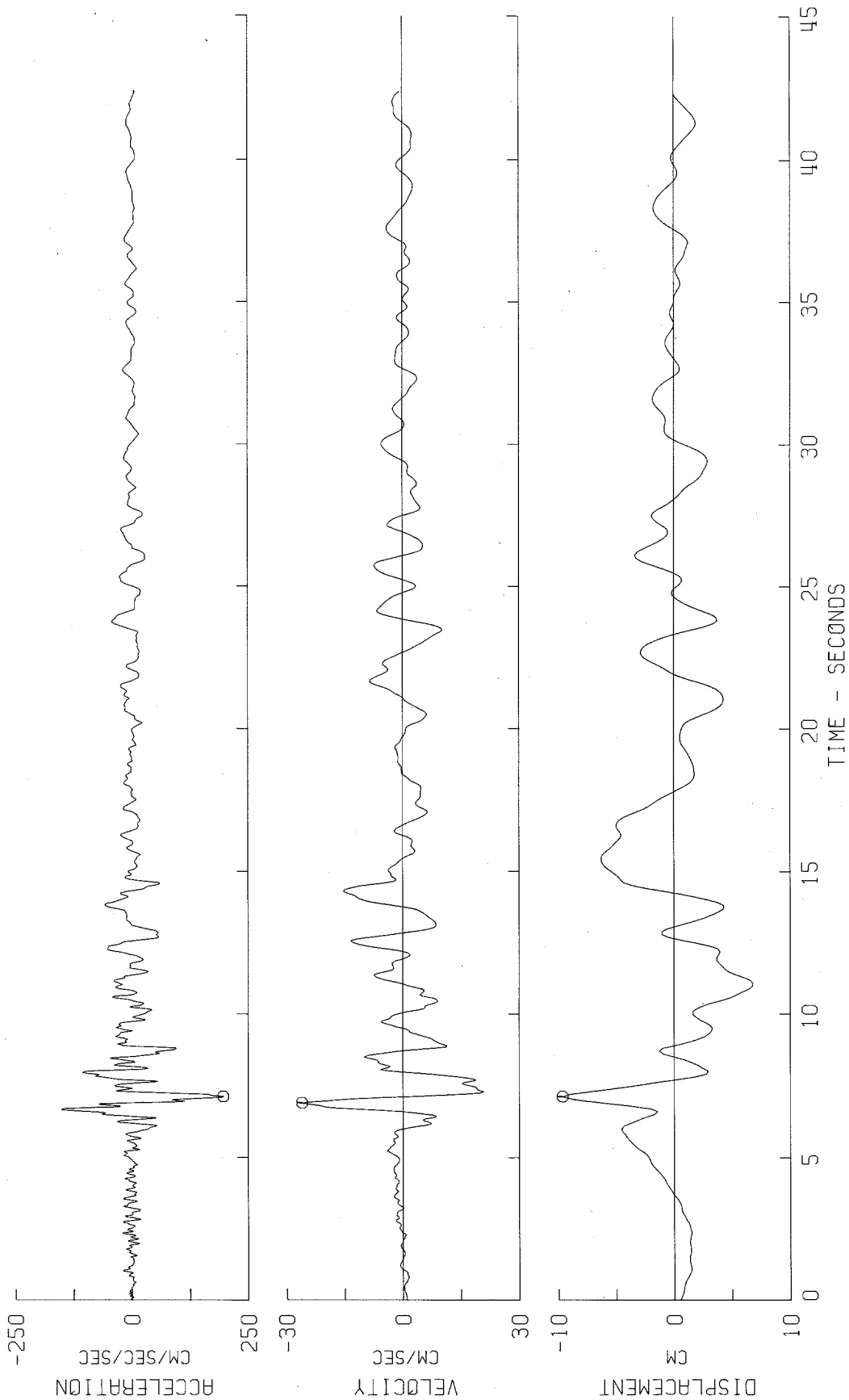
⊙ PEAK VALUES : ACCEL = 155.7 CM/SEC/SEC VELOCITY = 35.6 CM/SEC DISPL = -14.2 CM



EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST

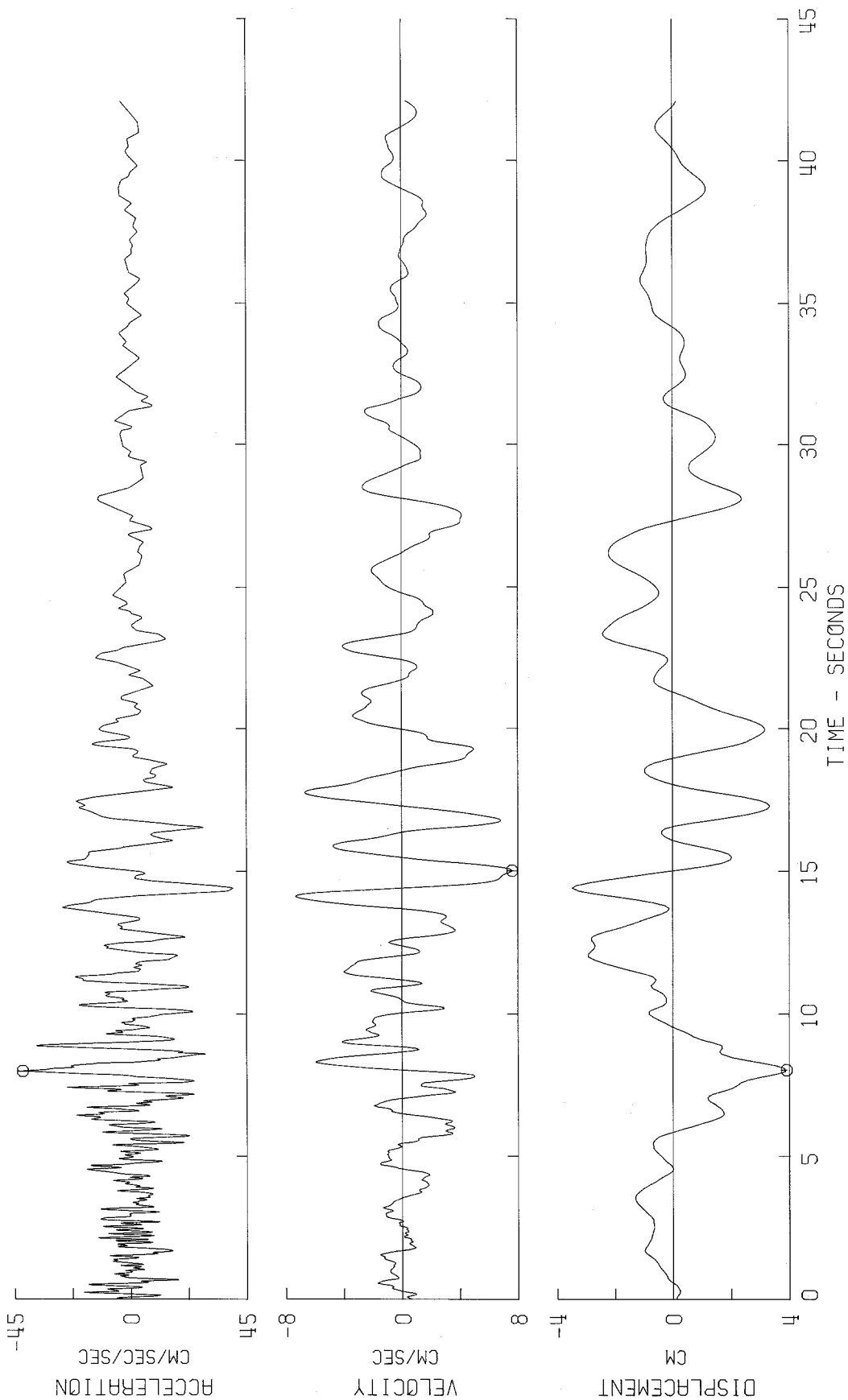
IIA009 54.004.0 FERNDALE CITY HALL COMP N46W

⊙ PEAK VALUES : ACCEL = 197.3 CM/SEC/SEC VELOCITY = -26.0 CM/SEC DISPL = -9.6 CM

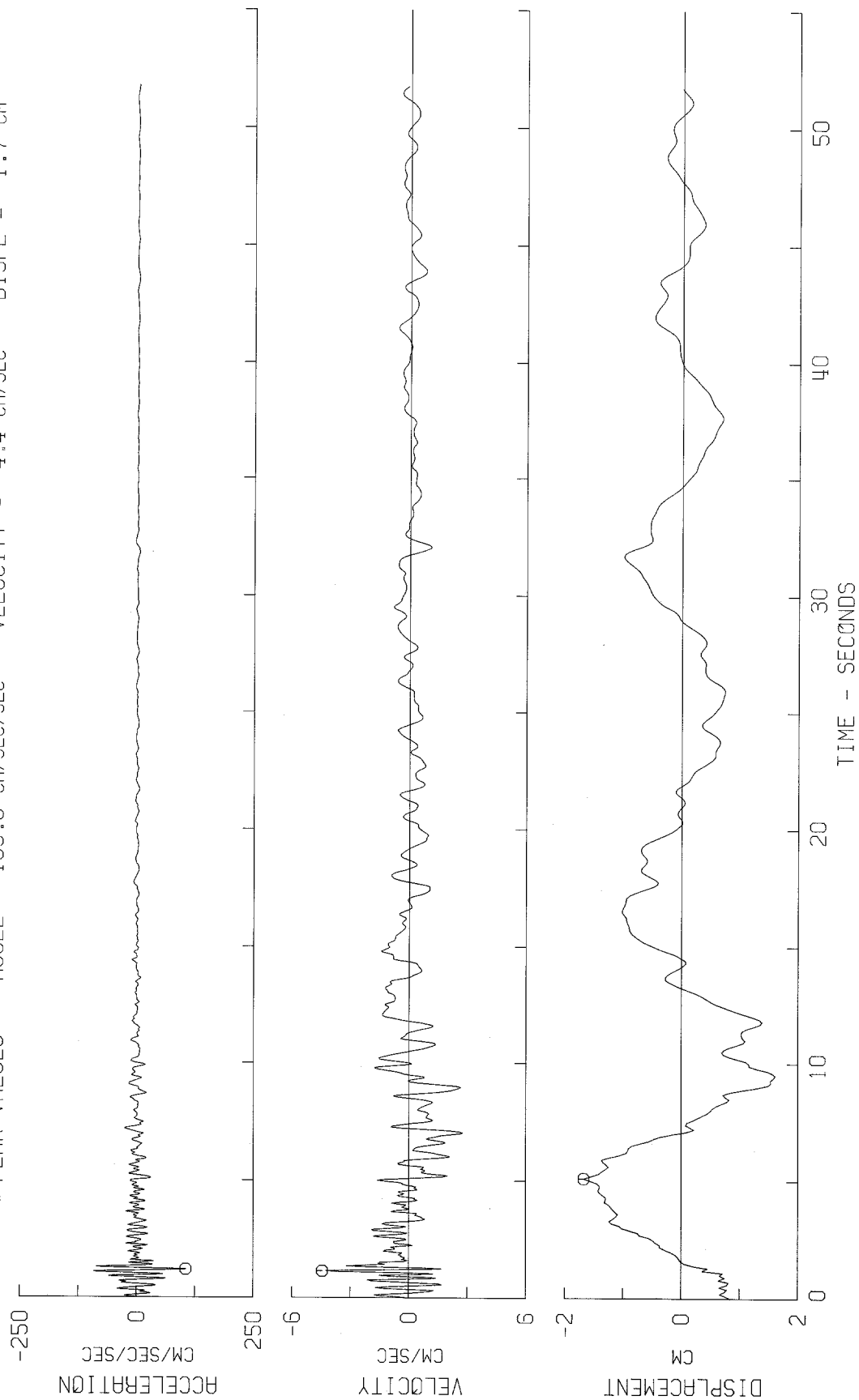


EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST IIA009 54.004.0 FERNDALE CITY HALL COMP VERT

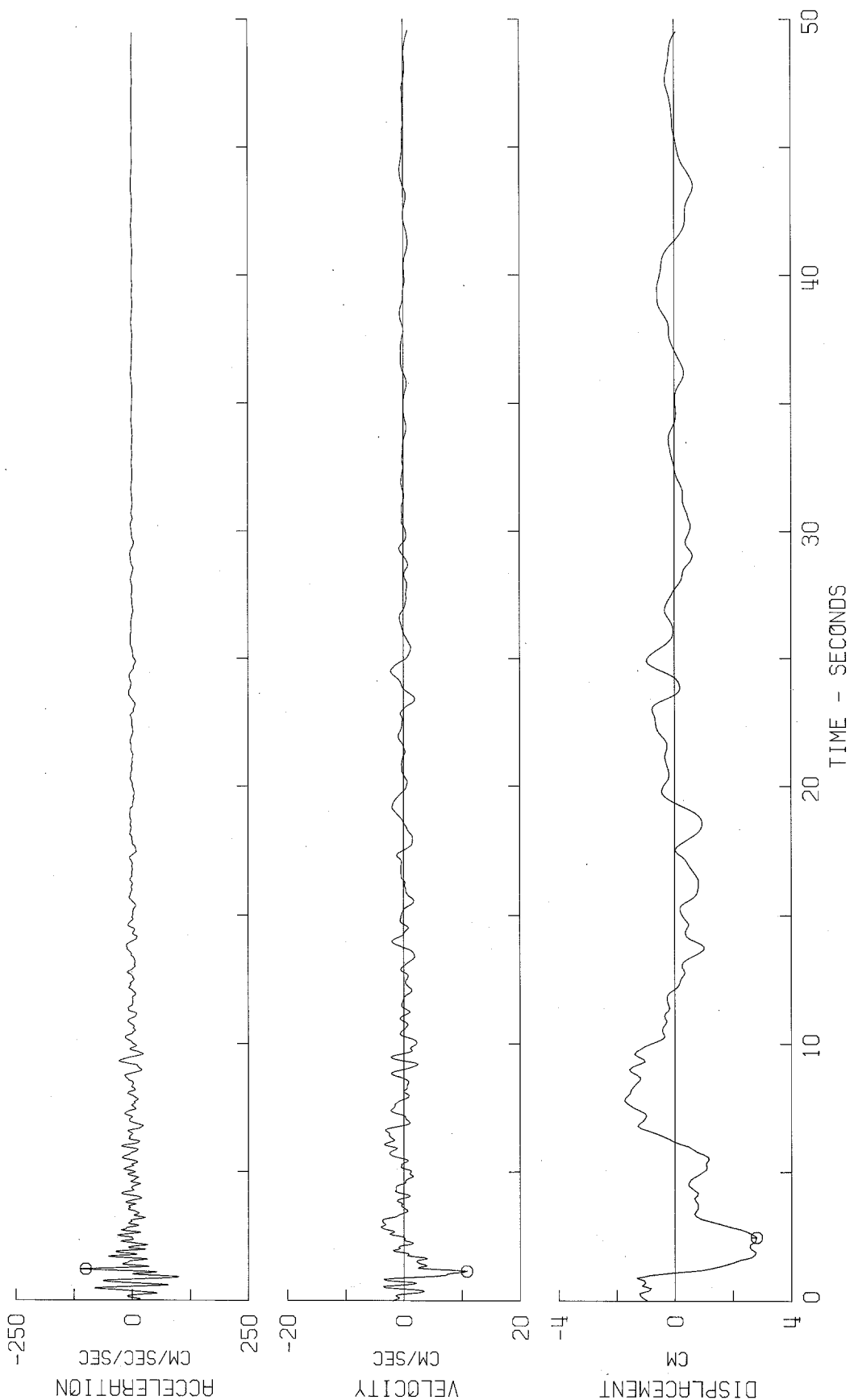
PEAK VALUES: ACCEL = -41.9 CM/SEC/SEC VELOCITY = 7.6 CM/SEC DISPL = 3.9 CM



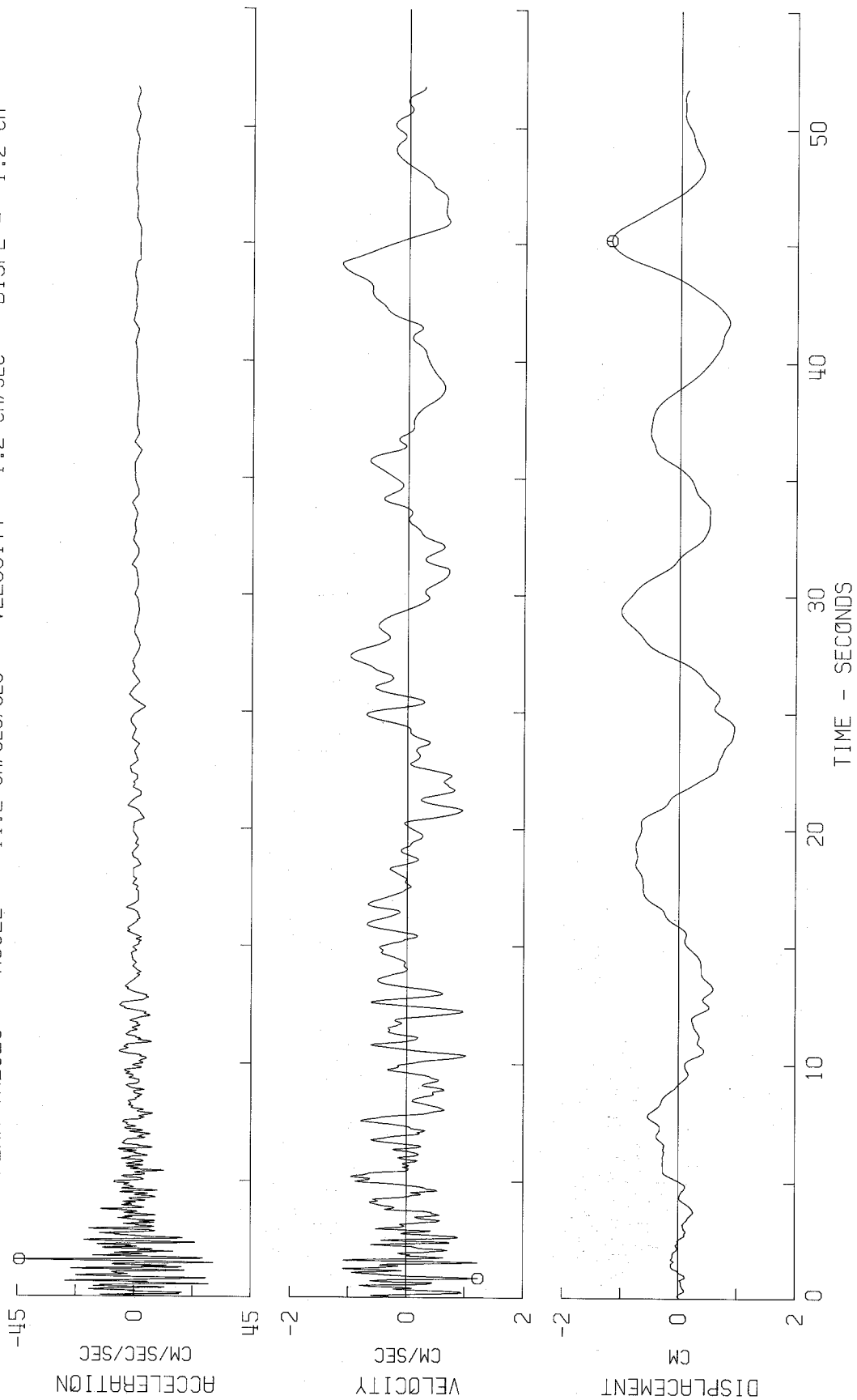
SAN JOSE EARTHQUAKE SEPT 4, 1955 - 1801 PST
 IIA010 55.001.0 SAN JOSE BANK OF AMERICA BASEMENT COMP N59E
 PEAK VALUES : ACCEL = 105.8 CM/SEC/SEC VELOCITY = -4.4 CM/SEC DISPL = -1.7 CM



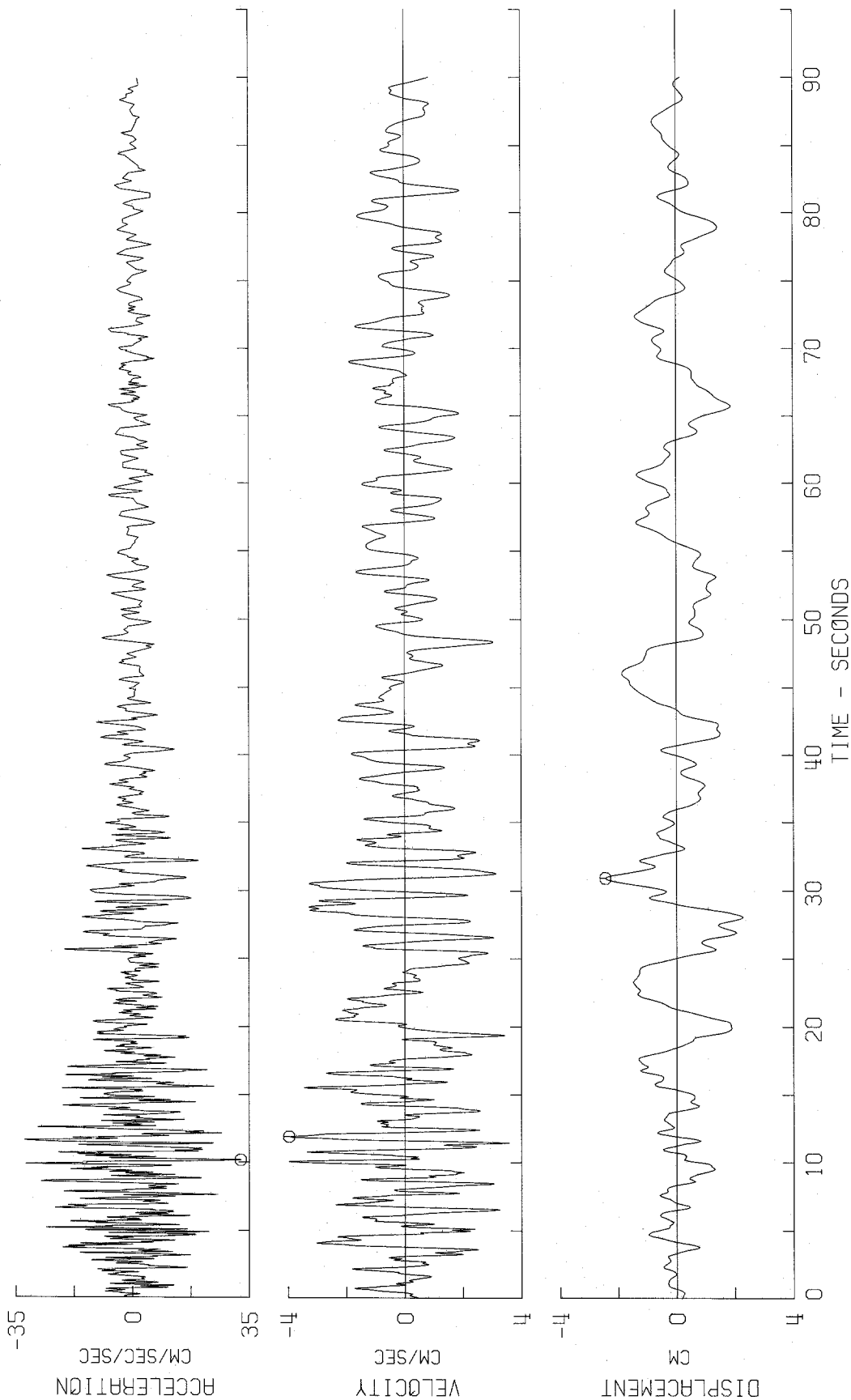
SAN JOSE EARTHQUAKE SEPT 4, 1955 - 1801 PST
 IIA010 55.001.0 SAN JOSE BANK OF AMERICA BASEMENT COMP N31W
 ○ PEAK VALUES : ACCEL = -100.2 CM/SEC/SEC VELOCITY = 10.8 CM/SEC DISPL = 2.8 CM



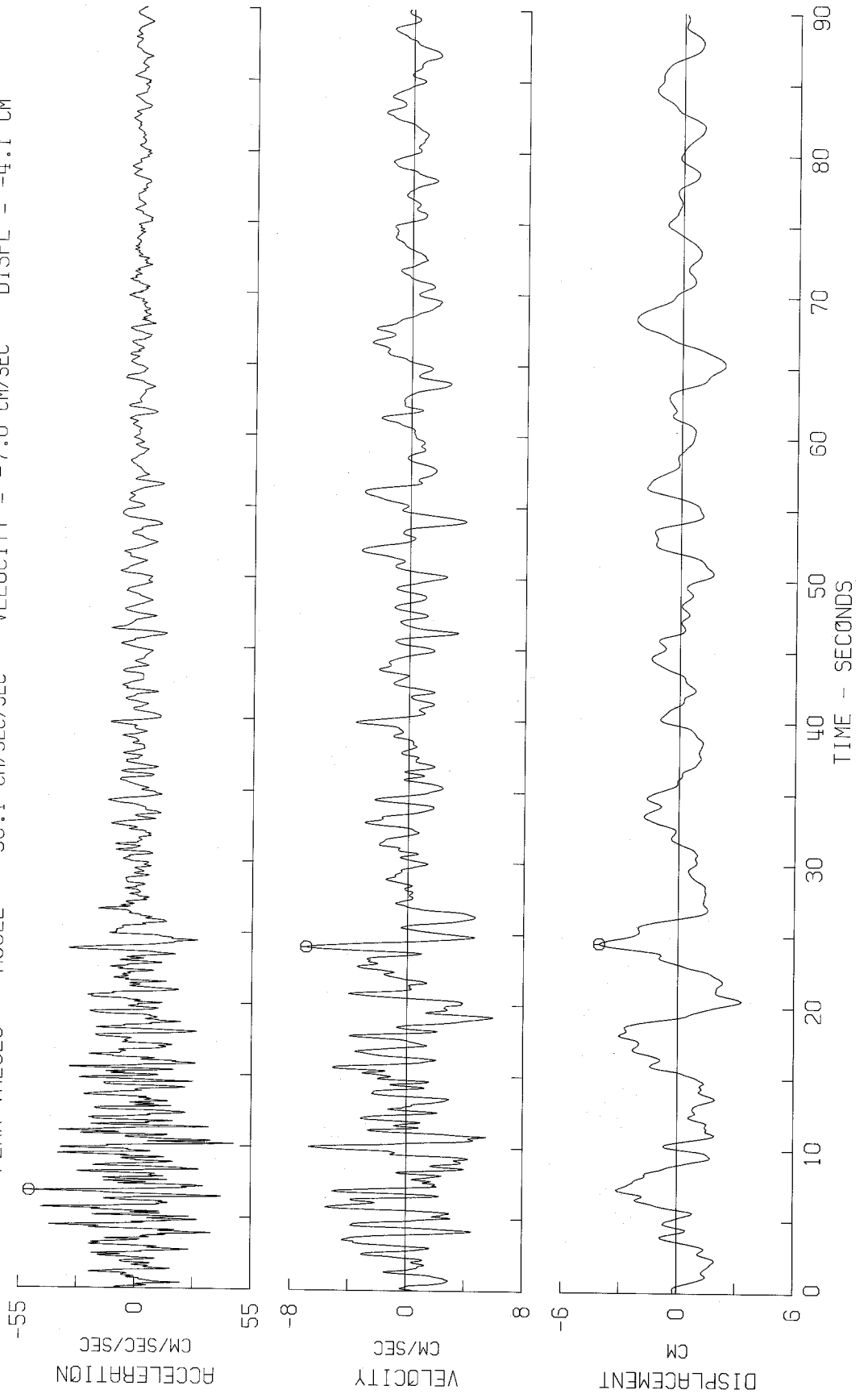
SAN JOSE EARTHQUAKE SEPT 4, 1955 - 1801 PST
IIA010 55.001.0 SAN JOSE BANK OF AMERICA BASEMENT COMP VERT
PEAK VALUES : ACCEL = -44.2 CM/SEC/SEC VELOCITY = 1.2 CM/SEC DISPL = -1.2 CM



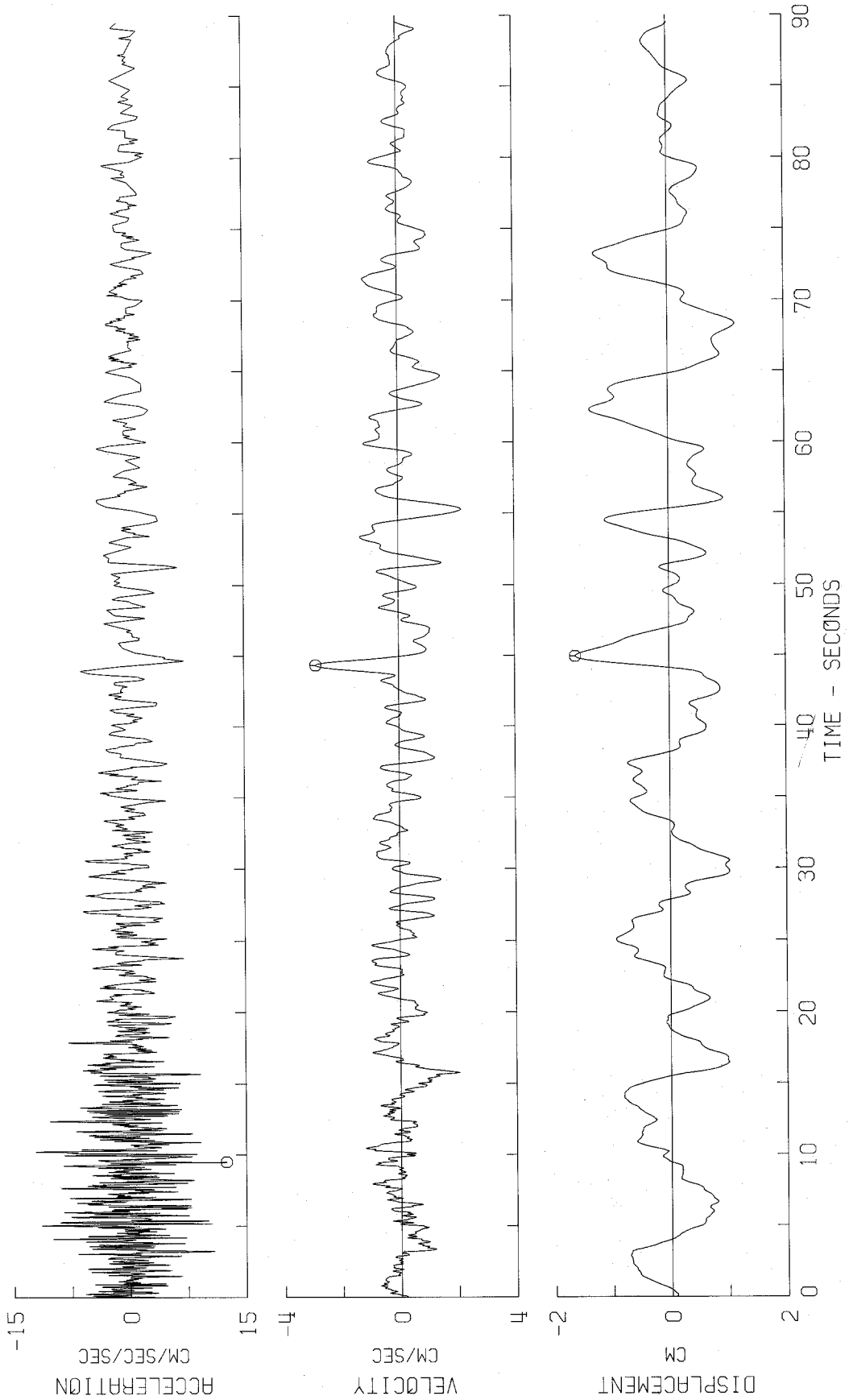
EL ALAMO, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST
 IIA011 56.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT COMP S00W
 ○ PEAK VALUES : ACCEL = 32.4 CM/SEC/SEC VELOCITY = -4.0 CM/SEC DISPL = -2.4 CM



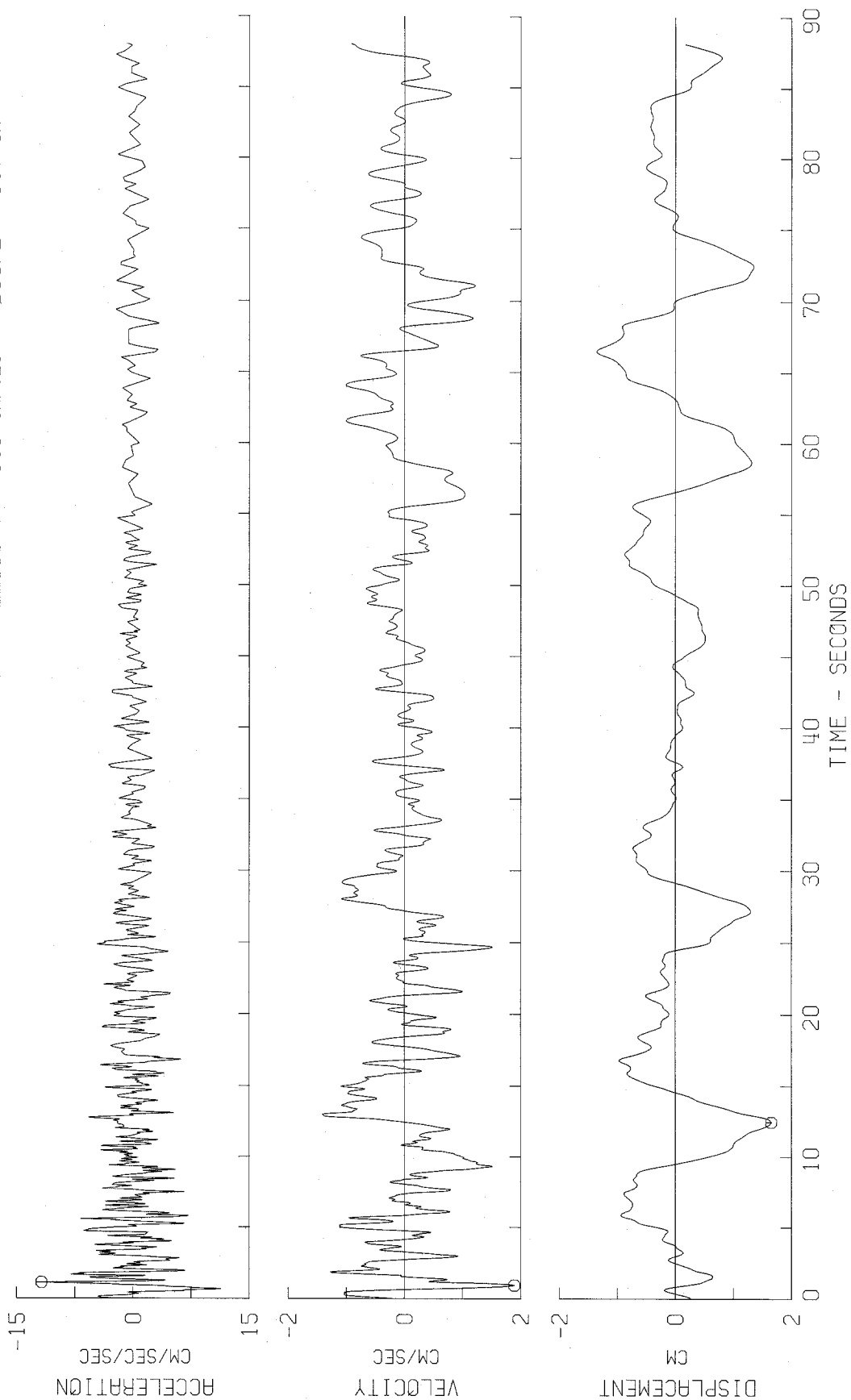
EL ALAMO, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST
IIA011 56.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT COMP S90W
⊙ PEAK VALUES : ACCEL = -50.1 CM/SEC/SEC VELOCITY = -7.0 CM/SEC DISPL = -4.1 CM



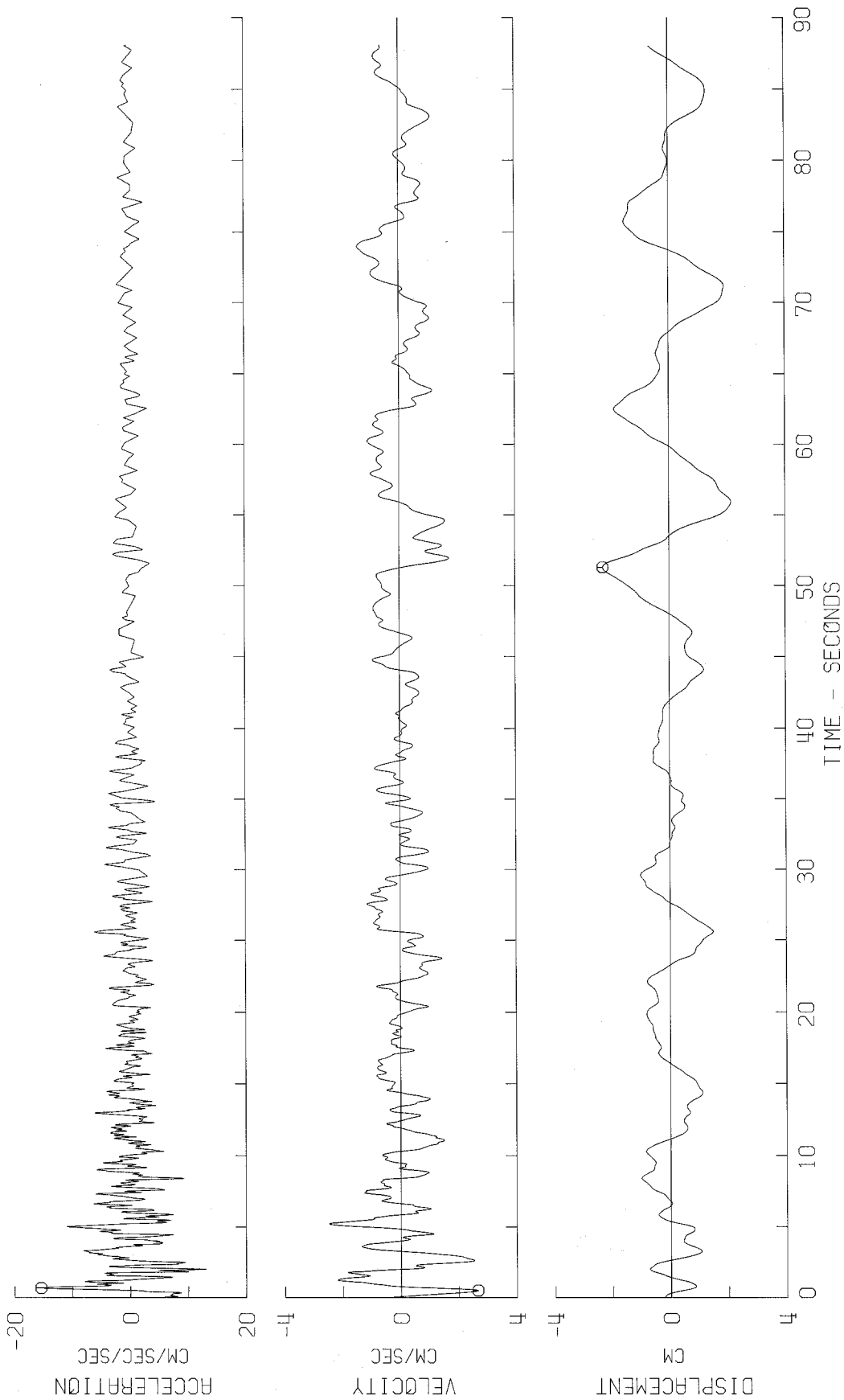
EL ALAM0, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST
IIA011 56.001.0 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT COMP VERT
0 PEAK VALUES : ACCEL = 12.4 CM/SEC/SEC VELOCITY = -2.9 CM/SEC DISPL = -1.6 CM



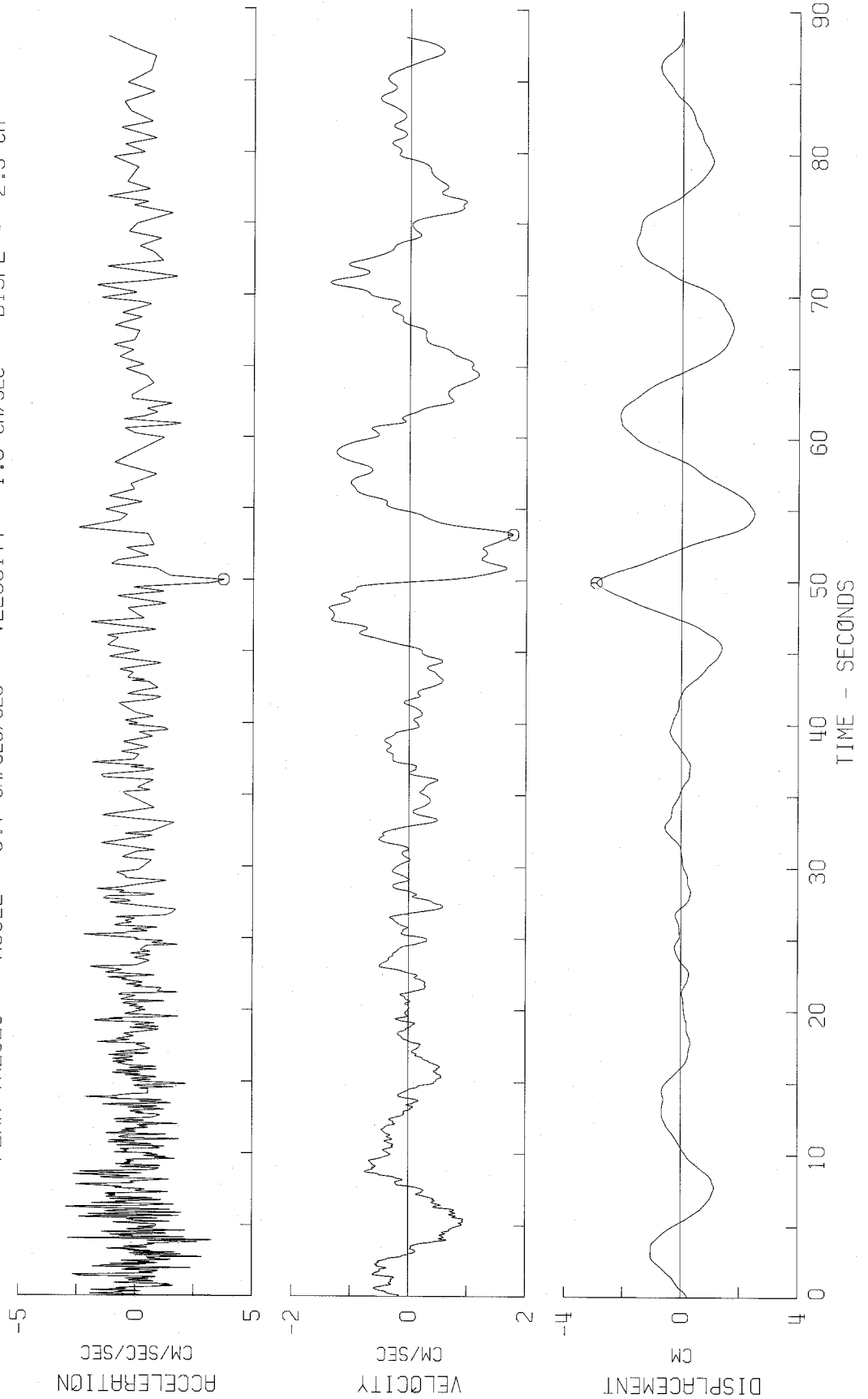
EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST
 IIA012 56.002.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP SOOW
 ◊ PEAK VALUES : ACCEL = -11.8 CM/SEC/SEC VELOCITY = 1.9 CM/SEC DISPL = 1.7 CM



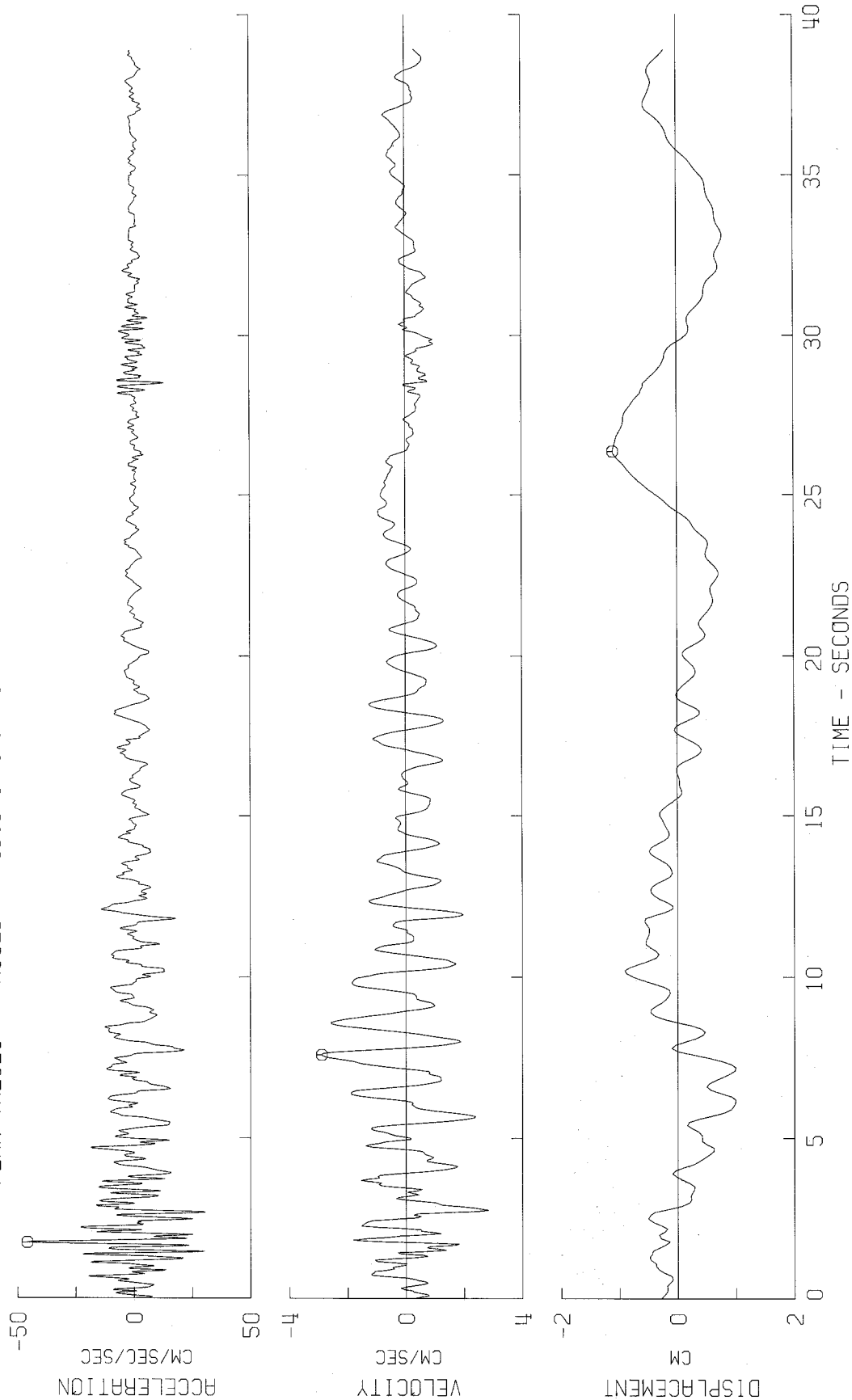
EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST
 IIA012 56.002.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S90W
 Ø PEAK VALUES : ACCEL = -15.4 CM/SEC/SEC VELOCITY = 2.7 CM/SEC DISPL = -2.3 CM



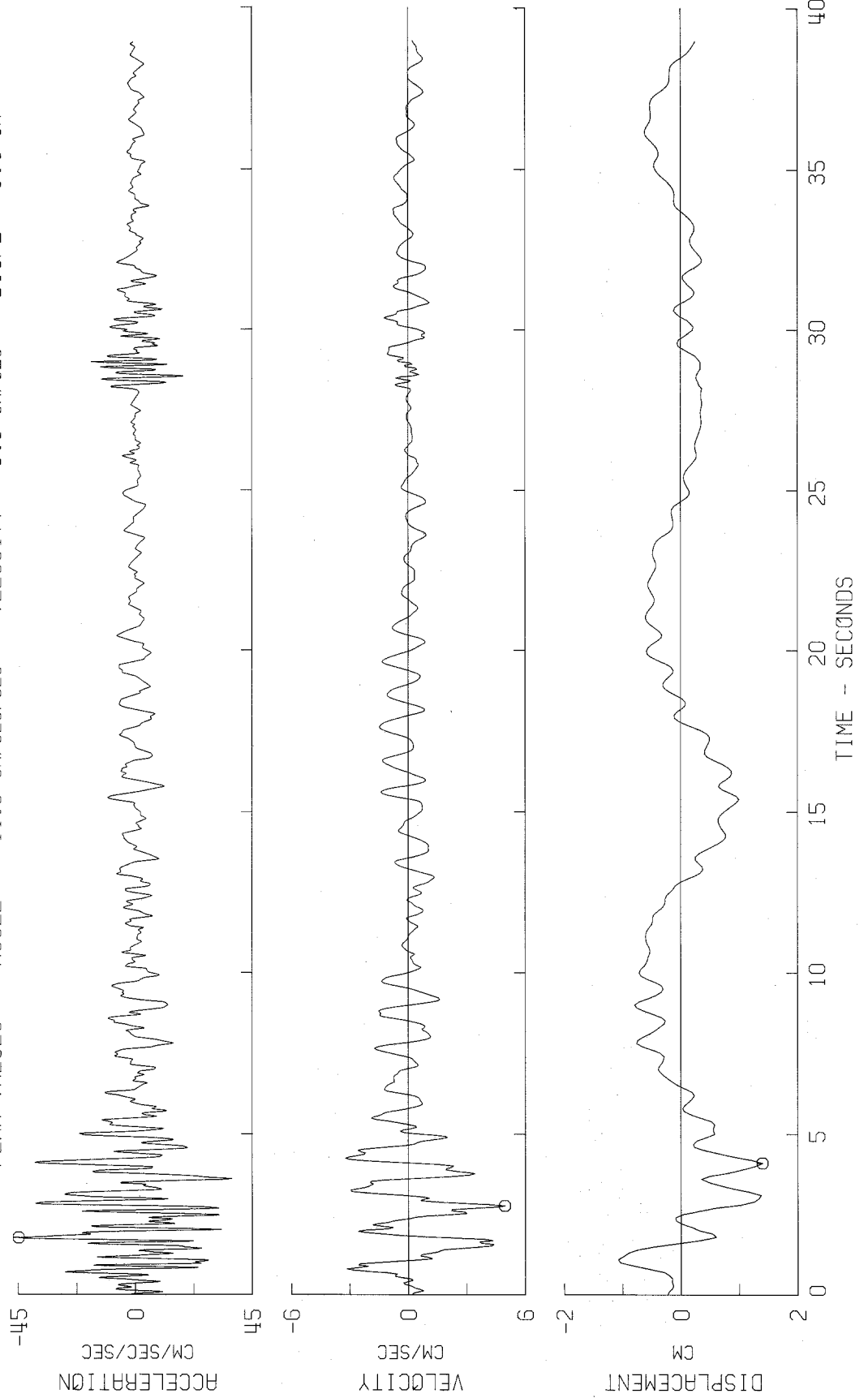
EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST
IIA012 56.002.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT
Ø PEAK VALUES : ACCEL = 3.7 CM/SEC/SEC VELOCITY = 1.8 CM/SEC DISPL = -2.9 CM



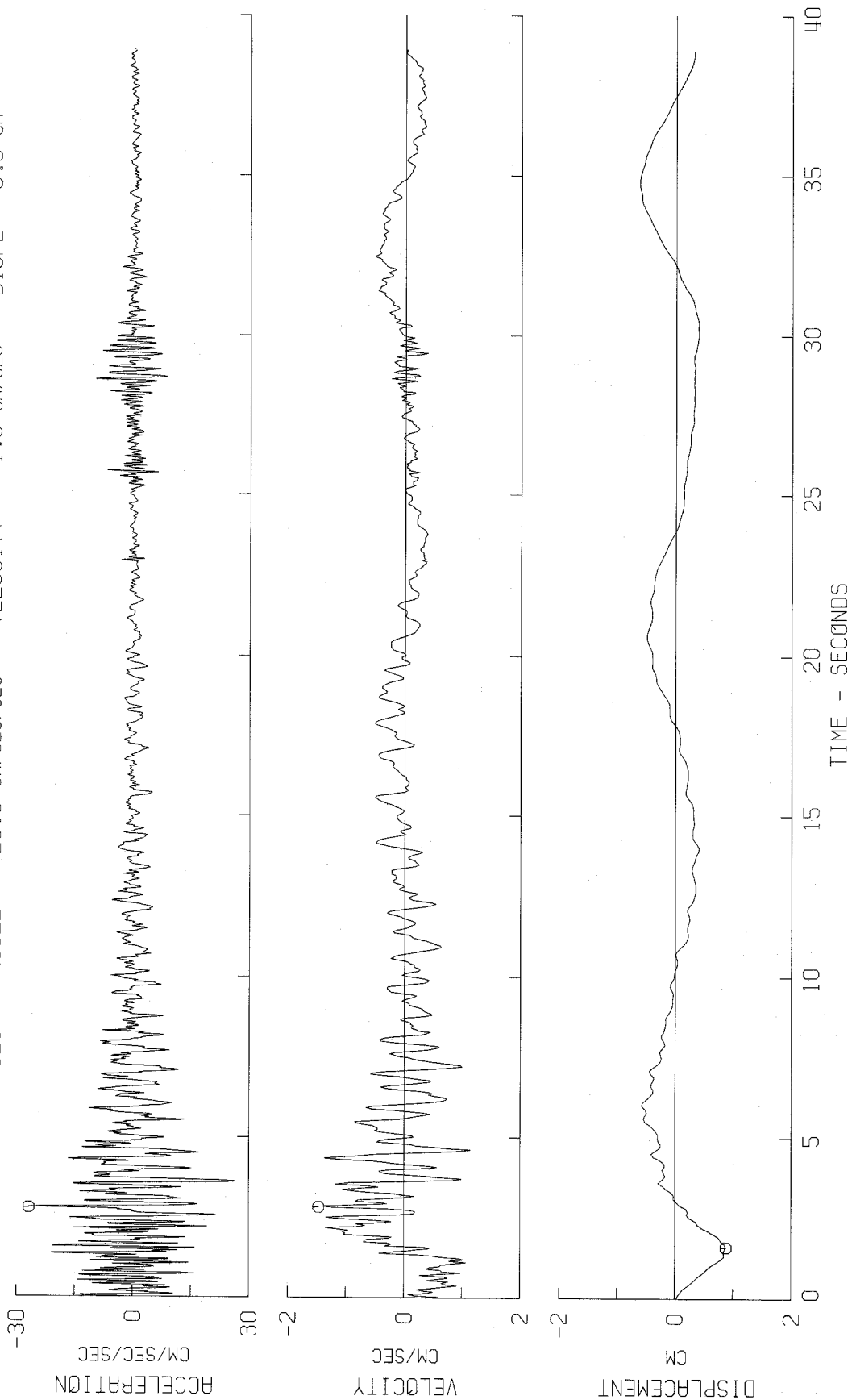
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA013 57.002.0 SAN FRANCISCO SOUTHERN PACIFIC BUILDING BASEMENT COMP N45E
PEAK VALUES: ACCEL = -45.9 CM/SEC/SEC VELOCITY = -2.9 CM/SEC DISPL = -1.1 CM



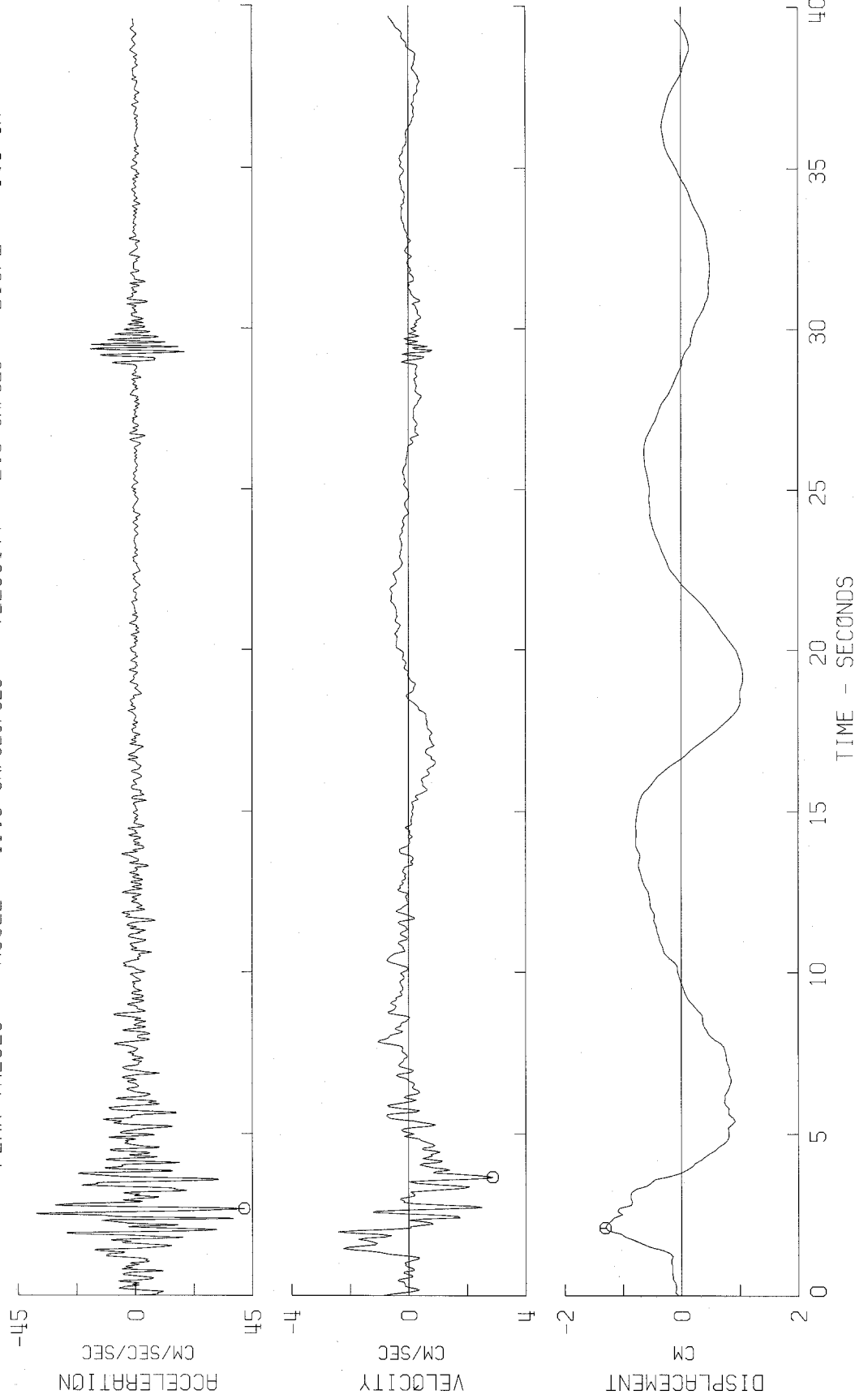
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA013 57.002.0 SAN FRANCISCO SOUTHERN PACIFIC BUILDING BASEMENT COMP N45W
PEAK VALUES: ACCEL = -44.9 CM/SEC/SEC VELOCITY = 5.0 CM/SEC DISPL = 1.4 CM



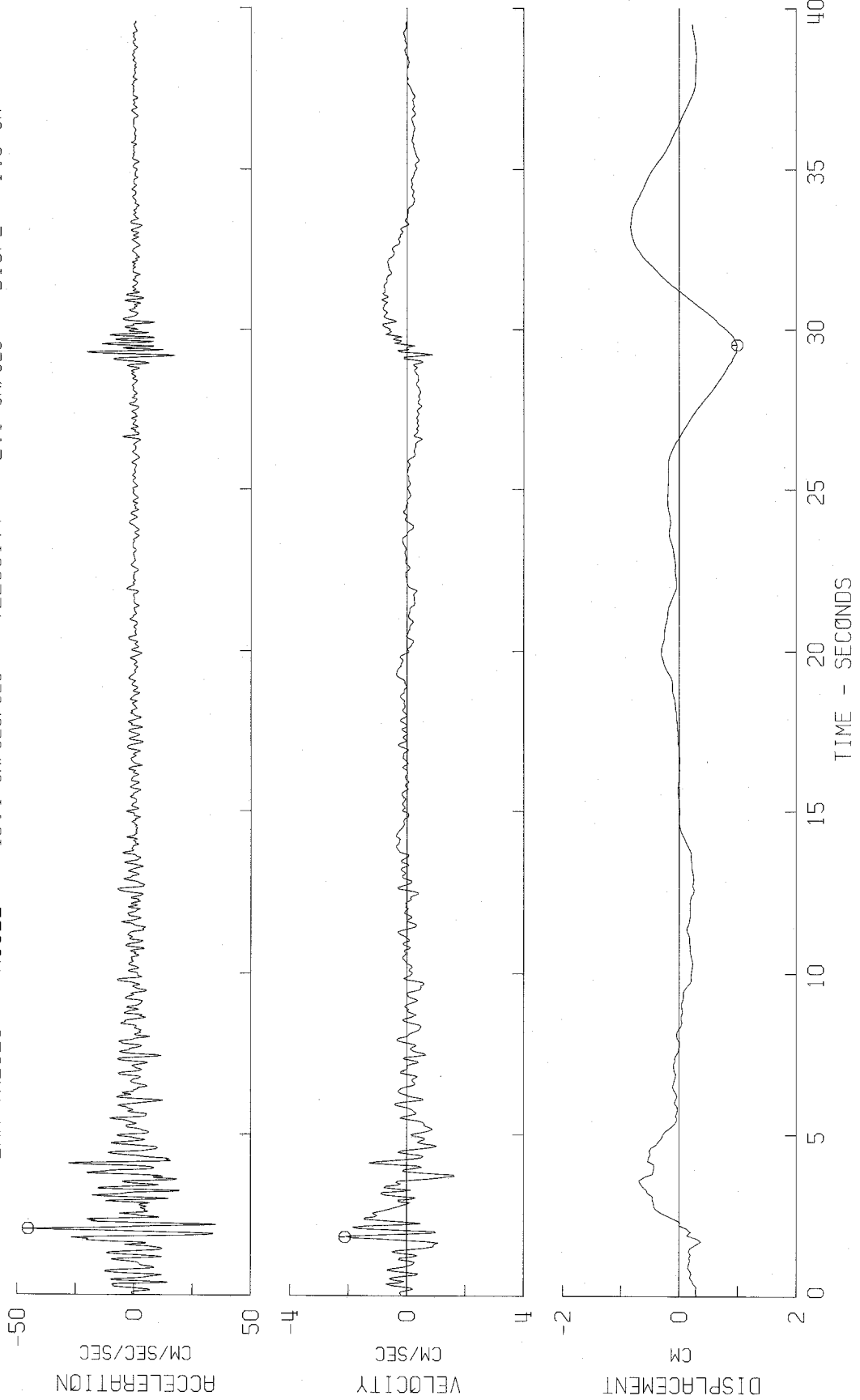
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA013 57.002.0 SAN FRANCISCO SOUTHERN PACIFIC BUILDING BASEMENT COMP VERT
PEAK VALUES: ACCEL = -26.8 CM/SEC/SEC VELOCITY = -1.5 CM/SEC DISPL = 0.9 CM



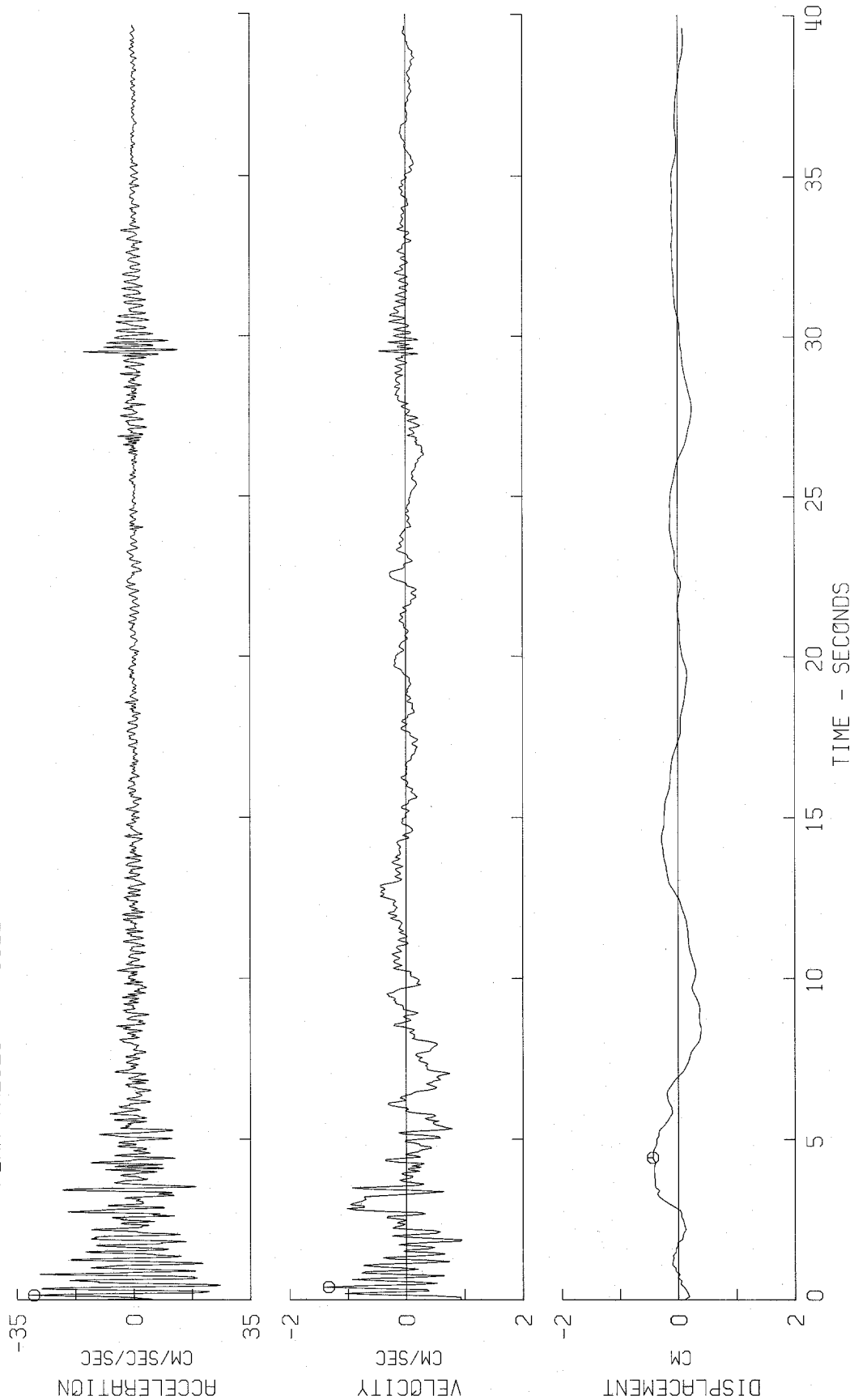
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA014 57.003.0 SAN FRANCISCO ALEXANDER BLDG BASEMENT COMP NO9W
PEAK VALUES : ACCEL = 41.8 CM/SEC/SEC VELOCITY = 2.9 CM/SEC DISPL = -1.3 CM



SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA014 57.003.0 SAN FRANCISCO ALEXANDER BLDG BASEMENT COMP N81E
⊙ PEAK VALUES : ACCEL = -45.4 CM/SEC/SEC VELOCITY = -2.1 CM/SEC DISPL = 1.0 CM

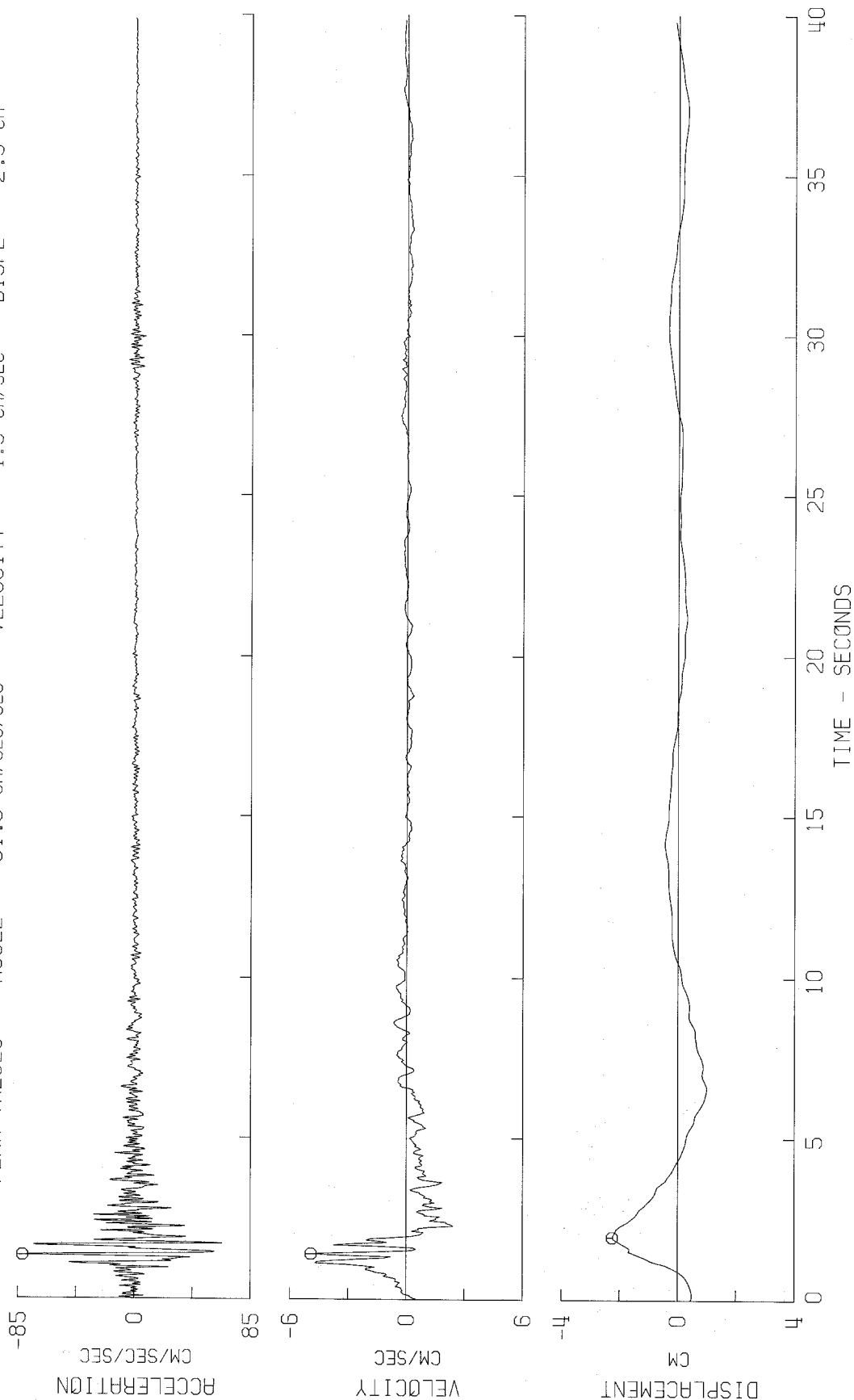


SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA014 57.003.0 SAN FRANCISCO ALEXANDER BLDG BASEMENT COMP VERT
PEAK VALUES : ACCEL = -30.0 CM/SEC/SEC VELOCITY = -1.3 CM/SEC DISPL = -0.4 CM



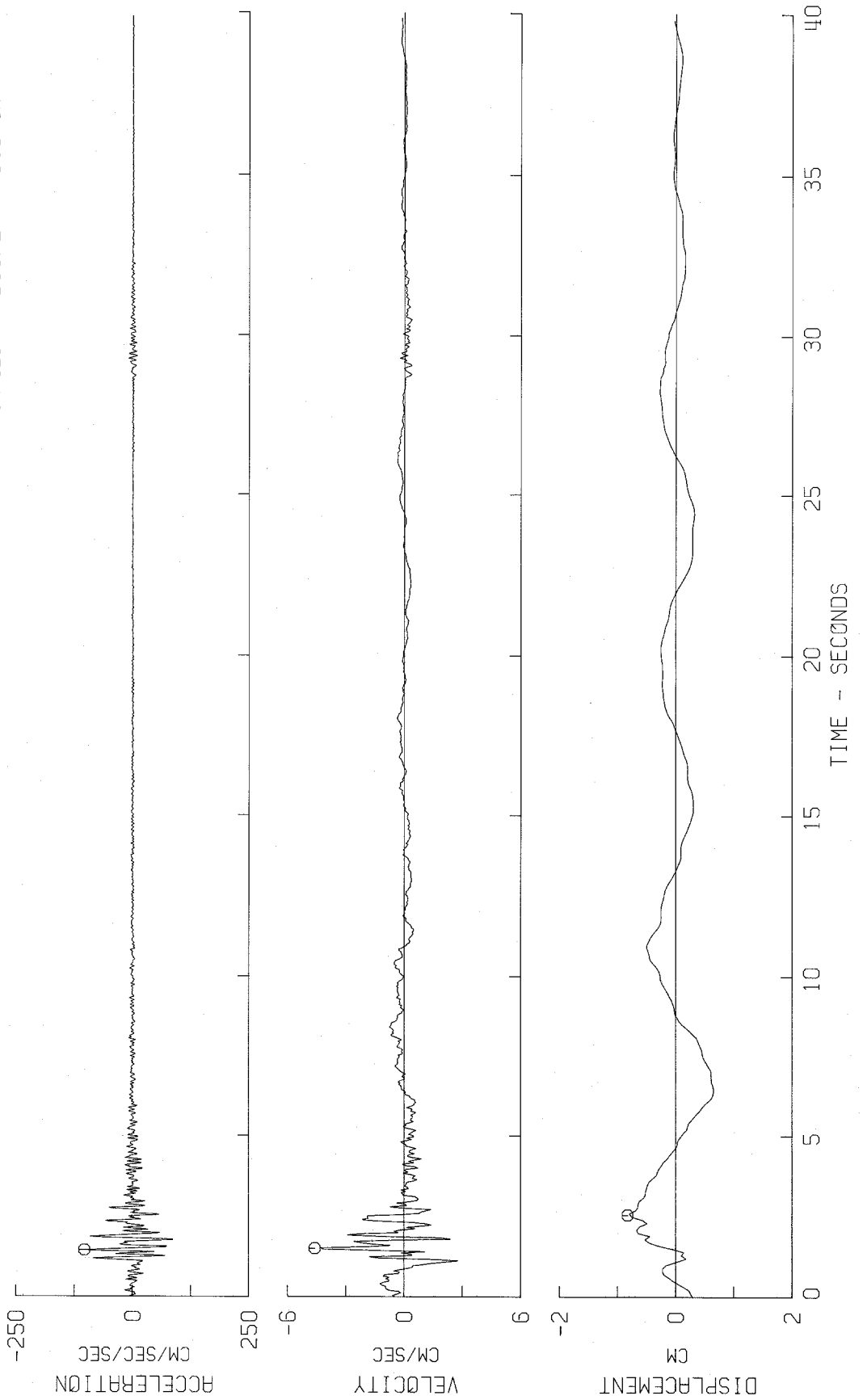
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA015 57.006.0 SAN FRANCISCO GOLDEN GATE PARK COMP N10E

⊙ PEAK VALUES : ACCEL = -81.8 CM/SEC/SEC VELOCITY = -4.9 CM/SEC DISPL = -2.3 CM

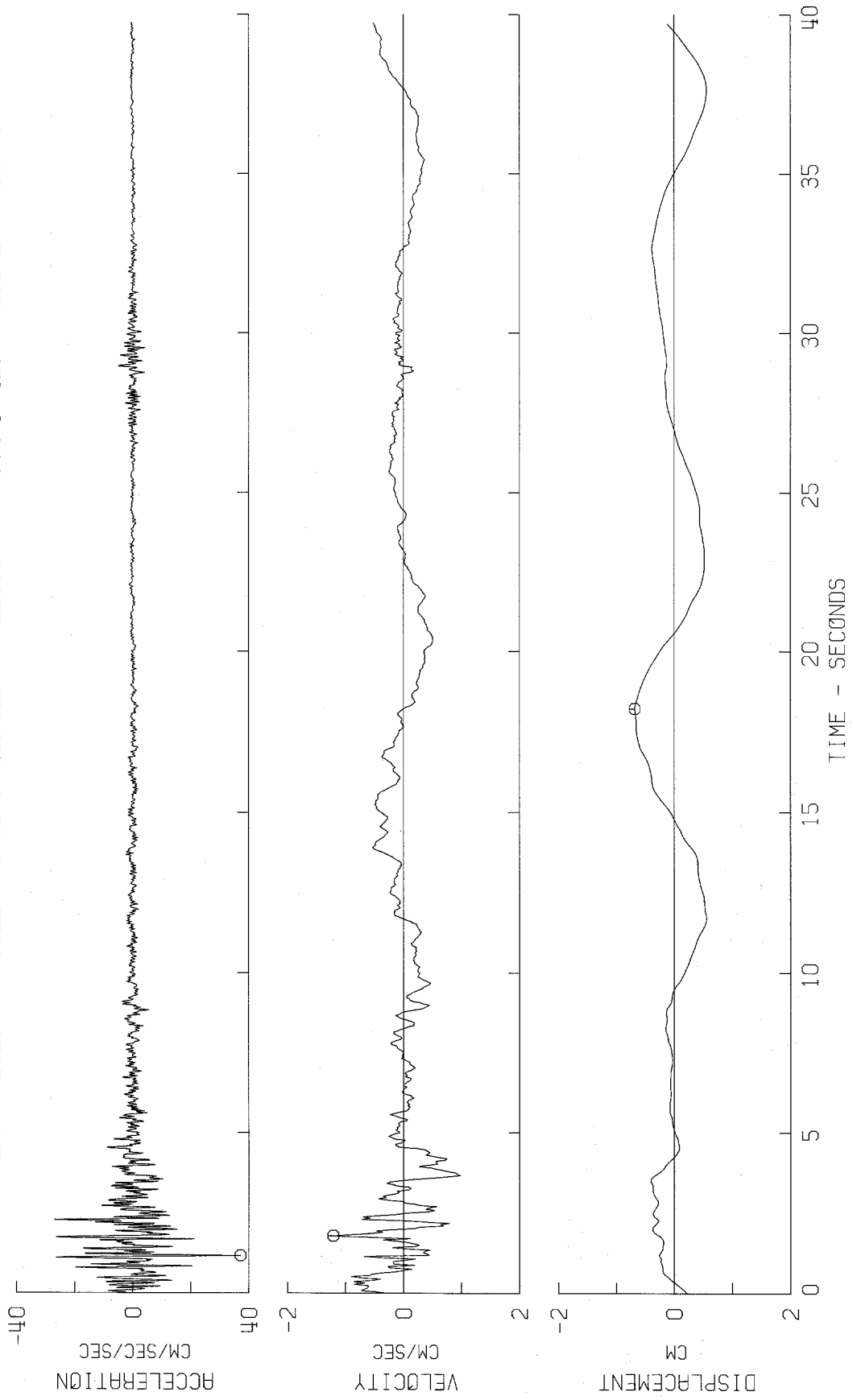


SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA015 57.006.0 SAN FRANCISCO GOLDEN GATE PARK COMP S80E

⊙ PEAK VALUES : ACCEL = -102.8 CM/SEC/SEC VELOCITY = -4.6 CM/SEC DISPL = -0.8 CM



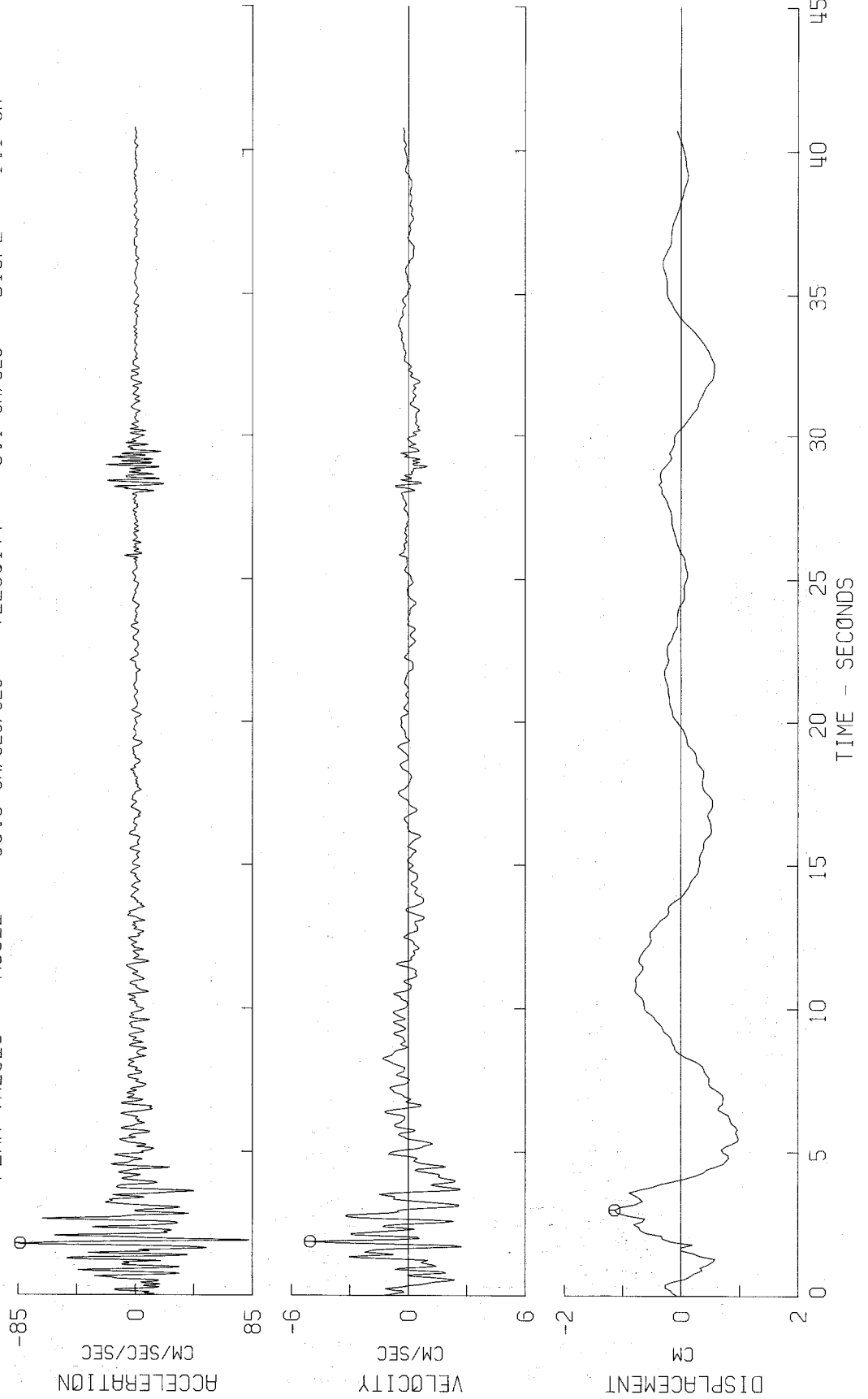
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA015 57.006.0 SAN FRANCISCO GOLDEN GATE PARK COMP VERT
PEAK VALUES : ACCEL = 37.2 CM/SEC/SEC VELOCITY = -1.2 CM/SEC DISPL = -0.7 CM



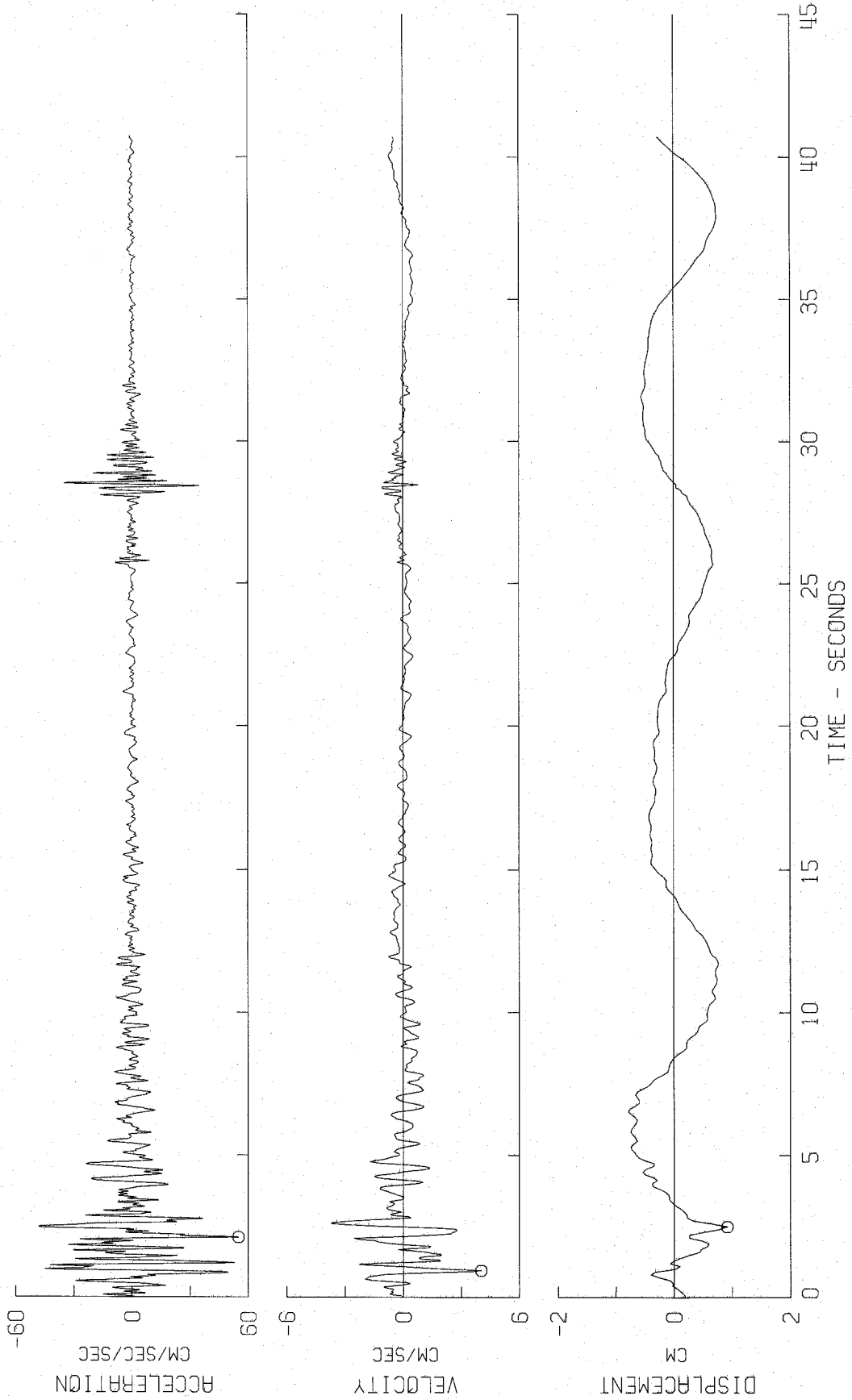
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST

IIA016 57.007.0 SAN FRANCISCO STATE BLDG BASEMENT COMP S09E

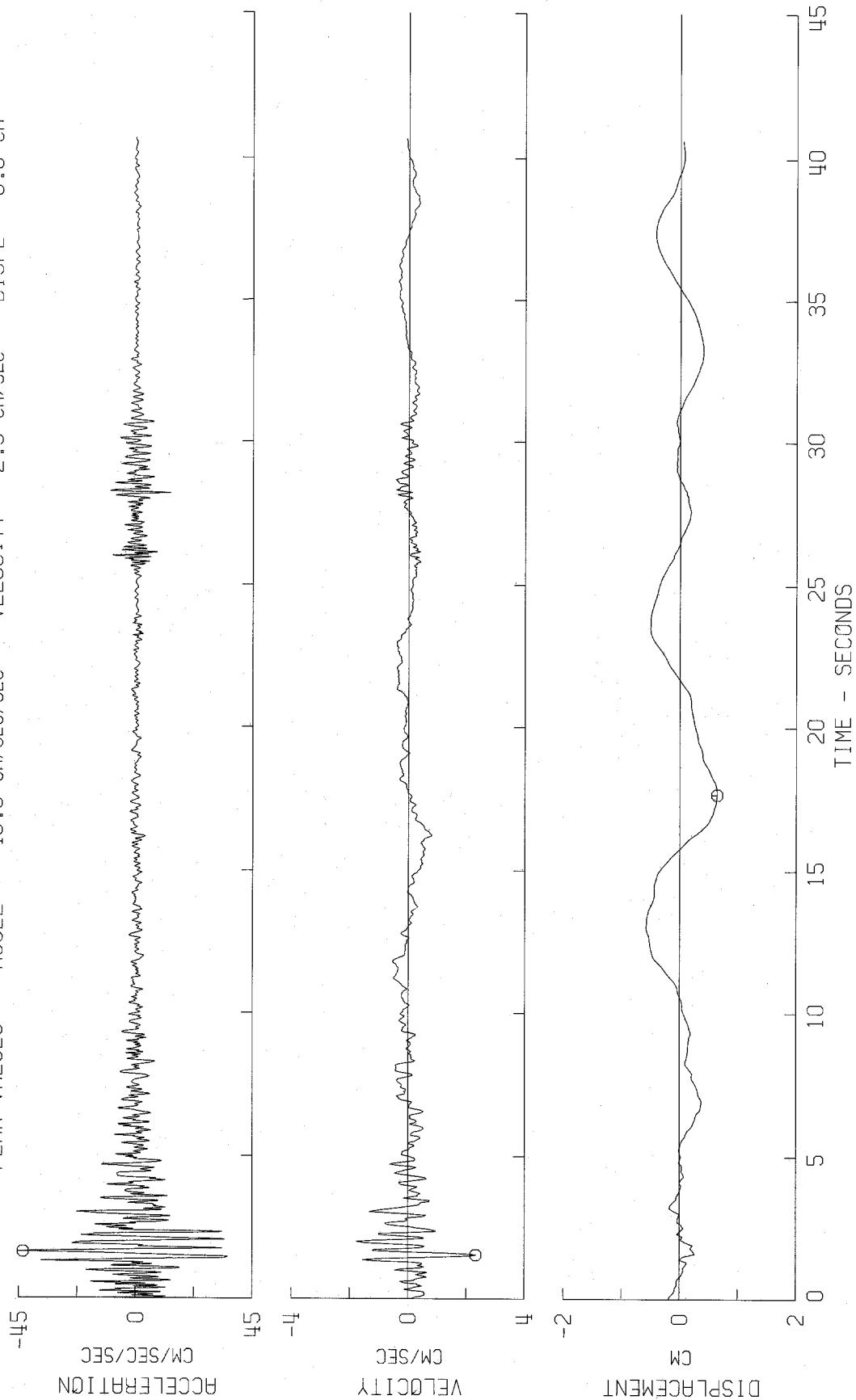
PEAK VALUES : ACCEL = -83.8 CM/SEC/SEC VELOCITY = -5.1 CM/SEC DISPL = -1.1 CM



SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA016 57.007.0 SAN FRANCISCO STATE BLDG BASEMENT COMP S81W
PEAK VALUES : ACCEL = 55.1 CM/SEC/SEC VELOCITY = 4.0 CM/SEC DISPL = 0.9 CM

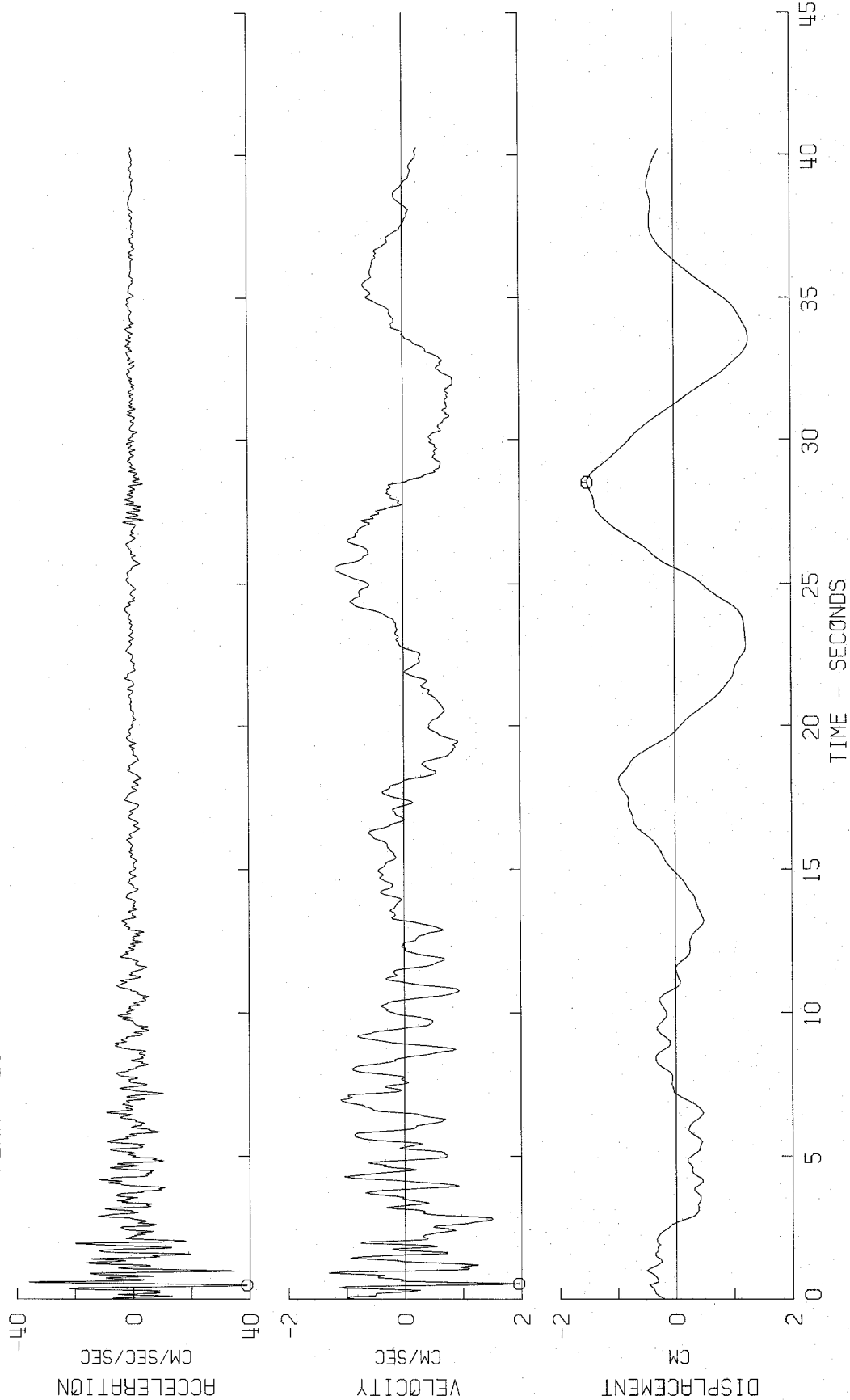


SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
 IIR016 57.007.0 SAN FRANCISCO STATE BLDG BASEMENT COMP VERT
 0 PEAK VALUES : ACCEL = -43.5 CM/SEC/SEC VELOCITY 2.3 CM/SEC DISPL = 0.6 CM



SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
IIA017 57.010.0 OAKLAND CITY HALL BASEMENT COMP N26E

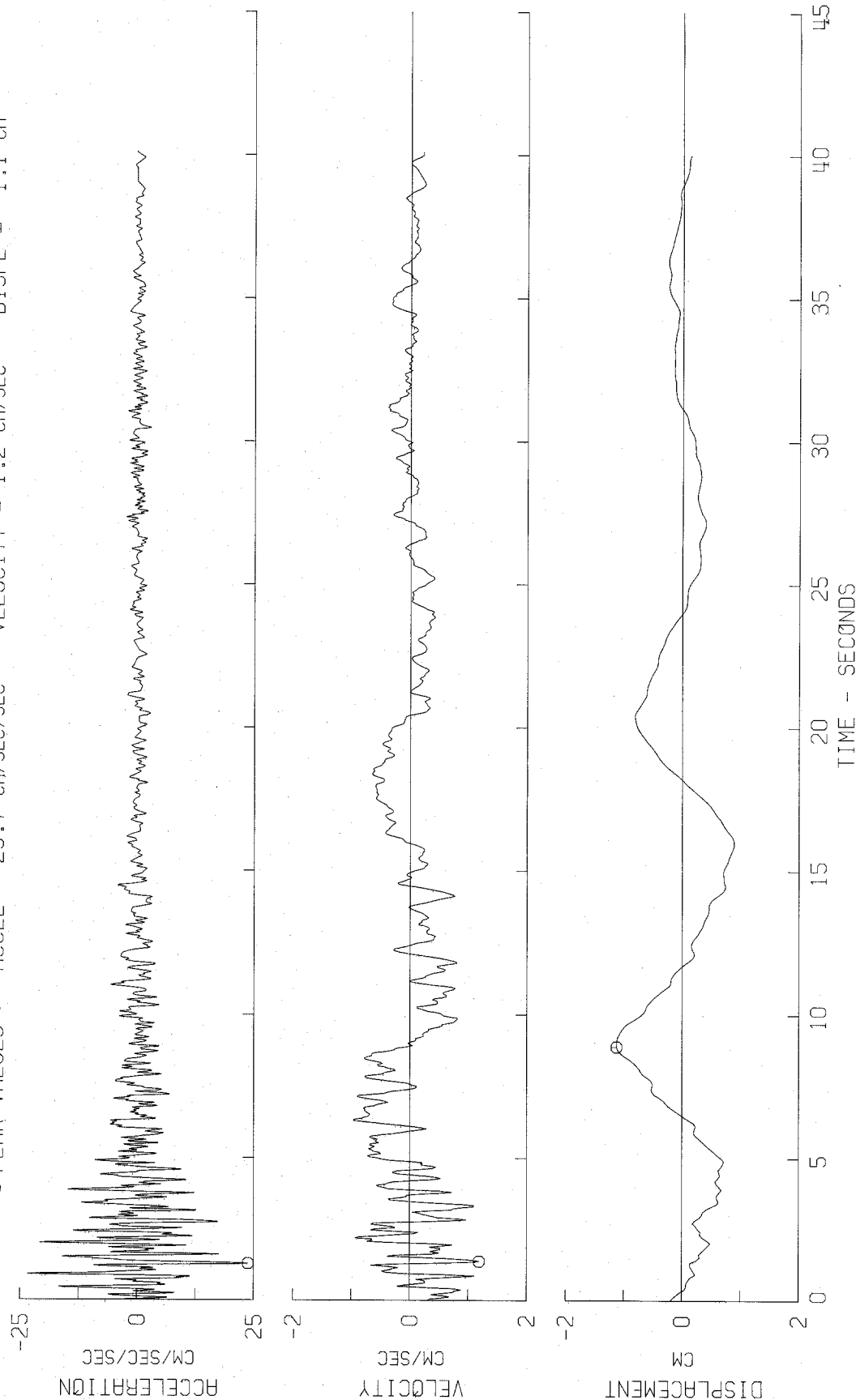
⊙ PEAK VALUES : ACCEL = 39.0 CM/SEC/SEC VELOCITY = 2.0 CM/SEC DISPL = -1.5 CM



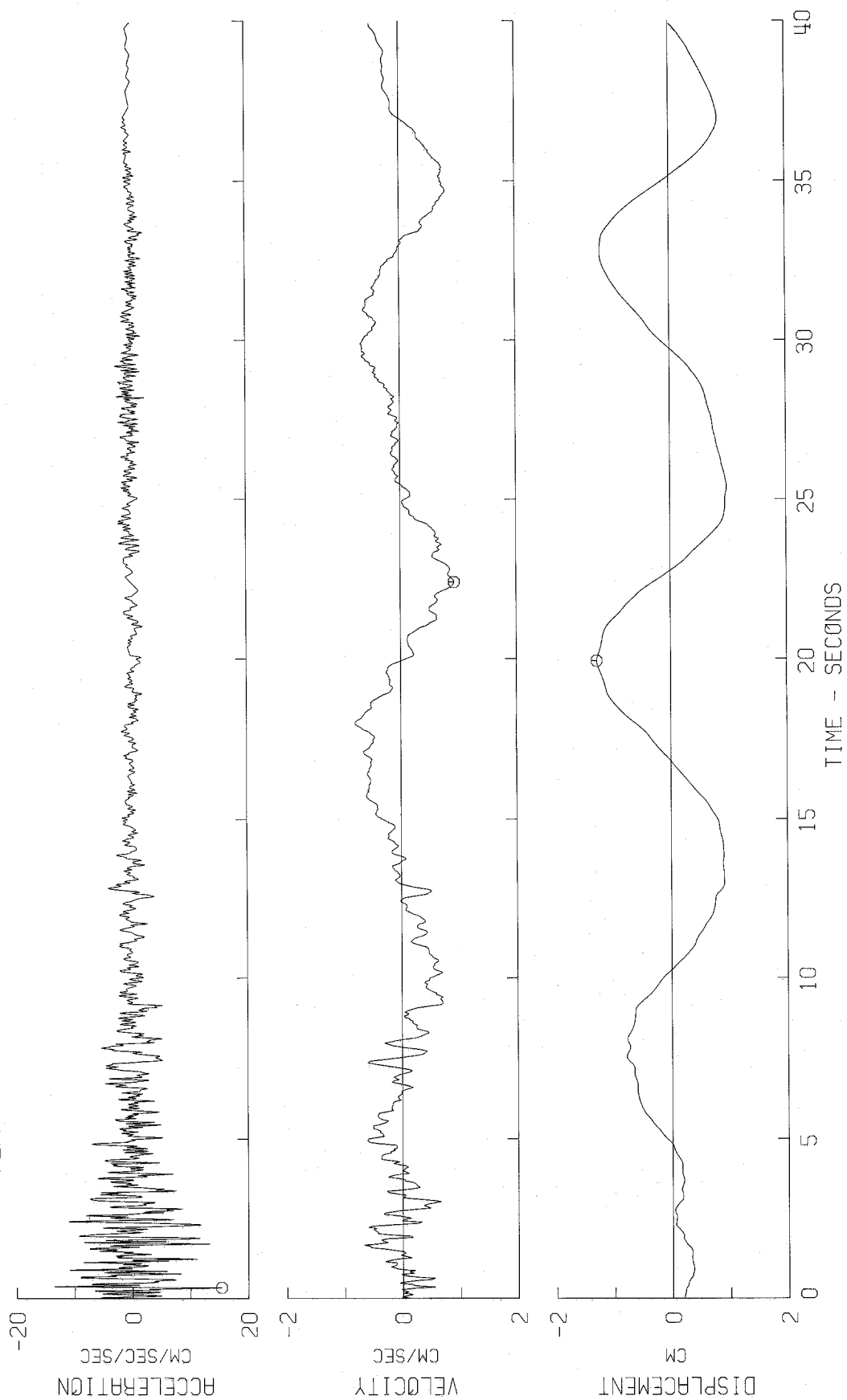
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST

IIA017 57.010.0 OAKLAND CITY HALL BASEMENT COMP S64E

⊙ PEAK VALUES : ACCEL = 23.7 CM/SEC/SEC VELOCITY = 1.2 CM/SEC DISPL = -1.1 CM



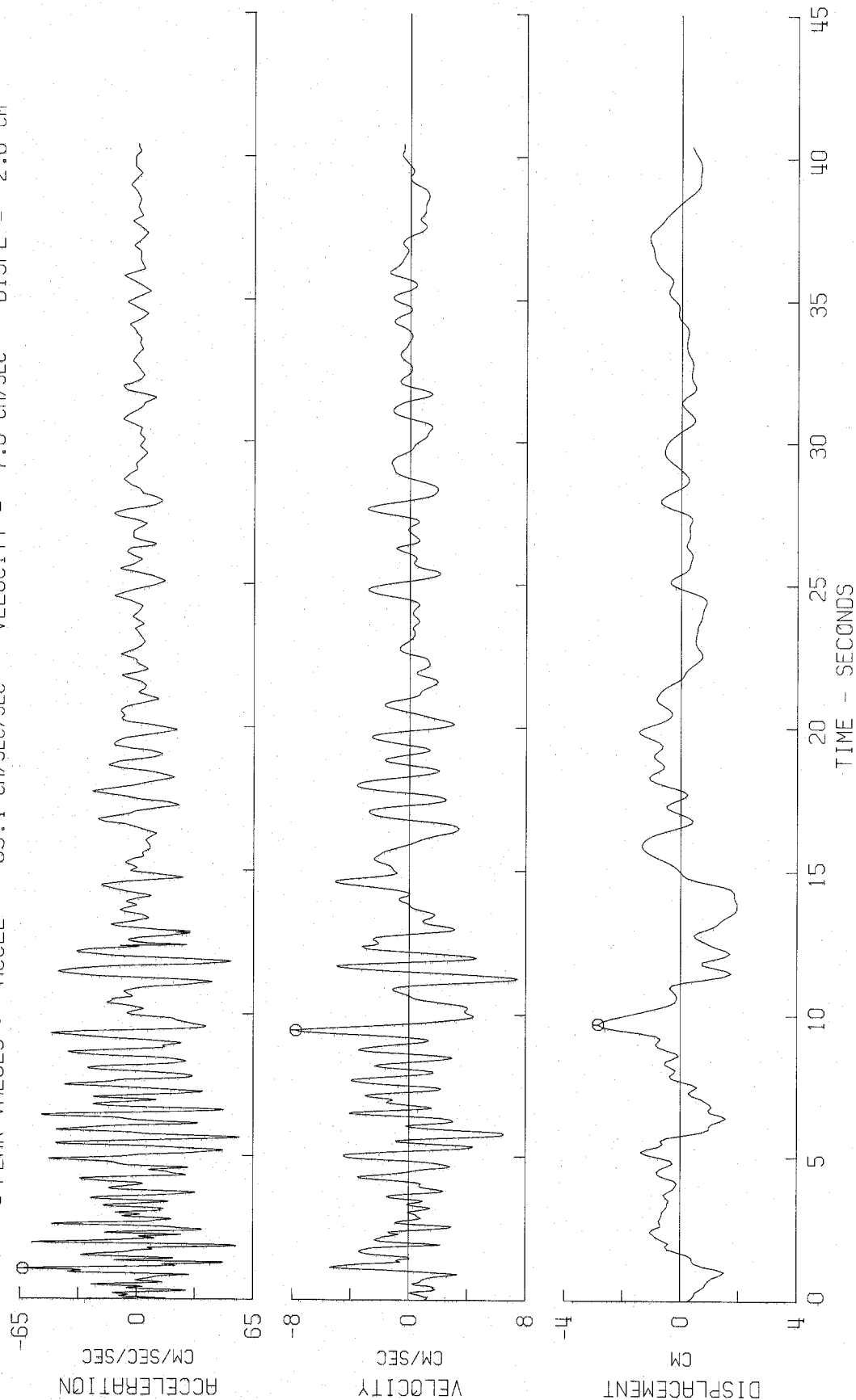
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
 IIA017 57.010.0 OAKLAND CITY HALL BASEMENT COMP VERT
 PEAK VALUES : ACCEL = 15.3 CM/SEC/SEC VELOCITY = 0.9 CM/SEC DISPL = -1.3 CM



HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST

IIA018 61.001.0 HOLLISTER CITY HALL COMP SO1W

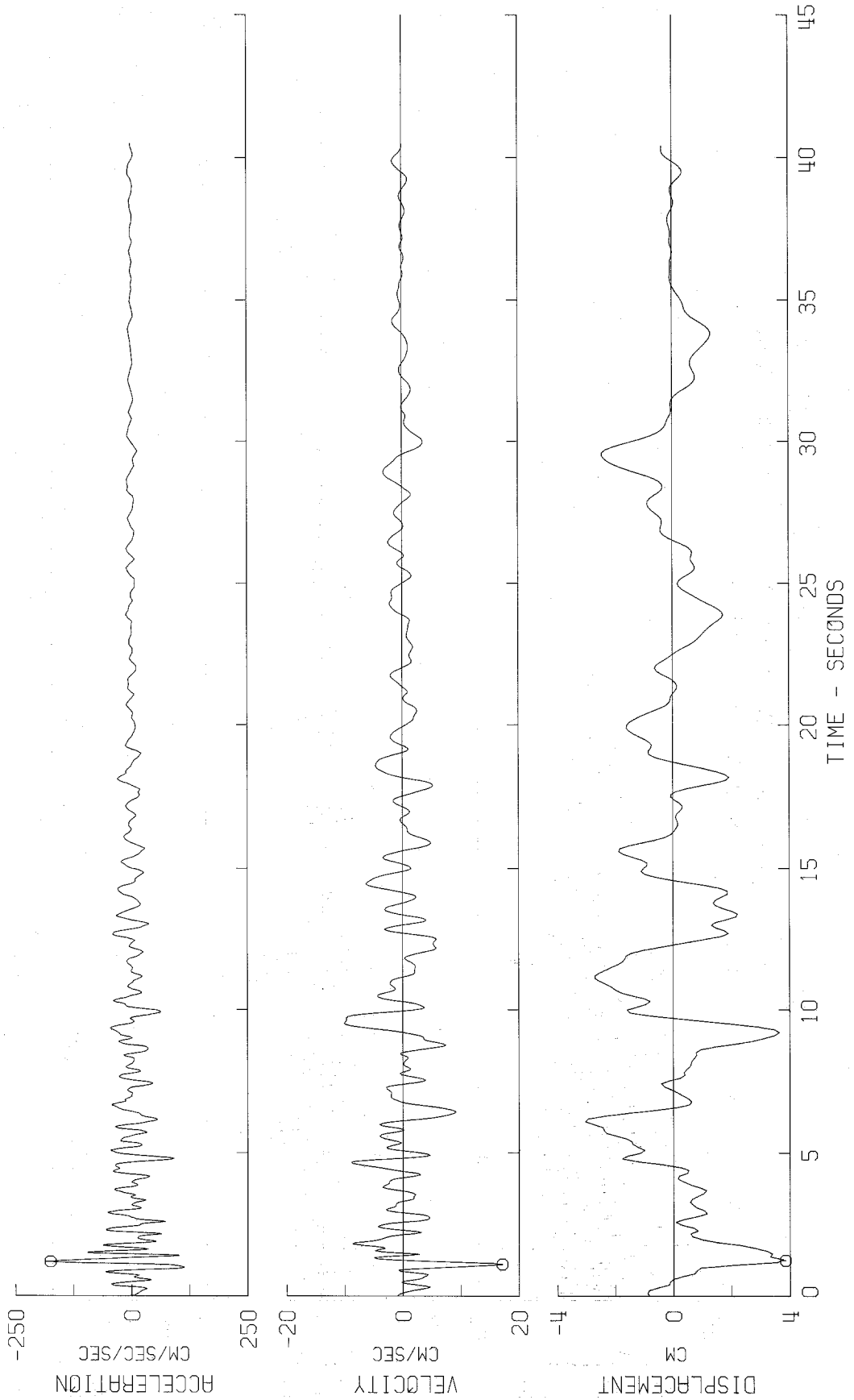
PEAK VALUES: ACCEL = -63.4 CM/SEC/SEC VELOCITY = -7.8 CM/SEC DISPL = -2.8 CM



HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST

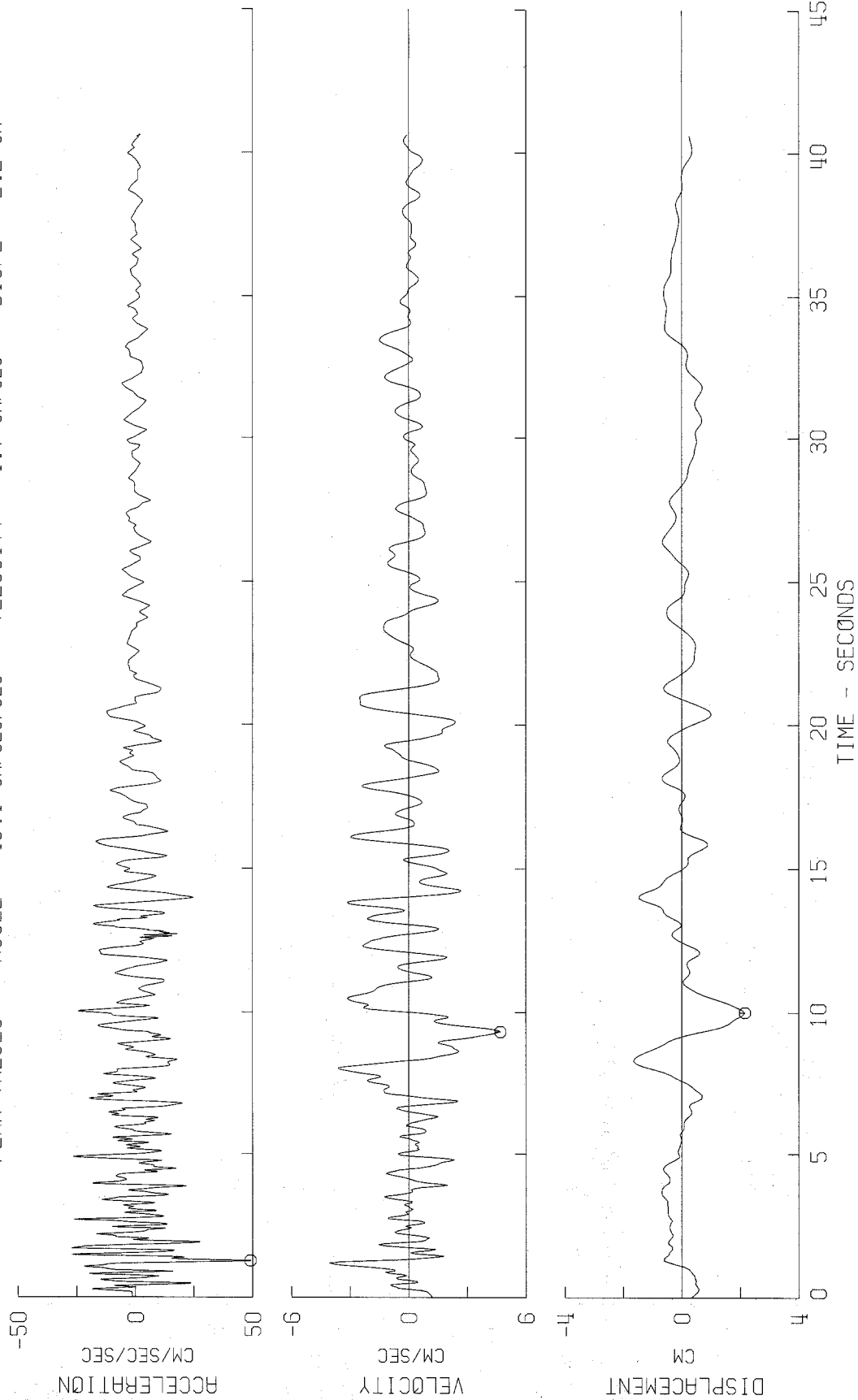
IIA018 61.001.0 HOLLISTER CITY HALL COMP N89W

⊙ PEAK VALUES : ACCEL = -175.7 CM/SEC/SEC VELOCITY = 17.1 CM/SEC DISPL = 3.8 CM

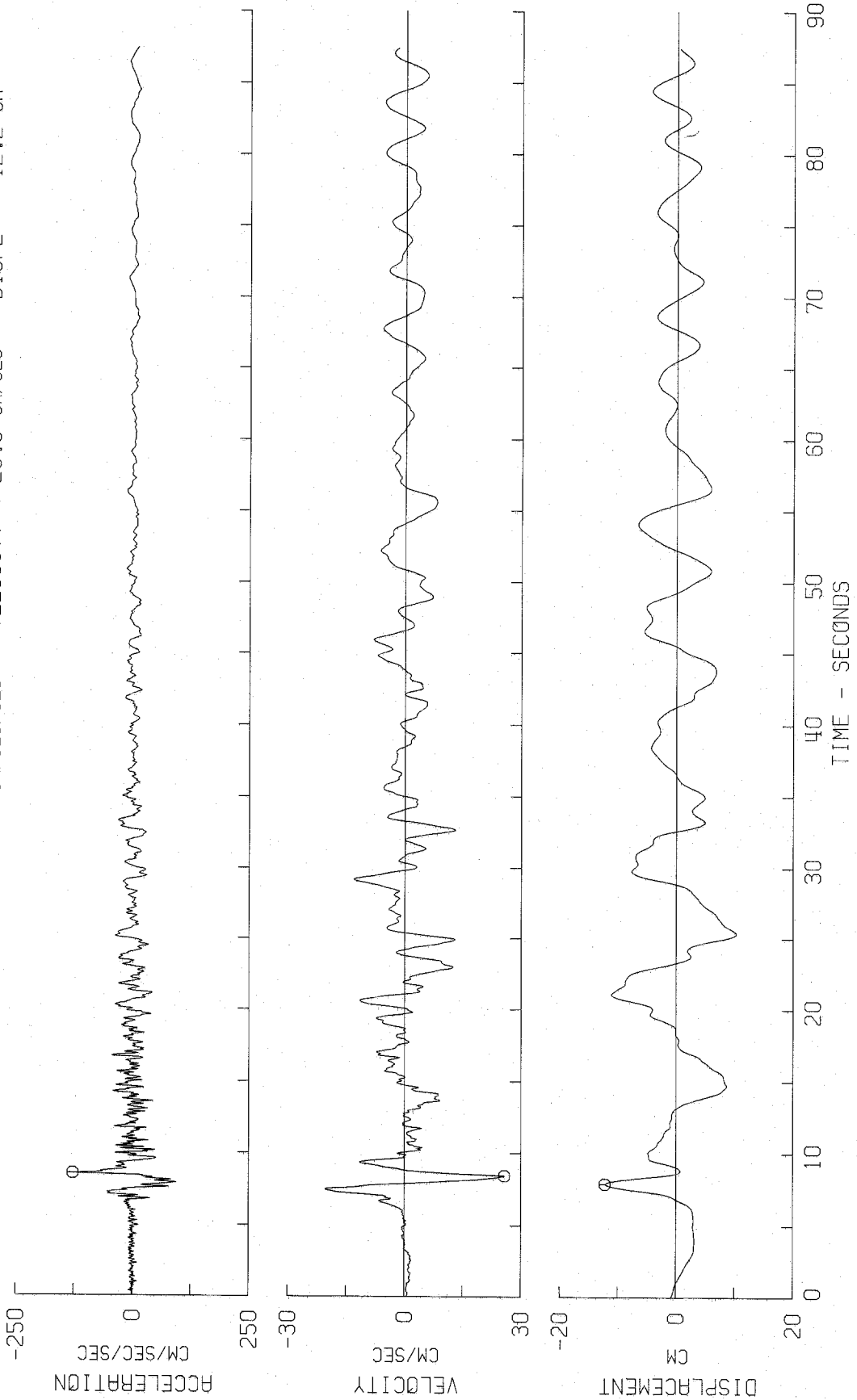


HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST
IIA018 61.001.0 HOLLISTER CITY HALL COMP VERT

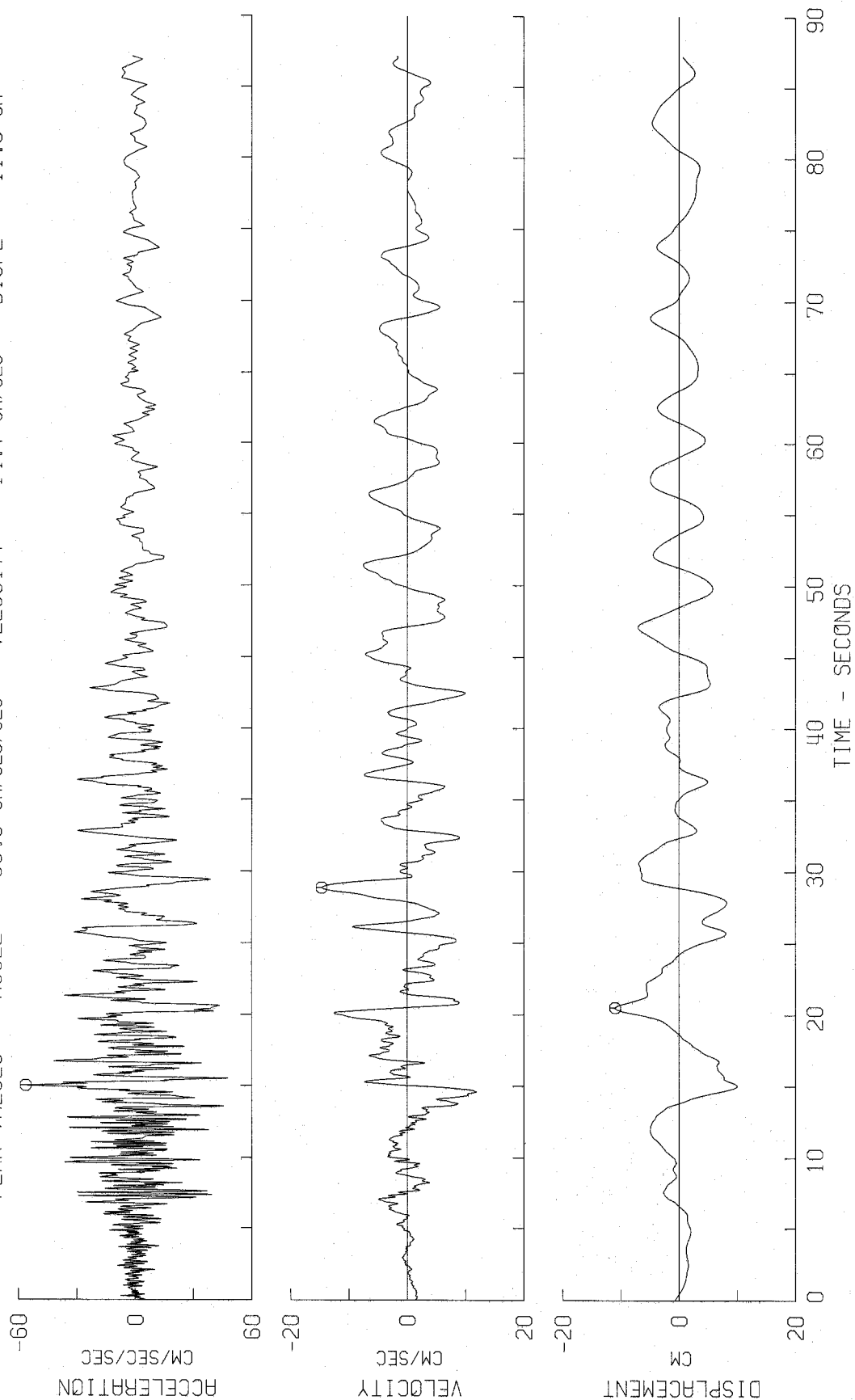
⊙ PEAK VALUES : ACCEL = 49.1 CM/SEC/SEC VELOCITY = 4.7 CM/SEC DISPL = 2.2 CM



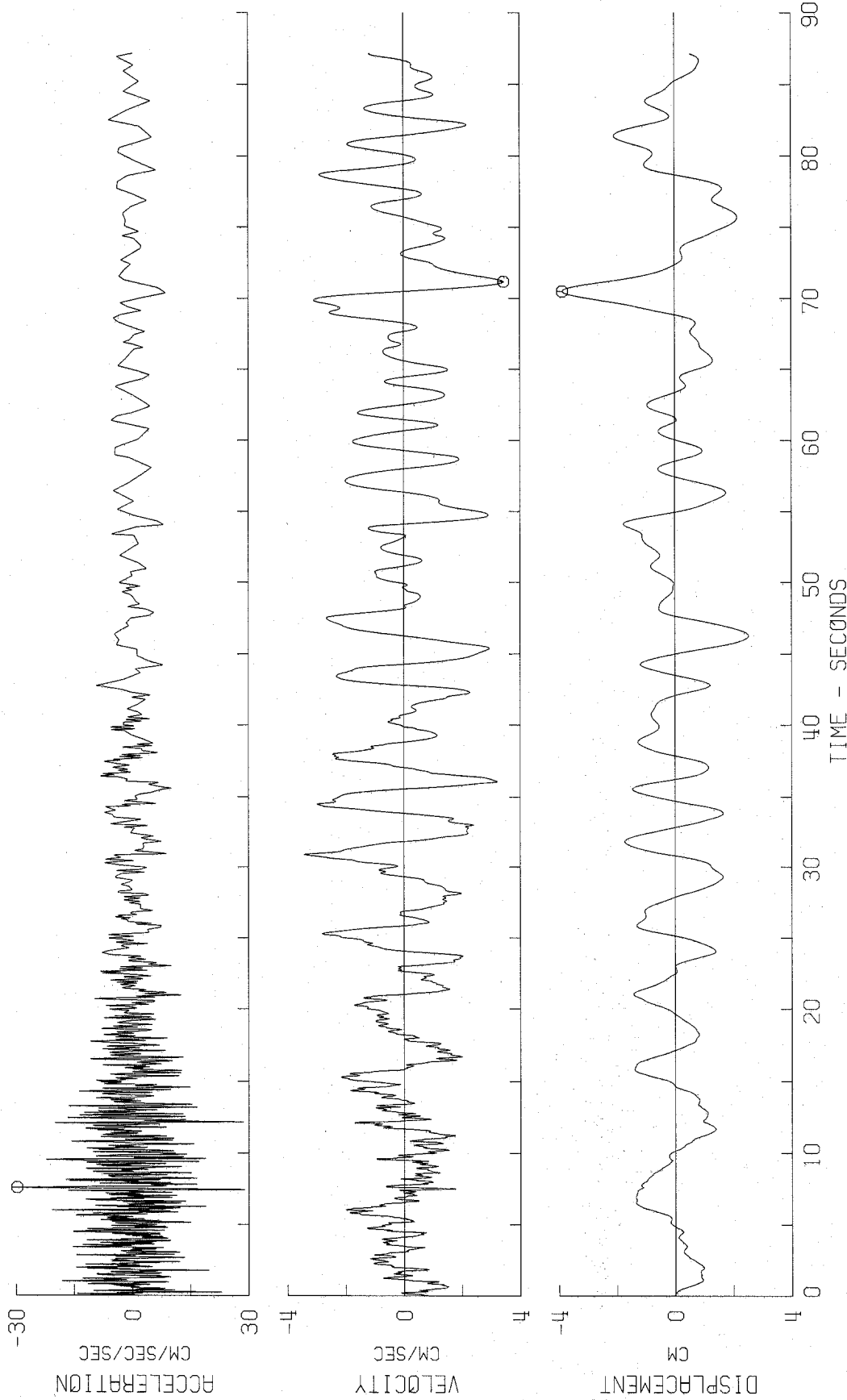
BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST
IIA019 68.005.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S00W
PEAK VALUES : ACCEL = -127.8 CM/SEC/SEC VELOCITY = 25.8 CM/SEC DISPL = -12.2 CM



BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST
IIA019 68.005.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S90W
PEAK VALUES: ACCEL = -56.3 CM/SEC/SEC VELOCITY = -14.7 CM/SEC DISPL = -11.0 CM



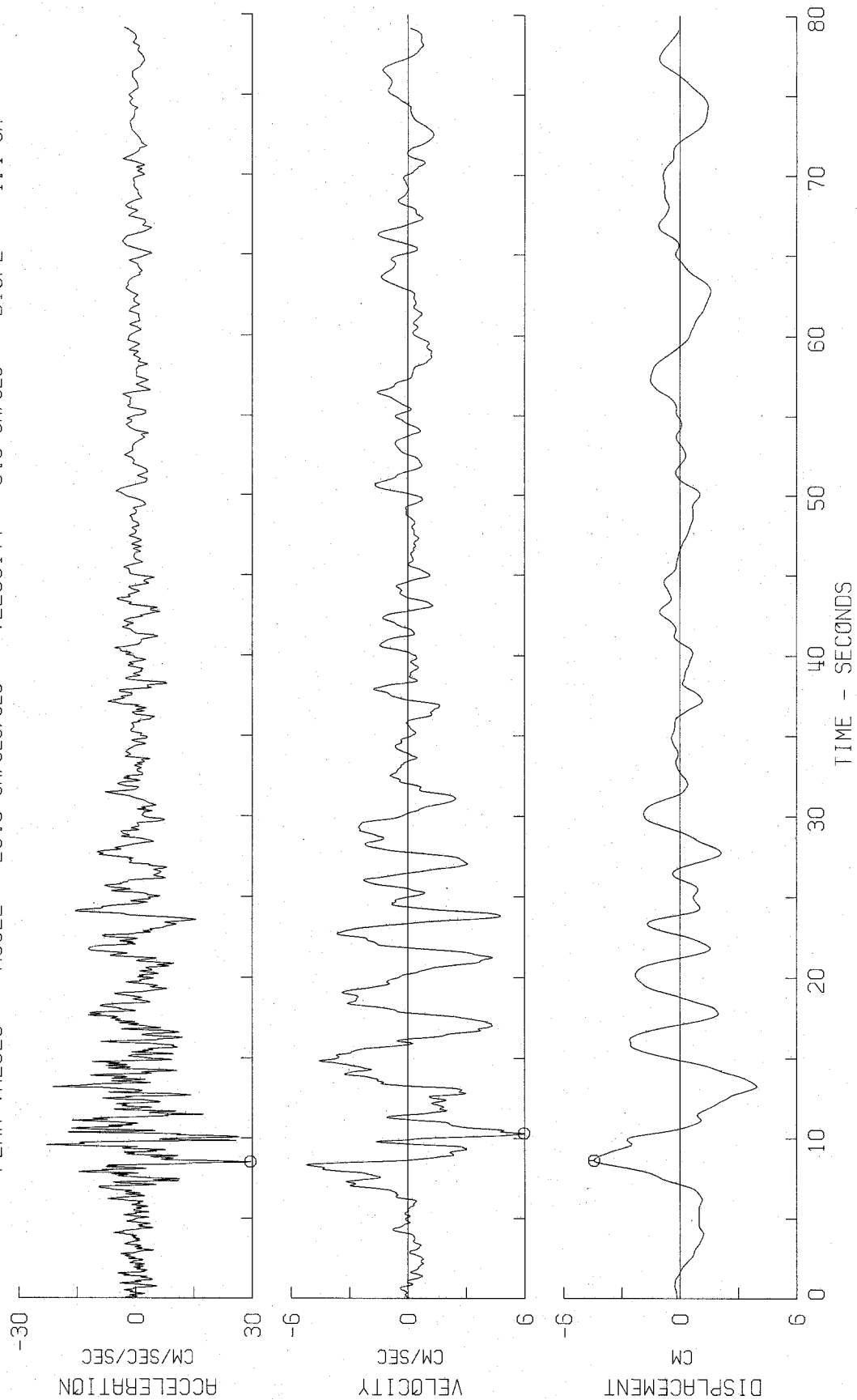
BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST
 IIR019 68.005.0 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT
 PEAK VALUES : ACCEL = -29.7 CM/SEC/SEC VELOCITY = 3.4 CM/SEC DISPL = -3.9 CM



BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST

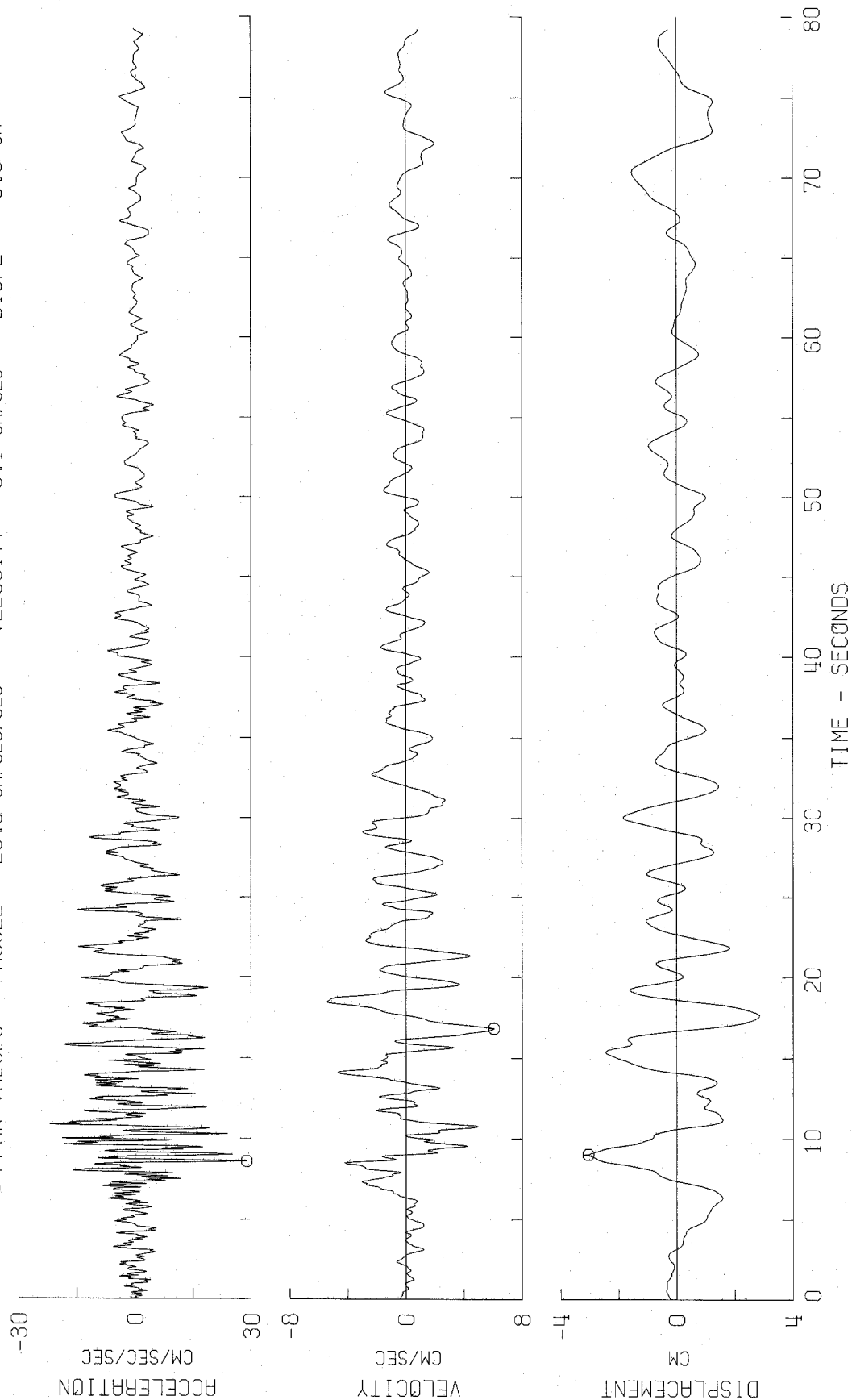
IIA020 68.007.0 SAN DIEGO LIGHT AND POWER BLDG COMP S00W

PEAK VALUES : ACCEL = 29.5 CM/SEC/SEC VELOCITY = 6.0 CM/SEC DISPL = -4.4 CM



BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST
IIA020 68.007.0 SAN DIEGO LIGHT AND POWER BLDG COMP N90E

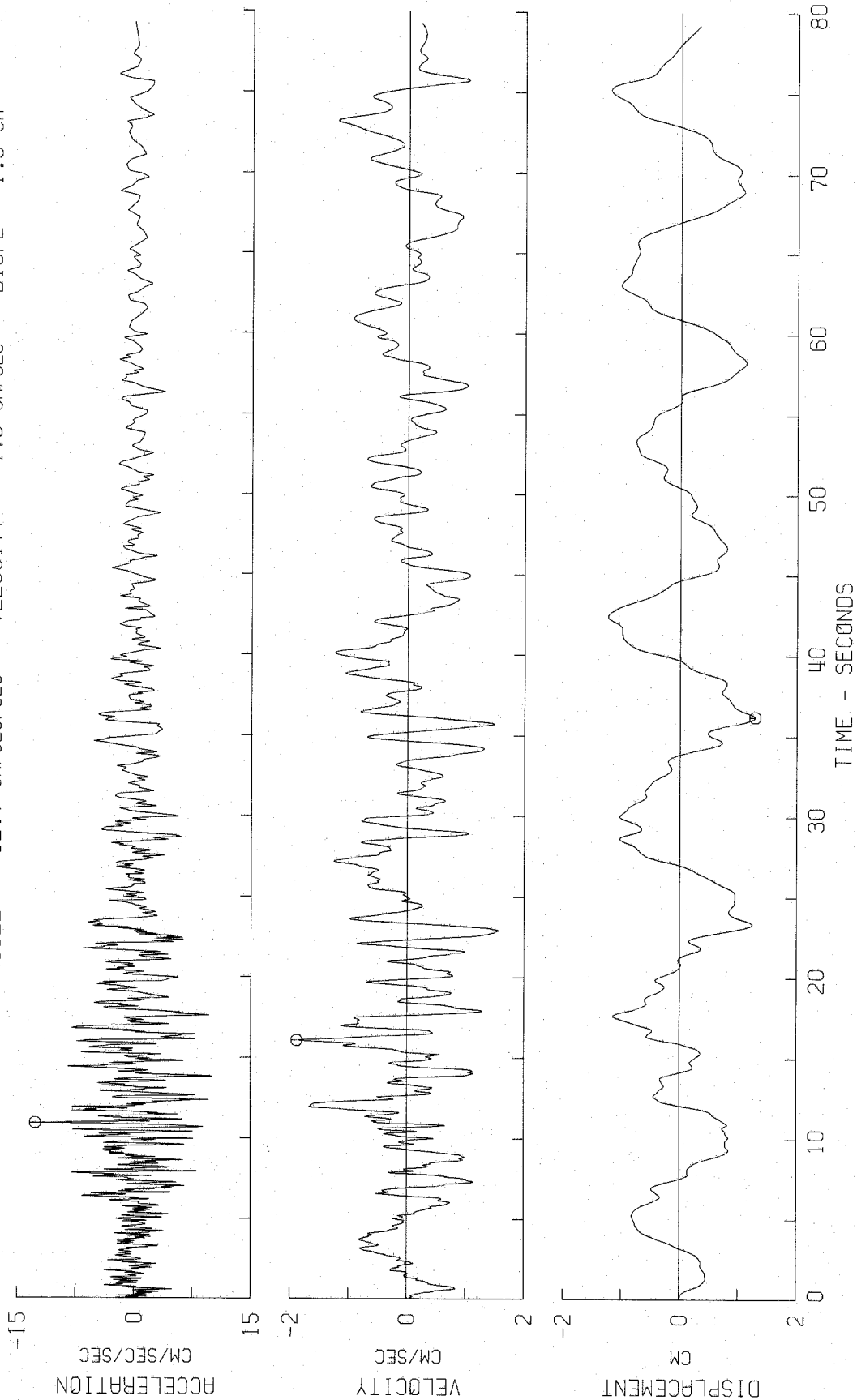
○ PEAK VALUES : ACCEL = 28.9 CM/SEC/SEC VELOCITY = 6.1 CM/SEC DISPL = -3.0 CM



BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST

IIA020 68.007.0 SAN DIEGO LIGHT AND POWER BLDG COMP VERT

PEAK VALUES : ACCEL = -12.7 CM/SEC/SEC VELOCITY = -1.9 CM/SEC DISPL = 1.3 CM



IIAC01 40.001.0 IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST EPICENTER 32 44 00N, 115 27 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP SOFF 32 47 43N, 115 32 55W
INSTR PERIOD = 0.099" SEC DAMPING = 0.552 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACIN = 341.7 CM/SEC/SEC AT 2.12 SEC VELO = 33.4 CM/SEC AT 2.18 SEC DISP = 10.9 CM AT 8.58 SEC

2688 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC									
INITIAL VELO = -4.66421 CM/SEC					INITIAL DISP = 2.15852 CM				
-14	-108	-101	-88	-95	-120	-142	-128	-110	-85
-131	-190	-196	-66	30	141	-49	-128	-144	-203
236	252	336	463	492	419	359	271	235	339
-787	-603	-484	-250	-59	134	308	499	710	995
1209	328	-1475	-2066	-1989	-2034	-1816	-1725	-1752	-1753
1598	1960	2412	2729	3036	3200	3417	2821	2324	-1198
1757	576	-2631	-1547	-1729	-1012	-579	237	-670	-1980
-95	-433	-838	-951	-716	-539	-334	-108	185	420
219	-641	683	689	1318	1353	2040	-931	-1308	-692
-126	-674	-324	-337	-109	17	299	488	608	222
29	259	293	-55	-147	143	206	499	645	957
-384	-311	-1118	-1661	-2464	-2025	-1835	-1317	-960	-325
1853	2456	1685	-1380	-999	-1089	-907	-469	-1250	-2111
-1145	-1717	-546	64	-804	-1634	-859	-961	-396	-147
1352	1606	1861	1281	640	204	314	373	496	235
255	-41	-428	-133	95	230	-129	-50	80	210
-16	38	85	-56	-304	-421	-244	-236	-177	-129
235	355	705	779	184	-263	-124	-42	159	48
-204	-82	-206	-137	-55	53	134	266	232	79
255	368	525	541	425	398	559	756	365	411
-208	-492	-530	-362	-405	-303	-316	-265	-265	-269
287	305	112	214	136	384	-861	-1349	-1342	-1354
85	163	50	264	582	867	1200	1695	1111	-1100
1072	1669	947	408	667	132	-95	-520	-827	-1152
20	146	537	798	-205	-590	-169	-175	-28	74
-79	168	567	93	-55	44	-123	-282	-437	-352
-217	-873	-973	-589	-336	77	259	508	361	81
-11	65	-37	-5	-168	-410	-80	79	374	615
-227	-428	-679	-661	-590	-513	-408	-309	-266	-541
211	432	613	767	933	1066	1130	1187	1247	1334
-1246	-1179	-1050	-920	-743	-809	-850	-860	-863	-873
589	525	355	197	199	492	343	288	432	239
-28	182	426	439	512	466	479	193	222	274
-347	-426	-416	-275	-270	74	428	-231	-387	-83
-333	-269	-301	-200	-67	-38	105	296	344	957
148	508	-22	-489	-358	-691	-516	-371	88	632
544	399	45	-82	-185	-20	6	-117	-210	-303
91	-548	-555	-243	-81	250	410	182	-27	-243
-110	50	241	-34	-216	-471	-363	-195	-18	170
683	172	-170	-527	-664	-387	-222	-33	119	-128
-144	-108	-82	-42	-66	-163	-164	-172	-197	-162
-163	-164	-82	-42	-66	599	400	400	63	-515
892	926	839	901	993	892	926	839	901	993
-429	-17	360	785	1164	-429	-17	360	785	1164
-173	113	533	895	1186	-173	113	533	895	1186
-751	-523	-271	-44	188	-751	-523	-271	-44	188
344	565	883	1130	1363	344	565	883	1130	1363
-1071	-1162	-762	-559	-215	-1071	-1162	-762	-559	-215
826	1206	1478	1737	421	826	1206	1478	1737	421
1984	1769	1250	-1207	-542	1984	1769	1250	-1207	-542
-169	285	447	983	1424	-169	285	447	983	1424
-510	-544	-1200	-1039	-1158	-510	-544	-1200	-1039	-1158
-27	292	445	785	1033	-27	292	445	785	1033
-157	-69	147	379	579	-157	-69	147	379	579
5	76	35	-95	-36	5	76	35	-95	-36
-106	-111	-99	-2	73	-106	-111	-99	-2	73
159	320	419	123	-160	159	320	419	123	-160
92	-22	-21	52	93	92	-22	-21	52	93
-471	-433	-458	-57	178	-471	-433	-458	-57	178
281	310	358	341	358	281	310	358	341	358
-258	-60	-91	-182	-147	-258	-60	-91	-182	-147
-597	-670	-552	-27	378	-597	-670	-552	-27	378
1178	1610	-270	34	-56	1178	1610	-270	34	-56
304	23	64	-406	-451	304	23	64	-406	-451
1144	733	237	-368	-271	1144	733	237	-368	-271
-550	-722	-803	-523	-340	-550	-722	-803	-523	-340
-243	-48	126	379	241	-243	-48	126	379	241
-582	-473	-333	-199	20	-582	-473	-333	-199	20
-140	-666	-555	-693	-984	-140	-666	-555	-693	-984
245	580	314	236	485	245	580	314	236	485
75	44	-145	-316	-241	75	44	-145	-316	-241
797	949	345	45	-123	797	949	345	45	-123
-251	-135	79	-115	-251	-251	-135	79	-115	-251
-744	-539	-330	-128	31	-744	-539	-330	-128	31
225	-88	-227	74	181	225	-88	-227	74	181
40	98	137	221	437	40	98	137	221	437
331	-14	-195	-247	-212	331	-14	-195	-247	-212
516	432	344	505	653	516	432	344	505	653
142	70	-63	-120	-322	142	70	-63	-120	-322

-346	-91	73	309	472	603	576	330	-73	-777	-608	-438	-209	31	350	293	121	338	317	254
206	198	174	21	-144	-343	-339	-145	-28	170	-96	-255	-279	-388	-242	-215	-182	-174	-38	-27
-185	-123	87	343	695	910	853	760	513	186	15	-190	-151	-73	21	129	215	24	-124	-329
-519	-708	-579	-462	-307	-145	-9	-180	-318	-465	-391	-345	-316	-435	-491	-475	-420	-361	-277	-258
-139	-68	507	722	878	-187	765	439	80	13	-126	-15	30	104	104	193	205	74	-56	-72
70	106	147	-9	-159	182	-187	-7	155	115	-302	-309	-95	-58	4	20	50	57	97	134
177	218	261	302	346	386	474	393	238	115	-79	-124	54	27	-250	-566	-630	-591	-413	-68
272	277	-21	-60	-110	-221	-416	-519	-222	30	79	139	171	253	323	391	164	-136	-323	-291
-287	-304	-339	-245	-76	125	376	402	245	156	-40	-153	-289	-316	-111	94	335	576	424	143
-7	-135	-270	-341	-357	-396	-402	-488	-480	-406	-407	-351	-187	-57	44	-19	-72	-169	-115	126
358	654	716	762	739	628	484	264	-44	-288	-384	-492	-428	-416	-276	-52	237	426	604	452
284	126	-54	-275	-423	-175	1	254	481	641	554	413	184	-48	-303	-531	-708	-928	-863	-631
-376	87	309	589	614	385	351	311	246	19	-198	-158	-15	99	286	408	563	531	314	165
-24	-189	-276	-371	-450	-534	-483	-379	-296	-196	-184	-159	-119	-53	2	59	-23	-112	-205	-322
-388	-341	-287	-328	-407	-487	-563	-644	-555	-446	-8	253	411	644	579	474	384	385	340	357
8	-254	-460	-471	-222	-65	164	355	504	371	280	158	41	-27	21	44	99	135	94	58
22	-31	-31	4	-25	-124	-235	-406	-530	-701	-323	-52	94	328	478	509	358	342	306	285
263	168	-5	-212	-365	-310	-297	-280	-237	-266	-308	-366	-357	-308	-193	19	196	160	129	140
110	108	92	89	19	-131	-247	-436	-432	-300	-192	-48	97	168	148	173	78	-58	-215	-234
60	262	269	84	-41	-227	-76	31	182	310	479	459	166	-58	-396	-444	-241	-101	217	261
121	8	-168	-382	-566	-781	-619	-256	44	456	783	1103	953	489	122	-387	-846	-1226	-864	-616
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40	23	-62	-286	-380	-457	-505	-777	-628	-189	189	509	744	749	562	455	525	635	731	851
927	975	929	814	264	-289	-901	-1364	-859	-468	81	594	823	556	301	-11	-380	-347	-20	180
633	1013	1122	1107	940	805	608	508	206	-201	-572	-1021	-1332	-1225	-1207	-1006	-762	-548	-489	-405
-291	-176	-141	-98	-50	19	80	35	-29	-61	-34	-13	76	205	327	450	577	562	464	300
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255	227	171	127	54	-47	-149	-210	-254	-252	-245	-226	-179	-136	-82	-14	44	89	97	100
100	104	136	121	100	72	19	-28	-83	-131	-190	-194	-139	-100	-92	-44	-40	-45	-49	-39
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38	31	27	21	17	12	7	3	13	19	22	9	-3	-17	-31	-47	-53	-48	-43
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-33	-51	-60	-56	-54	-50	-66	-91	-114	-138	-140	-121	-96	-74	-46	-34	-42	-45	-55
-63	-72	-80	-73	-52	-37	-26	-14	-45	-77	-23	31	41	26	13	15	61	73	74

IIA001 40.001.0 IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST EPICENTER 32 44 00N, 115 27 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S00W 32 47 43N, 115 32 55W
INSR PERIOD = 0.1000 SEC DAMPING = 0.528 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 210.1 CM/SEC/SEC AT 11.44 SEC VELO = -36.9 CM/SEC AT 2.14 SEC DISP = -19.8 CM AT 3.00 SEC

INITIAL VELO = 11.83165 CM/SEC INITIAL DISP = 1.35018 CM

2674 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

3	19	68	29	29	54	83	53	14	53	134	124	66	61	133	49	96	188	243	133
46	-81	-156	-85	-31	40	35	132	180	162	23	25	80	77	110	131	81	13	151	-330
-532	-466	-525	-415	-401	-515	-569	-572	-528	-497	-498	-550	-492	-431	-362	-280	-204	-147	-213	-47
215	479	580	188	-122	-538	-968	-1100	-1059	-1070	-999	-936	-1128	-1469	-1213	-1099	-858	-636	-380	-155
107	338	599	835	1092	1325	1485	1192	1105	1003	1079	824	369	-225	-1481	-1786	-1589	-1693	-1521	-1446
-1348	-1265	-1179	-1088	-997	-764	-595	-95	542	1059	770	585	247	-128	-675	-826	-521	-300	74	447
852	1118	922	775	544	156	-183	-612	-700	-318	-38	284	594	919	1109	651	270	-151	144	330
772	1181	1592	1780	1487	1183	788	326	351	529	690	711	663	621	542	521	634	698	810	431
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694	708	690	673	623	794	630	525	463	533	623	517	206	-67	-132	49	536	1002	323	-181
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198	578	531	84	-74	-403	-533	-498	-301	-106	-444	-792	-471	-414	-138	98	323	10	-287	-405
-235	-167	67	237	405	339	134	-48	-271	-439	-125	118	472	637	212	-64	-420	-661	-558	-500
-353	-173	-5	161	132	140	117	310	288	154	85	-76	-181	-366	-291	-13	274	245	109	92
-103	-240	-407	-526	-494	-719	-523	-260	131	693	873	616	419	-91	-549	-929	-853	-578	-396	-658
-718	-341	-43	262	567	801	961	856	661	498	284	113	-175	-476	-738	-517	-369	-113	-249	-317
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-244	-35	-238	-427	-281	-243	-138	-21	46	-89	-223	-418	-643	-471	-109	320	607	125	174	-280
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-120	-78	-46	8	13	-13	-27	-58	-49	-52	-36	-43	-34	-24						

IIA001 40.001.0 IMPERIAL VALLEY EARTHQUAKE MAY 18, 1940 - 2037 PST EPICENTER 32 44 00N, 115 27 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT 32 47 43N, 115 32 55W
INSTR PERIOD = 0.3950 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACIN = -206.3 CM/SEC/SEC AT 0.98 SEC VELO = -10.8 CM/SEC AT 3.26 SEC DISP = -5.6 CM AT 3.42 SEC

INITIAL VELO = 2.97210 CM/SEC INITIAL DISP = 1.03927 CM

2690 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

24	-230	-275	-357	-390	-60	409	209	-683	-647	51	134	317	738	600	-531	-261	-130	-439	-690
-117	260	840	1224	-232	-1371	-727	-381	394	771	356	179	-171	-58	-194	229	903	-80	-1112	-699
-188	577	1077	1734	-36	-968	666	1173	1728	-2063	-555	-431	936	220	-1836	-1837	-419	606	1722	-1410
-440	-267	519	875	-35	-809	-98	278	1093	421	-791	-664	-279	-423	-261	204	521	-399	-56	236
781	455	-589	-315	215	743	1242	-527	-133	-398	-641	18	946	52	-1522	-489	-99	543	-86	-219
-10	-121	-525	-426	-73	227	314	-606	-171	149	241	157	509	103	-289	-144	-241	-211	239	-867
-780	-265	22	595	-705	-898	-227	-66	785	31	-366	-214	-807	-106	302	1060	679	-1136	-493	441
1126	285	135	28	-244	-186	81	74	32	120	-187	65	347	419	216	-26	-531	-675	-242	-34
-230	-1021	-658	28	748	1645	1904	-1163	136	535	1347	772	515	-49	130	-215	-202	-369	-114	-48
156	270	78	-188	-9	-681	-425	143	406	-474	-761	-324	87	623	1015	-84	-521	-235	347	328
55	367	218	-404	-413	-21	241	-223	-5	609	-65	-556	19	495	23	-740	-149	-54	178	-165
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415	10	-308	-69	185	355	165	204	-109	-43	432	423	-36	-154	55	-79	-374	175	505	-831
-672	-233	142	556	-74	85	476	56	-683	-234	361	130	-13	-98	166	184	178	-124	-320	54
495	363	193	139	-460	-450	383	103	-820	-86	63	154	289	97	-448	-201	341	677	2	-774
-584	-157	471	750	-683	-660	153	278	447	173	-590	-739	-218	471	809	144	-637	-304	43	733
548	-619	-341	-6	457	802	387	-94	366	45	-866	14	736	470	-237	-426	-86	388	-307	-1233
-348	341	1100	-388	-1067	-520	-183	539	425	-304	-281	-22	548	271	75	-313	15	-348	-311	46
294	86	492	196	-505	198	399	220	-52	-632	-210	-19	-228	-585	-593	-75	-211	-117	115	651
221	-758	-760	-116	573	548	-665	-57	495	162	-72	-486	-40	183	27	146	-153	-388	-742	-540
410	306	-80	37	-197	-13	254	113	56	-52	-413	-161	245	-185	186	388	500	-20	-189	90
498	464	-40	-434	-210	50	398	588	85	-351	-206	90	259	153	45	-92	-21	87	51	69
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302	147	88	-55	-147	-36	-323	-274	196	288	-81	-231	158	197	-435	-740	-625	-451	-136	313
323	-39	-147	-39	149	125	-111	-325	-345	-214	-70	15	76	-47	-239	-182	-46	157	14	122
219	562	-100	-499	262	19	-314	12	242	98	-236	-192	129	318	-318	-343	84	93	303	249
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-615	-421	-349	-377	-452	-415	-415	-363	-356	-276	-272	-56	165	21	522	246	-9	-88	28	30
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IIA002 51.001.0 NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST EPICENTER 40 17 00N, 124 48 00W
STATION NO. 023 FERNDAL CITY HALL COMP S44W 40 34 00N, 124 15 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS	ACLN = -102.0	CM/SEC/SEC AT 4.14 SEC	VELD = 4.8	CM/SEC AT 3.26 SEC	DISP = -2.4	CM AT 2.32 SEC													
INITIAL VELO = -1.24010 CM/SEC INITIAL DISP = 0.33629 CM																			
2795 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
-37	38	52	96	144	108	27	-30	-48	-25	5	35	72	107	93	33	-10	-33	-52	-70
-64	-31	-14	-37	-73	-108	-103	-68	-42	-22	19	69	57	15	-12	-38	-58	-61	-35	-5
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-43	0	69	148	235	254	222	-75	-214	-232	-165	-88	-30	15	85	180	215	144	76	82
74	-13	-151	-200	-78	140	397	408	204	12	5	96	-65	-391	-668	-572	-190	109	299	313
196	83	-18	-137	-275	-244	-48	166	292	272	97	-19	7	19	41	121	298	463	449	227
-155	-503	-458	-109	168	217	175	130	72	37	70	143	158	7	-194	-367	-465	-299	-6	199
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424	456	493	243	-227	-663	-1019	-1020	-719	-415	-151	109	270	248	144	46	-29	57	310	613
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IIA002 51.001.0 NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST EPICENTER 40 17 00N, 124 48 00W
STATION NO. 023 FERNDAL CITY HALL COMP N46W 40 34 00N, 124 15 00W
INSTR PERIOD = 0.0650 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 109.5 CM/SEC/SEC AT 4.38 SEC VELD = -7.4 CM/SEC AT 4.30 SEC DISP = -2.7 CM AT 5.32 SEC

INITIAL VELO = -0.12523 CM/SEC INITIAL DISP = -0.02928 CM

2795 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

17	13	29	36	20	10	30	60	28	12	24	38	53	54	27	-8	-14	4	22
24	11	5	21	42	27	-35	-101	-117	-90	-91	-88	-57	6	128	144	25	-43	-51
-43	-38	-40	-40	-20	13	40	38	0	9	32	58	88	117	106	53	-5	-28	0
34	61	43	-38	-119	-175	-155	-80	-32	4	56	22	-93	-86	51	200	215	61	-55
-54	-51	-84	-98	-53	17	38	-38	-137	-278	-174	-15	100	81	-19	24	227	463	561
401	171	-46	-192	-236	-255	-311	-279	-71	142	-93	-161	117	354	411	330	145	-49	-222
-354	-444	-435	-282	-21	110	71	42	120	341	250	117	18	15	75	108	33	-75	-32
106	265	423	337	83	-127	-324	-510	-538	-300	-168	-31	112	204	142	-1	-107	-117	-79
-44	-1	70	141	60	-164	-335	-387	-405	-415	-210	106	458	760	752	550	355	160	-36
-230	-352	-380	-426	-599	-744	-654	-442	-243	255	496	479	139	-287	-492	-369	-11	269	550
588	346	44	-325	-494	-314	-74	108	87	-195	-255	-341	-360	-222	-12	286	670	947	1095
1035	832	734	574	267	-89	-502	-609	-397	-276	-374	-429	-358	-210	30	286	346	241	64
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23	-13	141	315	458	456	377	357	338	49	-127	-301	-399	-394	-391	-305	-86	71	92
95	155	220	254	266	232	170	168	221	54	-1	99	249	343	259	56	-131	-242	-275
-262	-237	-214	-190	-166	-145	-161	-216	-275	-277	-203	-89	37	81	57	-8	-87	-111	-38
37	64	103	188	302	378	334	221	131	109	57	109	247	368	330	165	68	42	11
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-18	-84	-79	-35	1	33	82	142	177	206	248	281	287	259	186	126	109	106	87
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275	244	230	220	209	212	258	283	211	34	5	-42	-118	-197	-270	-328	-380	-433	-480
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4	6	9	11	14	15	14	11	8	5	2	-1	-4	-7	-10	-13	-15	-17	-19	-18
-14	-8	-3	-2	8	12	16	20	24	24	22	20	18	16	14	12	10	8	6	4
1	-2	-5	-5	-4	-2	0	1	3	5	6	8	10	11	11	9	6	4	2	-1
-3	-5	-7	-10	-14	-19	-24	-28	-30	-26	-22	-17	-13	-10	-8	-6	-4	-2	2	5

IIA002 51.001.0 NORTHWEST CALIFORNIA EARTHQUAKE OCT 07, 1951 - 2011 PST EPICENTER 40 17 00N, 124 48 00W
STATION NO. 023 FERNDAL CITY HALL COMP VERT 40 34 00N, 124 15 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.621 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -26.4 CM/SEC/SEC AT 3.00 SEC VELO = 2.2 CM/SEC AT 9.80 SEC DISP = -1.6 CM AT 21.94 SEC

INITIAL VELO = 0.85423 CM/SEC										INITIAL DISP = -0.06553 CM									
2795 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC										AT EQUALLY-SPACED INTERVALS OF 0.02 SEC									
-63	21	-6	-58	-104	-73	10	59	31	-8	7	44	77	60	-23	-85	-82	-46	1	48
59	23	-34	-112	-116	-25	50	40	3	17	28	23	49	65	37	7	-44	-84	-35	34
60	43	3	-37	-74	-31	20	-15	-31	-8	-17	-44	-38	-15	-31	-61	-14	66	110	106
69	44	29	12	1	16	13	-38	-97	-99	-60	-24	-18	-30	-23	1	29	60	53	3
-32	-26	-37	-70	-64	-44	-46	-36	-6	20	27	22	33	61	79	69	66	96	117	75
31	-65	-164	-180	-184	-151	-74	30	71	-7	-82	-72	-67	-74	-42	-8	8	29	75	115
132	120	77	53	45	81	129	120	18	-107	-124	-93	-74	-15	49	67	72	91	101	32
-73	-83	-25	-8	-39	-65	-78	-105	-166	-252	-264	-153	-67	-26	52	168	212	127	40	21
52	106	127	83	-18	-83	-95	-81	-24	37	47	18	17	46	78	61	-10	-70	-84	-65
-51	-48	-35	-3	38	57	34	-1	-95	-139	-55	-10	-6	16	64	88	64	41	82	100
11	-10	33	8	-32	-41	-85	-122	-122	-71	5	54	42	1	10	52	63	58	110	176
172	125	142	81	-114	-242	-261	-248	-209	-112	-13	51	88	85	47	10	-2	-37	-99	-73
14	96	139	145	145	147	117	48	-26	-79	-106	-127	-150	-151	-114	-106	-128	-113	-61	11
99	176	165	123	105	72	30	-16	-72	-121	-105	-43	-7	39	101	101	-67	96	117	140
139	90	27	-32	-95	-156	-222	-246	-183	-107	-61	-18	-7	-47	-101	-116	-109	-77	-35	-46
119	101	107	139	168	198	220	212	194	157	71	-33	-100	-127	-135	-129	-109	-77	-35	-46
-88	-87	-66	-52	-38	-13	16	13	-22	-49	-48	-35	-23	-18	-26	-30	-13	14	32	25
9	-8	-9	-3	-17	-12	11	56	111	132	137	145	152	160	160	144	126	96	35	-20
-60	-97	-127	-151	-178	-191	-166	-130	-108	-94	-81	-84	-100	-113	-83	-11	48	79	91	85
53	15	-19	-43	-22	27	74	119	157	165	139	87	12	-29	-37	-50	-76	-108	-128	-112
-76	-48	-26	-6	15	33	49	59	62	65	78	94	93	78	61	44	36	44	57	73
76	60	37	8	-26	-69	-127	-167	-183	-194	-203	-210	-190	-139	-76	-8	53	94	130	159
177	194	203	186	160	104	31	-17	-55	-96	-119	-107	-86	-63	-30	8	36	29	5	-6
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165	151	136	118	99	89	89	87	72	47	15	-26	-62	-84	-84	-70	-53	-36	-29	-53
-90	-125	-153	-170	-154	-117	-81	-46	-6	23	35	44	54	63	73	83	93	99	84	56
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-17	-19	-28	-47	-47	-39	-18	0	0	-15	-22	-14	-2	6	10	11	13	10	5	0
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-14	-12	-9	-6	-4	-2	-7	-17	-28	-31	-17	3	21	41	55	51	1	35	7	-7
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188	103	11	-65	-113	-151	-188	-222	-263	-263	-197	-120	-37	44	128	201	242	266	241	197
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-170	-223	-280	-342	-394	-425	-454	-465	-469	-429	-395	-361	-315	-235	-143	-50	45	139	231	288
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42	85	142	174	163	142	107	72	34	-3	-31	-43	-59	-100	-150	-169	-168	-162	-156	-150
-143	-128	-108	-94	-87	-80	-83	-93	-95	-85	-67	-28	15	53	46	28	11	4	21	48
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-88	-95	-81	-61	-31	-3	24	49	47	32	16	24	57	67	49	26	5	33	73	77
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24	17	11	14	20	27	47	73	98	108	111	116	124	126	119	110	113	127	141	158

157	142	126	108	91	74	60	47	32	10	-15	-40	-64	-87	-109	-136	-161	-174	-177	-164
-148	-132	-120	-109	-100	-96	-97	-94	-87	-77	-67	-56	-45	-31	-17	-3	7	14	20	27
33	51	82	112	144	154	148	140	142	148	157	153	125	92	58	24	4	-6	-14	-22
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-96	-111	-128	-144	-141	-130	-116	-119	-133	-150	-163	-166	-167	-168	-166	-161	-156	-151	-146	-142
-136	-133	-131	-129	-127	-125	-122	-106	-83	-59	-34	-8	21	50	80	110	139	161	178	173
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11A303 52.001.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 475 PASADENA - CALTECH ATHENAEUM COMP S90W 34 08 20N, 118 07 17W
INSTR PERIOD = 0.0810 SEC DAMPING = 0.552 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -52.1 CM/SEC/SEC AT 16.70 SEC VELO = 9.1 CM/SEC AT 16.56 SEC DISP = -2.9 CM AT 18.52 SEC

INITIAL VELO = -0.01996 CM/SEC INITIAL DISP = -0.07693 CM

3869 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

19	-25	-24	-24	-17	-5	9	21	26	28	30	30	21	9	-3	-15	-17	-13	-7	-7
-11	-14	-9	-1	8	18	26	36	33	20	5	-5	-7	-8	-8	-8	-5	0	6	10
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-42	-34	-27	-23	-5	26	55	57	50	41	31	21	12	2	-8	-17	-11	3	18	34
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93	87	78	67	57	47	34	19	5	-10	-24	-39	-51	-63	-71	-70	-68	-64	-61	-57
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22	-5	-31	-56	-65	-67	-54	-24	1	-1	-12	-23	-18	-12	12	52	78	94	87	70
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474	479	474	444	362	271	174	80	-17	-112	-209	-303	-401	-479	-509	-521	-513	-507	-509	-516
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260	292	327	345	360	352	318	279	238	197	156	115	75	34	-7	-47	-72	-91	-112	-142
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IIA003 52-001.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 475 PASADENA - CALTECH ATHENAEUM COMP VERT 34 08 20N, 118 07 17W
INSTR PERIOD = 0.0820 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 29.3 CM/SEC/SEC AT 19.32 SEC VELO = -4.5 CM/SEC AT 24.90 SEC DISP = -3.0 CM AT 16.18 SEC

3865 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
INITIAL VELO = -0.10363 CM/SEC						INITIAL DISP = -0.08678 CM													
AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
46	-35	-39	-41	-38	-36	-24	12	57	88	71	48	46	50	56	52	28	4	-25	-43
-34	-20	-3	15	17	-20	-61	-87	-100	-99	-96	-79	-24	38	95	86	55	30	38	53
68	79	80	76	53	4	-43	-63	-76	-69	-41	-11	1	-13	-9	25	54	31	-4	-44
-61	-15	51	65	37	5	-19	-28	-38	-47	-55	-40	-27	-39	-49	-36	-16	7	25	10
-15	-9	12	38	45	25	3	-15	0	17	42	50	41	25	23	29	36	17	10	16
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2	-65	-81	-75	-120	-167	-180	-121	-66	-47	-30	10	48	80	105	134	108	48	-21	-72
-85	-46	-13	1	13	46	104	119	88	55	32	7	-33	-78	-105	-122	-120	-126	-83	31
156	182	146	113	112	126	110	12	-101	-210	-180	-114	-34	38	81	110	136	113	69	36
12	-12	-48	-89	-126	-138	-124	-96	-69	-47	-20	13	51	74	56	29	-11	-29	8	54
83	112	147	177	134	71	2	-68	-132	-123	-102	-118	-108	-61	-10	41	71	77	60	45
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24	0	-23	-2	29	47	43	37	4	-32	-74	-96	-80	-48	2	23	8	-4	3	35
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IIA004 52.002.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 095 TAFT LINCOLN SCHOOL TUNNEL COMP N21E 35 09 00N, 119 27 00W
INSTR PERIOD = 0.0810 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 152.7 CM/SEC/SEC AT 9.10 SEC VELO = -15.7 CM/SEC AT 3.40 SEC DISP = -6.7 CM AT 44.14 SEC

INITIAL VELO = 2.44204 CM/SEC INITIAL DISP = -0.78985 CM

2719 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-123	1	-4	30	41	21	19	36	-16	-61	-22	25	33	-3	2	15	35	28	14	-57
-112	-134	-117	-83	-21	57	58	46	41	47	67	145	192	204	146	43	-76	-132	-75	-16
40	47	18	-16	-85	-91	-47	7	52	20	-40	-37	-29	-46	-41	-25	-29	-64	-98	-70
-25	55	77	26	-18	-35	-24	90	175	137	40	-69	-173	-186	-145	-63	69	58	-62	-210
-226	-103	35	152	188	195	180	81	-25	-88	-147	-144	-114	-38	41	133	156	74	-10	-120
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-69	-92	-110	-164	-154	-56	67	137	73	15	54	78	47	37	84	151	206	197	178	155
172	229	231	217	246	293	312	256	202	176	144	48	-67	-167	-194	-180	-171	-166	-168	-170
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-151	-127	-123	-146	-179	-211	-261	-326	-365	-342	-280	-187	-74	-5	-8	-13	4	34	51	47
44	64	94	124	157	186	227	283	345	310	194	73	-62	-161	-206	-248	-284	-216	-116	-9
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156	129	78	26	56	129	210	285	257	191	123	81	46	-4	-55	-80	-51	-24	-76	-136
-164	-181	-210	-228	-242	-256	-255	-218	-162	-123	-143	-169	-180	-171	-134	-107	-112	-139	-148	-139
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-64	-56	-55	-53	-61	-20	57	133	118	68	30	19	-23	-96	-148	-100	-14	28	-37	-127
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23	41	14	-42	-22	62	128	111	71	70	97	102	88	93	118	127	77	10	-61	-114
-122	-78	-24	36	95	150	150	126	137	173	213	223	200	159	107	65	34	29	63	132
215	255	219	182	159	159	167	176	201	238	270	222	160	131	113	62	-12	-45	-25	49
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26	62	45	11	-16	-15	-9	-14	-19	-12	-10	-75	-155	-196	-198	-165	-127	-84	-43	-21
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-60	-81	-92	-109	-137	-166	-155	-119	-81	-38	0	47	45	-16	-91	-129	-90	-55	-39	-46
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-127	-140	-117	-96	-75	-48	-10	17	20	4	-14	-33	-34	-28	-13	13	34	22	0	-6
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-51	-9	30	72	92	92	89	84	78	82	100	121	115	84	57	47	57	70	75	87
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31	55	82	106	140	181	211	211	193	174	153	117	66	25	6	13	36	61	75	55
38	23	14	-15	-51	-62	-41	-10	2	3	8	30	49	60	67	55	42	32	22	4
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-72	-86	-88	-59	-20	22	63	91	87	65	39	22	20	18	17	1	-8	-14	6	49
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-95	-99	-95	-88	-82	-80	-79	-79	-69	-49	-30	-27	-45	-70	-88	-86	-77	-44	-6	35
68	62	23	-24	-54	-67	-62	-53	-52	-68	-86	-105	-105	-96	-85	-81	-81	-77	-65	-53
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-69	-68	-52	-32	-17	-8	-15	-34	-55	-78	-107	-133	-147	-135	-97	-61	-41	-28	-16	-4
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-91	-103	-92	-65	-32	-1	20	39	57	75	84	89	93	97	100	104	95	77	59	47
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99	103	96	89	82	80	75	59	40	19	-6	-32	-55	-59	-57	-54	-43	-25	-14	-8
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61	67	73	80	86	92	87	75	69	70	73	70	57	41	32	41	54	63	61	58
52	47	45	48	52	57	60	54	47	39	39	43	47	54	63	67	61	51	41	31
27	28	26	18	8	0	0	2	4	6	8	11	13	24	36	49	44	39	29	19

IIA004 52.002.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
 STATION NO. 095 TAFT LINCOLN SCHOOL TUNNEL COMPT VERT 35 09 00N, 119 27 00W
 INSTR PERIOD = 0.0800 SEC DAMPING = 0.552 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 102.9 CM/SEC/SEC AT 9.76 SEC VELO = 6.7 CM/SEC AT 7.80 SEC DISP = -5.0 CM AT 41.56 SEC

INITIAL VELO = -0.05273 CM/SEC INITIAL DISP = -0.16226 CM

2714 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

268	-49	33	-17	-34	66	218	284	134	-50	-277	-363	-207	3	228	317	194	4	-222	-346
-232	-52	149	320	190	17	10	153	325	364	393	370	86	-272	-553	-315	80	479	396	175
126	55	-175	-184	-69	72	-119	-312	-291	-252	-166	-72	-99	-356	-633	-525	-235	84	392	332
206	129	-8	1	281	596	924	764	374	-110	-364	-253	-59	8	-19	85	-1	-250	-457	-316
-8	134	44	-84	-95	-66	-156	-240	-294	-327	-229	-2	185	93	-104	-65	134	66	-96	-141
-70	-145	-327	-273	-58	-21	-138	-183	-165	-73	101	138	-16	-18	66	13	-61	19	103	32
-91	-231	-346	-238	-44	141	89	-48	-212	-334	-270	-144	-4	139	277	420	496	375	179	-27
-178	-132	91	425	456	133	-205	-167	88	358	350	79	-59	-92	-242	-373	-327	-182	-135	-114
-46	-67	-172	-277	-408	-400	-244	-63	117	148	61	74	343	589	367	-37	-408	-340	-121	138
384	391	175	94	231	350	335	310	280	86	-132	-391	-485	-277	-22	138	62	-143	-365	-339
-144	69	271	182	113	20	-59	-165	-113	148	403	357	79	-92	132	474	367	179	20	-246
-494	-68	-323	-187	-2	197	393	484	470	422	119	-242	-606	-435	-37	431	552	436	343	164
8	-40	-115	-254	-387	-342	-242	-156	41	291	497	315	-26	-130	-59	-133	-254	-139	156	479
475	204	158	157	-21	-290	-587	-754	-556	-275	8	13	-54	-142	-107	-58	46	-11	-152	-343
-204	164	582	504	235	-153	-382	-432	-476	-391	-88	-18	-77	-91	49	218	360	301	295	377
338	195	26	-75	-23	19	57	75	-45	-252	-451	-538	-544	-390	-100	38	47	35	73	164
239	315	409	538	563	372	128	-132	-391	-545	-604	-584	-435	-259	-64	86	87	142	275	207
37	-161	-181	-86	51	87	-76	-313	-407	-207	57	295	329	372	230	-114	-478	-812	-496	-179
45	355	620	562	392	185	27	-61	-180	-85	196	299	215	109	203	344	309	203	332	523
501	381	225	85	15	-44	14	121	257	276	87	-124	-379	-429	-47	194	25	-281	-460	-231
79	161	56	78	179	217	-8	-276	-573	-525	-291	-19	-51	-226	-472	-510	-237	-34	140	371
653	939	846	478	58	-304	-372	-377	-392	-347	-203	-50	118	166	68	31	131	256	162	-45
-255	-158	166	244	88	-118	-280	-277	-290	-307	-191	25	264	437	330	154	-71	-107	113	2
-256	-545	-475	-150	34	-61	64	327	502	377	236	154	141	67	5	-84	-232	-312	-358	-497
-687	-847	-804	-499	-140	248	624	997	1029	852	635	411	180	2	-60	-43	-3	41	96	99
126	132	69	-8	-127	-249	-386	-525	-647	-658	-445	-138	173	489	484	254	-17	-196	-231	-222
-135	51	288	411	334	281	346	306	142	-50	-141	-82	-21	101	141	17	-170	-351	-564	-595
-359	-180	-163	-252	-299	-58	274	611	559	294	107	-11	-189	-368	-534	-360	-140	-67	-46	68
212	314	-115	-348	-139	-360	-319	-208	-16	185	401	522	413	276	83	57	80	-42	-169	-283
-194	-58	96	165	202	68	-129	-329	-406	-453	-395	-235	-37	95	121	211	266	213	75	-103
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-241	-304	-190	-81	-25	99	267	351	239	110	54	85	140	162	138	111	76	241	370	2
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359	181	-1	-201	-263	-64	13	32	54	108	109	93	57	34	-71	-235	-399	-300	-54	222
-462	612	538	402	253	102	-17	-201	-308	-271	-195	-106	-6	104	214	234	177	110	37	-37
-86	-64	-38	-28	-39	-50	-15	10	-20	-61	-83	-98	-162	-222	-83	88	151	78	-67	-196
-254	-217	-101	-58	-34	89	250	305	241	209	281	366	271	87	-59	-106	-70	-36	-84	-150

-187	-79	76	188	122	15	-114	-180	-227	-235	-117	39	177	144	48	-40	-53	-42	-44	-68
-130	-161	-88	4	0	-41	-84	-31	54	161	198	128	36	-64	-163	-263	-344	-345	-330	-345
-400	-327	-156	24	65	35	19	34	3	-106	-148	-83	37	185	339	447	338	155	-2	-81
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132	64	-24	-73	-142	-210	-280	-340	-292	-190	-122	-79	-59	-71	-49	34	55	21	-26	-2
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-23	-68	-122	-183	-207	-186	-171	-155	-107	-41	-18	-43	-22	36	102	172	228	257	269	256
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-111	-103	-32	71	84	4	-98	-147	-84	3	76	82	105	110	56	-15	-87	-54	16	125
168	76	-48	-128	-88	-45	-43	-67	-56	-3	56	31	-46	-123	-163	-156	-124	-119	-98	-55
19	70	45	-2	-56	-107	-163	-235	-271	-236	-143	-49	-7	8	2	24	72	81	69	98
159	221	232	238	236	214	183	107	12	-105	-157	-97	-8	49	8	-42	-43	-64	-122	-148
-146	-90	-52	16	69	84	42	-22	-104	-181	-210	-132	-24	86	79	30	35	98	166	210
211	210	179	119	47	25	17	-35	-95	-100	-68	-48	-26	-3	17	31	30	19	11	12
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140	199	235	200	148	-138	-86	-59	-73	-134	-193	-223	-230	-227	-274	-254	-144	-9	78	87
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27	-3	-73	-131	-137	-98	-55	-46	-76	-80	-50	30	27	-45	-99	-119	-72	-19	22	2
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121	101	102	137	152	165	217	273	270	246	215	230	245	253	186	20	-134	-206	-198	-152
-196	-283	-351	-365	-311	-226	-138	-94	-82	-63	-38	-11	22	64	108	144	128	97	102	123
97	42	2	-26	-28	10	52	71	78	99	95	38	-53	-148	-215	-208	-146	-76	2	54
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77	72	54	33	-9	-57	-68	-41	-38	-70	-108	-113	-111	-117	-114	-106	-95	-86	-76	-76
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-58	-82	-79	-17	38	-104	-146	-170	-203	-187	-117	-62	-38	-19	-11	-31	-48	-27	10	17
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-49	23	75	92	54	-50	-174	-183	-176	-146	-117	-73	-12	52	33	-43	-111	-135	-99	-57
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22	31	40	52	72	63	41	25	8	-4	16	56	63	42	17	28	68	98	119	113
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-50	-52	-36	-18	-18	-35	-54	-68	-66	-73	-100	-131	-151	-136	-114	-109	-113	-110	-99	-86
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43	38	33	25	30	59	96	114	104	92	77	65	66	74	76	67	57	57	67	72
67	60	55	50	44	45	53	49	41	33	44	63	84	94	101	98	92	84	77	69
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-20	-26	-34	-40	-39	-38	-41	-38	-27	-16	-21	-32	-46	-57	-62	-65	-67	-64	-60	-54
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74	67	64	69	77	83	80	74	68	62	54	46	37	33	32	32	33	33	33	33
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IIA005 52.003.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 283 SANTA BARBARA COURTHOUSE COMP N42E 34 25 28N, 119 42 05W
INSTR PERIOD = 0.0640 SEC DAMPING = 0.495 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACEN = -87.8 CM/SEC/SEC AT 11.58 SEC VELO = -11.8 CM/SEC AT 17.10 SEC DISP = 4.6 CM AT 9.90 SEC

INITIAL VELO = -0.36310 CM/SEC		INITIAL DISP = 0.44127 CM		3775 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC															
-50	-31	-61	-80	-75	-63	-51	-39	-27	-15	-2	15	38	61	71	57	36	15	-2	2
22	28	9	-19	-36	-39	-38	-38	-23	17	37	10	-31	-71	-95	-94	-85	-77	-71	-61
-46	-22	16	29	13	-3	-9	2	18	32	29	9	-5	0	15	29	44	45	25	5
-1	11	32	53	73	94	106	95	74	53	31	7	-20	-27	-7	20	37	33	18	11
20	36	43	31	11	-8	-27	-36	-35	-33	-38	-53	-71	-75	-62	-37	8	63	97	104
91	59	19	-12	-25	-20	6	32	47	43	22	-7	-25	-11	12	28	34	27	15	4
-8	-12	5	32	58	86	96	62	21	1	-15	-24	-18	-9	-12	-23	-31	-30	-23	-17
-11	-2	16	33	31	-2	19	32	50	62	60	49	43	50	59	49	22	-8	-36	-54
-56	-55	-61	-78	-87	-65	-29	8	45	82	96	69	27	-15	-56	-97	-107	-72	-26	20
60	59	29	9	-3	-1	19	39	58	77	82	61	31	5	-19	-32	-23	-3	16	28
23	-1	-29	-58	-77	-65	-41	-17	7	31	48	38	13	-14	-33	-38	-38	-38	-38	-39
-43	-48	-37	-1	41	62	55	41	32	38	51	41	2	-42	-74	-92	-106	-119	-117	-102
-92	-81	-61	-52	-62	-62	-35	-52	16	36	56	75	96	100	77	51	32	13	-5	-27
-97	-92	-109	-93	-65	-44	-43	-52	-47	-31	-28	-39	-45	-25	9	45	65	52	28	4
-21	-45	-70	-87	-78	-55	-31	-7	10	-3	-34	-67	-85	-65	-29	-3	10	20	31	40
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338	334	335	343	338	320	287	233	174	115	49	-41	-145	-250	-355	-459	-565	-652	-696	-674
-535	-335	-132	69	274	446	519	521	504	466	403	332	261	191	117	6	-137	-284	-427	-518
-514	-450	-396	-365	-355	-371	-398	-381	-264	-107	47	204	357	516	584	460	264	73	-120	-307
-425	-456	-407	-301	-188	-84	-5	56	122	146	61	-77	-217	-343	-295	-64	172	318	404	484
532	519	501	513	487	413	336	258	168	59	-56	-167	-195	-117	-12	83	155	174	143	99
61	79	151	214	270	307	286	204	77	-66	-208	-351	-492	-635	-740	-781	-803	-809	-723	-570
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491	509	492	471	470	456	411	359	308	256	204	165	163	156	112	58	4	-44	-77	-91
-78	-44	-2	32	1	-88	-184	-279	-374	-469	-562	-627	-665	-699	-734	-764	-784	-793	-761	-675
-563	-449	-335	-222	-107	-12	35	44	28	8	15	45	65	65	60	73	100	130	144	116
70	25	-22	-64	-54	7	77	145	215	273	311	323	293	245	198	156	123	126	186	266
340	406	466	527	577	615	623	570	491	415	335	250	163	75	-11	-100	-174	-218	-226	-185
-118	-31	68	131	154	155	144	131	119	100	68	8	-96	-218	-337	-459	-578	-700	-812	-878
-861	-733	-557	-382	-207	-32	140	252	276	255	199	111	25	-36	-76	-105	-113	-94	-38	27
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-318	-248	-167	-99	-46	-4	17	22	28	32	44	79	127	146	116	53	-23	-99	-152	-175
-158	-110	-58	-7	44	92	120	131	140	146	149	148	134	113	92	71	50	28	-2	-43
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-459	-535	-577	-592	-606	-620	-634	-646	-649	-646	-659	-671	-652	-552	-344	-101	131	355	539	650
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133	106	78	67	81	93	88	75	80	111	150	175	174	164	158	161	188	229	271	312
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243	319	382	417	443	469	496	512	492	449	368	247	119	-6	-89	-133	-171	-183	-174	-162
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IIA005 52.03.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 CON, 119 02 00W
STATION NO. 283 SANTA BARBARA COURT HOUSE COMP VERT 34 25 28N, 119 42 05W
INSTR PERIOD = 0.366 SEC DAMPING = 0.523 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 43.6 CM/SEC/SEC AT 8.12 SEC VELU = 5.0 CM/SEC AT 9.78 SEC DISP = 2.2 CM AT 12.80 SEC

3779 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																					
INITIAL VELO = 0.13182 CM/SEC					INITIAL DISP = 0.38928 CM																
3779	INSTRUMENT	AND BASELINE	CORRECTED DATA IN	MM/SEC/SEC	AT EQUALLY-SPACED INTERVALS OF	0.02	SEC														
-32	-126	-196	-157	-32	103	97	6	187	145	91	101	126	93	-1	-76	-86	-57	-35	-36	-67	-113
-146	79	124	40	-62	-94	-56	-108	-35	-108	-142	-40	33	19	-28	-55	-75	-95	-90	-70	-69	
-33	18	47	12	-69	-55	-108	-62	-4	-108	-62	138	25	-99	-155	-108	-10	92	185	175	69	-29
66	196	199	77	-69	-156	-110	-14	83	160	83	160	166	137	148	194	178	109	-5	-125	-171	-76
-14	0	-68	-136	-166	-189	-198	-160	-81	3	3	3	166	137	148	194	178	80	-41	-129	-124	-71
-106	-74	-83	-124	-120	-91	-12	41	39	44	44	44	66	21	-84	-199	-292	47	10	-34	-94	-133
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148	178	162	127	105	88	90	81	-11	-123	-11	-123	-157	-108	-15	-86	-234	20	-29	-92	-143	-153
-136	-98	-42	3	-29	-112	-182	-165	-93	-16	-93	-16	15	-36	-111	-186	-234	-159	8	132	203	248
236	198	200	196	103	-18	-87	-130	-146	-104	-146	-104	-37	47	156	237	218	147	76	30	17	29
17	-48	-129	-198	-183	-102	-14	60	94	95	94	95	86	61	15	-22	-29	-19	-8	30	17	29
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303	289	190	85	-19	-108	-121	-61	16	80	16	80	105	81	44	21	5	-26	-84	-124	-124	-118
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IIA06 52.005.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - C453 PDT EPICENTER 35 00 00N, 119 02 00W
 STATION NO. 133 HOLLYWOOD STORAGE BASEMENT COMP SCOW 34 05 00N, 118 20 00W
 INSTR PERIOD = 0.0640 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -54.1 CM/SEC/SEC AT 13.28 SEC VELO = -6.1 CM/SEC AT 26.04 SEC DISP = -5.1 CM AT 35.80 SEC

4122 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
INITIAL VELO = 0.00336 CM/SEC						INITIAL DISP = -0.16435 CM													
-27	33	38	31	18	6	-6	-14	-7	10	26	40	36	21	6	-10	-20	-16	-6	3
9	2	-11	-23	-18	1	23	34	22	0	-16	-13	1	14	23	27	32	37	43	45
35	16	4	8	18	20	5	-18	-40	-62	-77	-66	-42	-18	5	44	55	43	7	-30
-21	-17	-34	-54	-42	-13	13	21	6	-11	-14	-4	9	20	32	-44	-38	-25	-12	-5
-69	-95	-73	-20	18	36	47	49	37	16	-11	-32	-39	-41	-43	33	46	54	50	32
-7	-13	-18	-22	-27	-31	-19	4	28	42	32	10	-4	2	18	22	33	35	29	24
11	-10	-31	-52	-64	-53	-34	-17	-4	-9	-23	-26	-15	-3	10	9	23	26	24	24
18	13	4	-21	-56	-75	-54	-15	23	51	44	17	-10	-31	-27	-9	66	86	84	59
24	33	46	59	55	21	-20	-58	-79	-86	-93	-98	-89	-58	-16	29	25	20	3	15
29	0	-26	-33	-26	-19	-13	-5	8	24	36	33	21	9	-3	-14	-25	-20	-3	15
19	0	-25	-49	-67	-80	-84	-75	-57	-33	-6	20	43	54	60	68	71	65	53	42
28	8	-14	-34	-56	-69	-57	-31	2	31	39	33	28	22	17	11	6	8	15	24
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-12	0	11	22	33	32	16	-5	-17	-14	-2	7	4	-10	-26	-38	-27	3	34	48
36	17	0	-8	-5	-4	-10	-18	-25	-15	10	38	56	48	29	14	2	-7	-17	-27
-36	-46	-55	-51	-22	13	41	56	64	73	80	68	34	-3	-40	-51	-26	8	39	73
89	63	23	-14	-51	-67	-61	-55	-64	-80	-97	-99	-75	-44	-15	16	43	43	21	-1
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-47	-28	0	24	26	7	-15	-30	-22	0	21	39	44	40	36	32	26	10	-13	-36
-59	-75	-64	-32	-43	23	15	-2	-7	5	22	19	-8	-40	-70	-77	-44	-1	41	59
-76	-72	-81	-92	-100	-99	-92	-85	-77	7	-17	-35	-52	-70	-87	-105	-120	-119	-105	-90
29	55	92	131	163	183	200	213	207	181	129	61	-7	-72	-102	-91	-75	-59	-52	-66
-86	-107	-111	-76	-28	17	58	82	98	93	67	40	14	-13	-37	-51	-32	8	50	72
50	13	-21	-56	-91	-119	-136	-137	-99	-43	13	48	44	30	21	52	127	201	246	254
224	173	121	83	68	61	52	43	35	37	52	68	89	116	141	135	102	68	34	26
54	90	125	160	193	189	142	89	37	-7	-20	-29	-77	-142	-207	-271	-334	-333	-248	-145
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-139	-166	-167	-147	-129	-144	-184	-226	-254	-184	-32	122	267	350	369	351	315	285	256	227
193	138	67	-4	-75	-145	-216	-286	-359	-388	-329	-248	-199	-171	-141	-100	-53	-7	12	-2
-21	-42	-73	-107	-142	-167	-167	-155	-149	-176	-232	-287	-342	-332	-225	-96	29	155	277	349
370	384	401	405	385	343	267	179	94	12	-2	63	124	158	164	131	86	46	-17	-127
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267	171	76	-19	-112	-170	-185	-194	-229	-288	-135	-335	-287	-214	-139	-64	2	36	52	78
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343	317	239	130	18	-76	-122	-128	-104	771	-45	-30	-18	-6	1	-26	-80	-129	-153	-141
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27	27	28	28	28	27	24	21	17	13	10	6	3	-1	-4	-6	-6	-7	-8	-9
-10	-10	-11	-12	-13	-14	-13	-11	-9	-7	-5	-3	-5	-10	-14	-19	-23	-27	-32	-36
-40	-45	-49	-54	-58	-62	-64	-63	-61	-60	-59	-57	-56	-55	-53	-52	-50	-47	-41	-35
-29	-23	-17	-11	-6	0	5	6	5	5	4	4	3	3	2	2	1	0	0	1
2	4	5	7	8	10	11	13	14	16	18	19	21	22	24	25	26	27	27	20
9	9	10	11	12	13	14	15	16	16	2	6	9	11	14	16	19	22	24	27
29	32	35	37	39	38	36	34	32	30	28	27	25	23	21	20	18	17	15	14
13	11	10	9	7	6	4	3	3	4	6	8	9	11	12	11	6	0	-6	-12

[illegible]

IIA006 52.015.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 133 HOLLYWOOD STORAGE BASEMENT COMP NO. 34 05 00N, 118 20 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.552 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
PEAK VALS ACCLN = 43.5 CM/SEC/SEC AT 12.92 SEC VELO = 9.4 CM/SEC AT 13.66 SEC DISP = -5.9 CM AT 12.50 SEC

INITIAL VELO = -0.54775 CM/SEC										INITIAL DISP = -0.48473 CM									
4125 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC										AT EQUALLY-SPACED INTERVALS OF 0.02 SEC									
-29	109	91	45	13	-4	-8	0	15	27	23	4	-17	-34	-33	-21	-17	-21	-16	0
18	35	39	28	15	2	-4	-7	-7	-3	3	9	15	21	27	29	18	-2	-16	-13
-2	8	19	30	38	33	18	1	-18	-38	-46	-43	-36	-24	0	35	61	60	44	29
14	-2	-17	-18	-2	18	37	56	59	36	6	-23	-35	-23	-5	11	29	41	38	26
13	1	-10	-14	-13	-11	-14	-11	-14	-17	-17	-14	-10	-7	-4	0	3	6	9	8
1	-8	-21	-38	-45	-33	-14	5	17	11	-7	-21	-23	-19	-15	-4	13	29	30	20
-23	-46	-60	-54	-39	-25	-11	3	55	42	24	7	-8	-9	-2	6	14	22	18	-2
19	20	10	-7	-24	-41	-58	-71	-63	-44	-25	5	-3	-15	-24	-21	-10	1	10	15
31	28	10	-15	-39	-42	-26	-7	11	29	42	49	46	34	19	4	-10	23	25	28
5	21	33	29	18	14	17	19	5	-23	-51	-80	-94	-80	-58	-37	-20	-6	8	18
10	-11	-33	-49	-40	-16	9	31	47	47	28	2	-20	-33	-31	-14	7	28	49	68
65	46	25	7	-9	-23	-38	-52	-59	-60	-61	-62	-51	-22	-1	-6	-20	-32	-41	-45
-50	-49	-33	-5	29	65	90	82	59	36	14	-9	-25	-24	-15	-1	17	33	33	21
9	-2	-12	-22	-32	-34	-30	-34	-47	-60	-60	-49	-36	-24	-18	-18	-20	-21	-23	-24
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-59	-24	20	52	63	54	25	-7	-39	-54	-46	-33	-25	-27	-33	-29	-14	4	12	7
-2	-10	-18	-27	-31	-16	11	39	63	77	86	88	75	57	39	20	0	-19	-18	4
25	23	5	-13	-30	-45	-59	-76	-95	-114	-113	-76	-29	18	52	55	42	12	-30	-65
-88	-93	-78	-43	3	51	93	115	117	98	70	41	13	-16	-43	-49	-37	-33	-42	-48
-40	-26	-20	-26	-36	-37	-33	-29	-26	-15	14	50	75	66	40	14	-10	-22	-13	7
27	44	45	35	26	30	50	72	95	111	99	67	37	15	-3	-25	-49	-71	-66	-39
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81	93	116	154	194	236	257	239	209	181	148	107	62	17	-27	-72	-117	-143	-140	-130
-121	-111	-95	-60	-24	-14	-19	-24	-29	-35	-44	-54	-64	-69	-62	-49	-37	-17	11	39
37	11	-16	-42	-61	-75	-95	-121	-145	-146	-121	-93	-79	-87	-98	-100	-91	-80	-67	-40
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-92	-98	-110	-126	-141	-137	-112	-84	-55	-39	-57	-92	-126	-161	-177	-162	-138	-118	-103	-94
-83	-78	-89	-107	-125	-145	-166	-180	-168	-144	-107	-38	43	124	204	285	349	327	250	170
92	12	-66	-148	-196	-163	-95	-29	37	103	169	236	281	261	212	164	115	70	67	102
141	178	217	240	245	244	244	248	269	300	333	320	230	119	10	-98	-211	-286	-259	-187
-106	1	119	237	352	423	435	417	337	193	57	-9	-12	15	69	124	151	156	143	113
76	38	2	-17	-19	-21	-16	-5	10	15	-9	-50	-90	-131	-123	-48	43	111	141	133
104	73	41	1	-42	-86	-101	-60	-1	56	108	98	36	-28	-92	-144	-177	-202	-210	-210
-207	-204	-213	-242	-269	-285	-300	-316	-330	-330	-299	-236	-156	-76	-117	69	117	135	118	93
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73	31	-17	-52	-66	-58	-35	-10	8	14	17	17	-5	-42	-78	-105	-121	-117	-101	-66
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294	229	152	77	0	-75	-152	-209	-193	-137	-81	-25	32	79	83	58	30	17	44	89
133	177	221	238	217	188	155	109	56	3	-45	-58	-44	-29	-14	0	-2	-22	-46	-90
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113	165	190	187	144	71	-6	-81	-144	-197	-249	-303	-346	-367	-361	-337	-310	-284	-268	-259
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270	261	195	126	59	-10	-67	-58	-2	56	114	172	231	255	222	172	128	101	86	88
106	131	158	184	210	223	214	200	187	179	181	185	190	195	211	239	271	296	299	289
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28	16	-12	-38	-57	-71	-85	-100	-114	-127	-141	-160	-183	-205	-212	-208	-197	-176	-144	-104
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88	84	112	152	190	228	226	175	112	51	-11	-73	-131	-146	-118	-85	-52	-19	13	46
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139	131	114	99	83	68	52	41	41	47	52	58	54	23	-21	-64	-108	-151	-192	-229
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-294	-315	-320	-302	-269	-219	-164	-109	-54	-7	16	27	39	51	66	92	124	148	163	172
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127	110	93	75	58	40	24	28	48	71	93	114	125	122	115	109	103	97	90	78
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39	42	41	38	35	31	28	25	22	19	16	16	20	24	28	32	32	30	28	26
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IIA006 52.005.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 133 HOLLYWOOD STORAGE BASEMENT COMP VERT 34 05 00N, 118 20 00W
INSTR PERIOD = 0.0650 SEC DAMPING = 0.621 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 22.5 CM/SEC/SEC AT 21.98 SEC VELO = -4.2 CM/SEC AT 11.52 SEC DISP = -2.2 CM AT 12.22 SEC

4131 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC														
INITIAL VELO = -0.59727 CM/SEC					INITIAL DISP = -0.19824 CM									
-49	-2	-59	-46	12	9	-38	-9	100	112	23	2	26	-27	-34
31	42	0	-40	-30	8	28	9	-25	-30	5	52	78	68	45
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36	6	-48	-53	-26	-1	23	10	-34	-37	-6	14	11	-4	-16
42	30	20	9	2	9	13	-2	-1	26	37	13	-20	-49	-56
-35	-20	34	48	23	0	-23	-45	-62	-62	-25	20	37	46	54
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IIAC07 52.006.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 135 HOLLYWOOD STORAGE P.E. LOT COMP S00W 34 05 00N, 118 20 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -58.1 CM/SEC/SEC AT 13.30 SEC VELO = -6.6 CM/SEC AT 26.10 SEC DISP = -4.5 CM AT 35.90 SEC

INITIAL VELO = -0.44253 CM/SEC INITIAL DISP = 0.09634 CM

3932 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

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IIIC07 52.006.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT
STATION NO. 135 HOLLYWOOD STORAGE P.E. LOT
INSTR PERIOD = 0.0660 SEC DAMPING = 0.574
ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
EPICENTER 35 00 00N, 119 02 00W
COMP N9GE 34 05 00N, 118 20 00W

PEAK VALS	ACLN =	41.2	CM/SEC/SEC AT 12.98 SEC	VELD =	8.9	CM/SEC AT 13.20 SEC	DISP =	6.4	CM AT 14.62 SEC
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INITIAL VELO = 0.72119 CM/SEC
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3332 INSTRUMENT AND BASELINE CORRECTED DATA IN										MM/SEC/SEC										AT EQUALLY-SPACED INTERVALS OF										0.02										SEC									
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-19	-7	-3	-13	-29	-43	-58	-72	-87	-89	-81	-49	2	14	0	-8	-13	-17	-20	-13																														
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96	118	77	32	14	3	-8	-19	-29	-32	-9	32	83	135	139	98	58	41	43	58																														
75	82	80	96	139	191	231	230	204	179	153	125	95	39	-30	-82	-112	-115	-109	-107																														
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[illegible]

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37	37	38	40	41	42	40	33	11	7	4	1	-2	-6	-10	-16
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9	12	13	3	-1	-4	-8	-15	-19	-20	-24	-32	-43	-49	-50	-49
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44	50	56	54	51	48	45	39	33	30	28	25	22	19	16	13

IIAC07 52.066.0 KERN COUNTY, CALIFORNIA EARTHQUAKE JULY 21, 1952 - 0453 PDT EPICENTER 35 00 00N, 119 02 00W
STATION NO. 135 HOLLYWOOD STORAGE P.E. LOT COMP VERT 34 05 00N, 118 20 00W
INSTR PERIOD = 0.0650 SEC DAMPING = 0.552 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS		ACLN = -20.3 CM/SEC/SEC AT 18.06 SEC		VELO = 3.0 CM/SEC AT 13.12 SEC		DISP = -3.4 CM AT 50.38 SEC													
		INITIAL VELO = 0.49672 CM/SEC		INITIAL DISP = 0.12528 CM															
3930 INSTRUMENT AND BASELINE CORRECTED DATA IN		MM/SEC/SEC		AT EQUALLY-SPACED INTERVALS OF		0.02 SEC													
-13	-9	-59	-35	4	-21	8	111	117	-4	-54	-1	-23	-3	67	-10	-77	-7	53	32
-27	-77	-47	25	47	-5	-60	-26	50	95	61	-4	-1	18	-20	-58	-52	-27	-1	49
70	-2	-97	-63	52	35	-78	-150	-75	36	27	3	5	6	3	23	44	9	-81	-140
-60	54	53	14	-18	-64	-34	44	34	-37	-62	-24	8	-1	8	47	31	0	25	42
21	45	39	-51	-81	18	60	-10	-55	-65	-67	-28	25	-2	-80	-65	-7	-10	17	99
85	-18	-66	-66	-66	-67	-16	54	63	24	19	61	71	43	0	-20	0	-21	-53	-54
-38	3	34	35	22	1	-16	15	48	22	-15	21	58	-23	-73	-33	-26	-46	17	71
-5	-78	-20	79	94	71	55	47	47	43	34	22	9	2	24	64	59	4	-27	-26
-35	-80	-107	-93	-81	-43	5	11	-6	-23	-37	-18	11	-8	-66	-89	-56	-46	-44	-4
2	0	37	72	92	114	108	54	-31	-31	69	75	0	-30	-25	-19	-12	0	0	-28
-62	-47	-8	-11	-12	7	-9	5	105	138	42	-39	-15	-3	-48	-51	-19	-29	-55	-45
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IIA008 54.003.0 EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST
 STATION NO. 022 EUREKA FEDERAL BLDG
 INSTR PERIOD = 0.0670 SEC DAMPING = 0.621
 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
 EPICENTER 32 38 00N, 117 07 00W
 COMP N11W 40 48 00N, 124 09 00W

PEAK VALS	ACLN = 164.5 CM/SEC/SEC AT 4.84 SEC	VELO = -31.6 CM/SEC AT 3.44 SEC	DISP = 12.4 CM AT 2.92 SEC																	
3899	INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC	INITIAL DISP = -2.14906 CM	AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																	
	INITIAL VELO = -2.03055 CM/SEC																			
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IIA008 54.003.0 EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST EPICENTER 32 38 00N, 117 07 00W
STATION NO. 022 EUREKA FEDERAL BLDG COMP N79E 40 48 00N, 124 09 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -252.7 CM/SEC/SEC AT 3.84 SEC VELO = 29.4 CM/SEC AT 3.72 SEC DISP = 14.1 CM AT 4.22 SEC

INITIAL VELO = -0.53800 CM/SEC INITIAL DISP = 0.16794 CM

3979 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

225	-163	-122	-96	-62	-13	14	-17	-56	-79	-98	-119	-139	-166	-171	-150	-115	-117	-160	-199
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180	166	163	192	159	57	-46	-150	-226	-225	-192	-153	-61	77	173	151	95	123	207	264
262	249	212	101	-47	-104	-50	-41	-82	-22	-116	147	84	44	123	192	208	222	270	327
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100	102	100	93	86	79	72	65	59	52	45	41	38	35	32	29	26	23	19	11
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-100	-91	-82	-73	-65	-56	-50	-48	-45	-43	-40	-35	-28	-20	-12	-4	3	11	19	27
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IIAOC9 54.004.0
STATION NO. 023
INSTR PERIOD = 0.0640 SEC DAMPING = 0.621
EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST
FERDALE CITY HALL
ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
EPICENTER 32 38 00N, 117 07 00W
COMP N46W 40 34 00N, 124 15 00W

PEAK VALS ACLN = 197.3 CM/SEC/SEC AT 7.10 SEC VELO = -26.0 CM/SEC AT 6.88 SEC DISP = -9.6 CM AT 7.10 SEC

INITIAL VELO = 0.99049 CM/SEC INITIAL DISP = 0.53365 CM

2120 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-44	-12	-16	4	25	32	-5	-49	-38	3	-21	-67	-36	0	-20	-53	-52	-28	-9	-2
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25	12	-40	-73	-49	-26	-24	-27	-100	-129	-73	-22	2	8	-22	-60	-52	48	162	159
87	21	-47	-91	-49	39	123	139	68	-16	-38	13	78	89	11	-88	-181	-207	-134	-40
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36	42	43	44	44	34	16	-2	-19	-37	-55	-72	-90	-108	-121	-128	-134	-139	-139	-137
-135	-134	-129	-122	-114	-107	-99	-92	-84	-77	-69	-62	-54	-47	-39	-31	-24	-16	-9	-1
6	14	22	30	38	46	54	63	69	69	68	67	66	65	64	62	61	60	59	58
57	56	55	54	52	51	50	50	53	60	66	72	78	84	84	81	77	74	70	67
63	60	56	53	49	46	42	39	36	33	32	32	33	34	34	35	35	36	37	37
38	37	35	32	30	27	24	21	18	16	13	10	7	4	0	-6	-12	-18	-24	-30
-36	-42	-48	-54	-59	-63	-66	-69	-72	-75	-78	-81	-84	-87	-90	-93	-96	-100	-101	-99
-94	-90	-85	-78	-68	-58	-48	-38	-28	-18	-8	2	12	22	32	42	52	63	72	83
91	94	96	98	99	96	93	90	87	84	81	78	75	73	70	67	63	55	41	28
14	1	-4	-4	-4	-4	-4	-4	-4	-4	-2	2	5	9	12	16	19	20	17	13
10	6	2	-1	-5	-8	-12	-15	-19	-23	-28	-36	-44	-52	-63	-68	-75	-83	-91	-98
-99	-99	-100	-100	-100	-100	-98	-96	-94	-92	-90	-85	-78	-72	-65	-58	-52	-45	-38	-32
-25	-18	-12	-5	2	7	7	3	0	-3	-6	-9	-13	-16	-19	-22	-25	-25	-17	-8
1	10	17	22	27	32	37	42	46	51	56	61	65	71	75	81	83	92	87	82

IIAC09 54.004.0 EUREKA EARTHQUAKE DEC 21, 1954 - 1156 PST EPICENTER 32 38 00N, 117 07 00W
STATION NO. 023 FERNDAL CITY HALL COMP VERT 40 34 00N, 124 15 00W
INSTR PERIOD = 0.0660 SEC DAMPING = 0.632 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -41.9 CM/SEC/SEC AT 8.00 SEC VELO = 7.6 CM/SEC AT 15.02 SEC DISP = 3.9 CM AT 8.04 SEC

2108 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
INITIAL VELO = 0.59185 CM/SEC										INITIAL DISP = 0.10178 CM									
-14	-58	-56	-41	18	83	99	114	51	-4	-64	-155	-184	-118	-48	-58	-63	-85	-95	-16
31	42	21	-49	-104	-161	-167	-87	-8	59	68	36	40	108	184	176	76	4	-22	-25
-39	-45	-9	-23	-68	-48	-17	-3	7	-3	-24	1	52	37	7	6	34	40	-24	-42
113	48	32	4	-20	-51	-72	-68	-52	-67	-69	-19	21	37	0	-53	-84	-49	20	84
103	82	89	125	157	162	148	134	101	50	-2	-50	-52	-15	-23	-54	-53	-13	71	85
14	-56	-60	21	67	-9	-116	-127	-68	-4	74	89	25	-55	-88	-24	65	83	47	-1
-56	-58	7	47	11	-45	-98	-110	-63	-1	42	20	-41	-39	38	112	74	-30	-90	-115
-119	-113	-103	-60	-7	0	-5	-2	-6	-3	7	57	110	84	16	-41	-81	-118	-115	-43
45	89	76	52	31	17	27	29	7	6	28	28	35	62	60	26	20	55	74	70
65	57	76	84	83	72	59	30	-19	-56	-42	0	39	79	87	51	17	22	35	27
9	-7	-24	-24	-7	-6	-28	-52	-70	-50	-1	42	45	16	-6	21	73	72	37	-4
-37	-48	-61	-81	-100	-120	-139	-159	-172	-139	-71	-37	-69	-112	-159	-153	-65	-13	2	28
63	107	121	78	19	-33	-48	-29	-8	9	7	-7	-21	-25	-7	19	37	21	-21	-41
-11	36	81	107	96	76	58	40	15	-20	-60	-74	-11	85	178	206	147	77	38	15
0	-4	7	51	109	166	218	228	198	148	77	5	-69	-113	-84	-29	15	52	87	129
83	0	-38	-49	-62	-76	-87	-60	4	52	75	93	71	4	-70	-135	-155	-141	-130	-118
-119	-149	-190	-212	-173	-116	-104	-121	-127	-86	-9	33	8	-23	-44	-80	-128	-172	-143	-54
36	75	56	27	20	48	83	75	48	65	109	145	177	204	185	151	142	135	163	225
247	221	153	65	-24	-92	-92	-56	-37	-76	-144	-213	-249	-186	-77	13	32	9	-11	34
147	209	229	246	234	207	180	155	119	64	24	7	-10	-35	-97	-169	-222	-271	-322	-372
-419	-411	-356	-326	-313	-296	-254	-219	-229	-232	-226	-209	-174	-145	-130	-73	20	52	71	110
116	101	115	152	175	190	206	226	239	254	290	256	182	192	202	174	146	96	27	-43
-111	-181	-249	-320	-367	-361	-337	-289	-216	-142	-68	-2	45	101	149	165	170	163	147	131
116	93	46	-8	-65	-97	-82	-52	-29	-30	-57	-59	-12	21	27	52	75	68	56	43
21	-6	-24	-24	-26	-38	-17	8	12	12	17	9	4	15	47	71	78	97	108	115
136	163	190	216	241	239	217	197	169	115	48	-18	-85	-141	-171	-190	-201	-194	-166	-126
-84	-49	-26	-12	-20	-35	-35	-27	-28	-47	-72	-88	-96	-98	-93	-85	-81	-88	-102	-92
-46	9	54	80	109	150	195	225	225	213	201	155	107	72	15	-55	-105	-135	-172	-188
-186	-186	-186	-194	-208	-218	-213	-189	-149	-106	-73	-64	-57	-33	0	26	33	34	36	37
30	16	10	18	29	40	43	32	19	18	23	30	41	60	94	131	149	153	157	162
166	171	175	181	177	145	98	56	30	14	-3	-19	-36	-53	-69	-86	-95	-90	-88	-95
-103	-102	-88	-71	-55	-37	-3	46	82	95	105	115	134	161	190	210	204	183	164	145
126	107	88	69	51	33	15	-3	-21	-38	-43	-39	-34	-34	-38	-44	-48	-51	-49	-40
-26	-14	-1	12	25	34	35	35	35	27	11	-6	-23	-40	-57	-74	-91	-108	-125	-142
-159	-176	-193	-210	-228	-245	-261	-265	-257	-249	-242	-231	-213	-194	-175	-161	-155	-150	-145	-140
-134	-121	-97	-72	-47	-22	2	30	69	113	157	200	244	287	332	368	382	384	388	392
396	392	374	352	331	307	278	248	219	189	159	129	99	75	58	43	27	16	14	16
18	19	21	28	40	51	57	53	48	40	22	-2	-25	-48	-71	-94	-117	-138	-155	-171
-188	-204	-220	-232	-238	-244	-248	-241	-224	-208	-192	-179	-173	-172	-170	-168	-166	-165	-163	-161
-161	-162	-162	-163	-155	-137	-117	-98	-79	-59	-42	-34	-26	-12	5	22	39	56	73	90

107	124	141	158	164	152	137	124	114	107	100	92	86	83	79	79	83	89	98	118
139	160	182	203	224	245	265	282	272	239	205	177	158	141	123	103	79	54	30	5
-20	-44	-67	-82	-93	-104	-113	-118	-122	-127	-132	-137	-141	-146	-151	-156	-162	-169	-176	-183
-190	-197	-200	-195	-187	-180	-176	-180	-186	-191	-196	-201	-207	-210	-204	-193	-182	-171	-160	-149
-137	-120	-101	-82	-63	-43	-24	-5	14	33	52	71	90	109	128	147	164	163	149	136
123	110	97	84	70	59	55	53	52	50	51	60	72	84	93	95	97	98	98	92
84	77	75	77	78	79	80	82	83	85	91	98	106	113	120	128	135	142	140	130
120	109	99	88	78	68	56	42	28	16	11	9	8	11	16	20	25	27	28	29
30	27	22	16	9	-10	-39	-67	-95	-117	-128	-138	-148	-149	-141	-134	-124	-105	-84	-63
-42	-22	-10	-5	-1	-2	-7	-13	-23	-34	-46	-58	-69	-81	-92	-104	-111	-116	-120	-122
-120	-117	-115	-112	-109	-106	-100	-91	-81	-72	-63	-53	-46	-46	-49	-52	-56	-55	-47	-36
-25	-14	-3	7	18	27	31	33	36	38	40	42	42	38	33	29	25	20	16	16
-16	-9	-2	4	11	18	24	31	38	44	51	58	64	71	78	84	89	87	83	80
77	74	71	68	64	61	58	55	52	47	39	29	20	13	0	-5	-1	6	12	18
24	30	36	40	35	29	23	16	10	4	-2	-9	-15	-21	-27	-34	-40	-46	-53	-64
-76	-88	-101	-112	-125	-134	-134	-130	-128	-125	-122	-120	-117	-114	-107	-95	-82	-70	-58	-48
-44	-39	-35	-30	-25	-14	-2	11	23	35	47	60	72	84	97	109	118	125	133	139
138	134	130	127	123	119	116	111	101	88	74	60	46	33	25	22	20	17	15	12
10	7	5	4	6	10	13	16	19	22	25	29	33	37	42	45	46	45	43	40
33	23	14	7	5	4	2	0	-5	-14	-24	-33	-42	-45	-40	-35	-30	-25	-20	-15
-11	-10	-11	-13	-14	-17	-21	-27	-32	-37	-42	-47	-52	-57	-62	-66	-66	-64	-61	-59
-57	-55	-52	-50	-48	-45	-43	-41	-38	-36	-34	-32	-29	-27	-25	-22	-20	-18	-16	-16
-17	-18	-18	-19	-19	-20	-20	-21	-22	-22	-23	-23	-24	-24	-20	-16	-12	-8	-4	-1
3	7	11	15	19	23	27	31	35	37	37	38	39	39	40	40	41	42	42	43
43	44	45	45	46	46	44	41	38	35	32	30	30	31	31	32	33	34	35	36
37	38	39	41	43	45	47	49	51	50	46	40	35	30	25	20	15	10	5	0
-5	-8	-7	-2	4	14	26	37	49	61	72	83	86	83	81	78	73	66	58	51
43	35	28	20	13	5	-1	-2	0	2	4	6	8	10	11	7	1	-4	-9	-14
-19	-24	-29	-34	-39	-45	-50	-55	-60	-65	-70	-75	-80	-85	-90	-96	-101	-106	-111	-116
-120	-122	-124	-125	-126	-125	-124	-123	-122	-119	-112	-103	-95	-87	-79	-71	-63	-55	-47	-39
-31	-23	-15	-7	-1	2	6	9	12	15	19	22	25	29	32	35	39	42	45	49
51	51	51	50	50	49	49	48	48	47	47	46	46	45	45	44	44	43	43	42
42	42	41	41	45	49	54	58	63	64	57	48	39	29	20	12	6	1	-4	-7
-6	-5	-3	-1	0	2	3	4	0	-3	-7	-10	-14	-18	-21	-25	-27	-28	-29	-29
-30	-30	-31	-31	-32	-32	-33	-33	-34	-34	-35	-35	-36	-36	-37	-37	-38	-38	-37	-37
-36	-35	-34	-33	-30	-21	-9	0	4	7	8	5	-1	-8	-14	-21	-27	-34	-40	-47
-53	-58	-57	-54	-51	-48	-45	-42	-39	-36	-33	-30	-27	-24	-21	-18	-15	-12	-9	-5
4	16	28	40	52	64	76	83	85	86	85	81	74	67	60	53	46	44	47	51
55	59	63	67	71	70	64	58	52	46	40	34	28	24	21	18	16	13	10	8
5	2	0	-3	-6	-8	-11	-15	-18	-21	-24	-27	-30	-34	-37	-40	-43	-46	-50	-52
-52	-49	-46	-43	-41	-38	-35	-32	-30	-27	-24	-21	-18	-16	-13	-10	-7	-5	-2	1
4	7	9	12	15	18	20	23	26	29	32	34	37	37	35	32	29	26	23	20
17	14	11	8	5	2	-1	-4	-7	-10	-13	-16	-19	-22	-25	-27	-25	-23	-21	-19
-16	-14	-14	-16	-18	-20	-22	-24	-26	-28	-30	-32	-34	-36	-38	-40	-42	-42	-40	-37
-34	-31	-28	-25	-22	-18	-15	-12	-10	-8	-6	-5	-4	-2	-1	0	3	6	10	13
17	20	24	27	31	34	38	41	45	45	43	40	37	34	31	28	25	22	20	17
14	11	8	5	2	-1	-3	-6	-9	-11	-11	-10	-9	-8	-7	-5	-4	-3	-3	-5
-7	-9	-11	-14	-16	-18	-20	-20	-18	-15	-12	-10	-7	-4	-2	1	4	6	9	12
14	17	20	22	25	28	30	32	34	35	37	38	40	40	37	33	28	24	20	15

11	7	3	-2	-4	-5	-6	-7	-7	-8	-9	-9	-10	-11	-11	-12	-12	-13	-14
-14	-15	-16	-16	-17	-18	-18	-17	-14	-11	-8	-5	-3	0	3	6	7	7	2
7	6	6	6	6	7	8	9	11	12	13	11	10	9	7	4	3	3	2
0	0	2	4	6	8	11	15	17	19	22	24	26	28	30	29	27	25	23
22	20	18	17	15	13	14	15	16	16	17	18	19	20	21	22	23	24	24
23	20	16	13	10	7	0	-3	-7	-10	-13	-16	-19	-19	-16	-14	-11	-9	-7
-4	-2	1	3	5	8	3	-1	-5	-8	-12	-16	-19	-23	-27	-30	-34	-38	-40
-41	-41	-41	-41	-41	-42	-42	-42	-42	-42	-43	-43	-43	-42	-41	-41	-40	-39	-38
-38	-37	-36	-35	-35	-34	-31	-22	-18	-13	-9	-5	-3	-2	-1	0	1	2	2
4	6	9	12	15	17	20	25	28	31	31	28	26	24	22	20	17	15	13
11	9	6	4	2	0	-2	-6	-8	-9	-11	-12	-13	-15	-16	-17	-16	-14	-13
-11	-9	-7	-6	-4	-3	-4	-5	-5	-6	-7	-7	-8	-8	-9	-9	-10	-7	-3
1	5	10	14	18	23	27	31	37	36	36	36	36	35	35	35	35	34	34
34	33	33	33	33	32	32	31	29	27	25	23	22	20	18	16	14	13	11
9	7	5	3	2	0	-2	-4	-6	-9	-11	-13	-15	-17	-19	-20	-22	-24	-26
-27	-29	-31	-33	-35	-37	-32	-6	-8	-9	-11	-13	-15	-17	-19	-20	-22	-24	-26

IIAC12 55.001.0
STATION NO. 081
INSTR PERIOD = 0.660 SEC DAMPING = 0.528
SAN JOSE EARTHQUAKE SEPT 4, 1955 - 1801 PST
SAN JOSE BANK OF AMERICA BASEMENT
ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
EPICENTER 37 22 00N, 121 47 00W
COMP N59E 37 20 00N, 121 53 00W

PEAK VALS ACCLN = 105.8 CM/SEC/SEC AT 1.20 SEC VELO = -4.4 CM/SEC AT 1.14 SEC DISP = -1.7 CM AT 5.10 SEC

INITIAL VELO = -0.21293 CM/SEC INITIAL DISP = 0.83694 CM

2588 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

72	-110	-191	-257	-206	-76	58	193	297	283	206	121	74	120	179	80	-134	-349	-414	-325
-230	-122	29	188	342	409	382	293	139	-31	-204	-326	-304	-220	-257	-378	-303	-53	204	472
622	474	196	-78	-359	-594	-499	-144	235	566	535	227	-111	-431	-781	-914	-604	-131	317	796
1058	797	303	-182	-668	-858	-624	-286	54	308	350	260	83	-131	-160	15	247	366	244	17
-131	-95	16	53	33	6	-41	-64	-22	21	-1	-49	-33	34	74	28	-54	-143	-182	-115
-24	34	85	128	93	-6	-59	-67	-18	82	200	239	112	-75	-227	-186	-39	-1	-27	-12
44	90	101	86	45	-15	-79	-144	-204	-207	-155	-70	34	140	239	246	163	65	-23	-87
-141	-180	-196	-192	-128	-18	96	203	226	188	152	77	-40	-154	-178	-126	-80	-47	-4	46
97	146	197	218	179	122	71	27	-18	-49	-35	0	-2	-29	-59	-61	-26	21	49	12
-66	-148	-222	-200	-83	50	167	177	102	21	-44	-70	-64	-32	16	46	48	20	-48	-117
-142	-86	14	119	186	181	125	55	-19	-63	-31	27	5	-74	-128	-133	-108	-25	56	73
57	22	-29	-60	-58	-30	29	104	173	159	70	-21	-62	-43	14	46	3	-68	-93	-81
-64	-41	-83	4	-26	-73	-116	-136	-129	-123	-77	60	214	293	303	291	271	216	137	56
-24	-106	-163	-154	-117	-83	-43	-6	32	58	39	-10	-57	-57	-12	40	51	12	-40	-91
-140	-153	-125	-87	-51	-13	23	60	66	36	-6	-20	32	114	172	199	202	191	162	96
26	-16	-45	-75	-95	-84	-51	-35	-57	-91	-108	-118	-109	-67	-11	27	25	7	6	25
48	60	64	69	83	106	115	96	68	40	11	-23	-58	-82	-91	-96	-84	-51	-10	31
69	78	60	40	40	67	99	133	143	109	60	15	-22	-56	-90	-124	-159	-193	-228	-252
-241	-208	-158	-99	-39	21	79	102	90	70	68	92	125	148	132	89	50	23	2	-19
-40	-45	-35	-22	-9	4	13	10	5	8	14	11	1	-11	-23	-36	-48	-59	-58	-38
-15	8	19	21	21	24	28	30	27	25	27	31	35	39	38	22	-1	-23	-44	-55
-59	-65	-81	-103	-125	-138	-126	-99	-72	-34	22	81	140	188	208	199	173	142	118	98
78	58	42	37	39	40	42	35	7	-29	-65	-101	-135	-157	-166	-165	-155	-134	-106	-77
-49	-20	8	36	65	92	104	84	44	-1	-47	-85	-104	-103	-90	-74	-57	-41	-33	-37
-48	-60	-72	-83	-89	-88	-82	-67	-41	-5	38	82	126	166	183	166	122	70	17	-35
-74	-95	-110	-117	-112	-105	-96	-72	-38	-4	21	32	39	46	52	54	54	56	58	61
64	66	65	63	62	63	67	72	70	60	50	39	34	38	43	46	39	29	19	9
-2	-19	-42	-65	-89	-113	-123	-117	-107	-98	-79	-46	-9	26	38	29	20	12	9	9
9	8	10	20	33	46	54	49	39	32	36	46	56	64	61	50	38	27	16	3
-14	-33	-51	-61	-59	-63	-75	-88	-98	-98	-78	-63	-54	-56	-61	-66	-71	-69	-58	-45
-32	-19	-6	4	7	7	8	8	9	10	10	11	12	12	13	14	14	15	15	8
-4	-17	-31	-35	-21	0	20	41	53	48	37	27	16	9	7	5	4	2	1	0
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82	71	56	40	28	27	27	26	20	8	-4	-16	-17	-6	8	22	36	50	64	78
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IIACIO 55.001.0
STATION NO. C91

SAN JOSE EARTHQUAKE SEPT 4, 1955 - 1801 PST
SAN JOSE BANK OF AMERICA BASEMENT

EPICENTER 37 22 00N, 121 47 00W
COMP N31W 37 20 00N, 121 53 00W

DAMPING = 0.592

ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS

ACLN = -100.2 CM/SEC/SEC AT 1.20 SEC

VELO = 10.8 CM/SEC AT 1.14 SEC

DISP = 2.8 CM AT 2.48 SEC

INITIAL VELO = -1.88356 CM/SEC INITIAL DISP = -0.94296 CM

2479 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

46	95	171	152	84	18	-47	-93	-110	-84	17	157	294	435	532	475	337	201	67	-68
-204	-366	-541	-726	-811	-623	-320	-23	270	574	778	688	454	229	3	-221	-444	-580	-344	-595
-379	-82	209	500	786	964	997	903	665	394	127	9	119	280	437	527	341	-3	-344	-685
-1002	-996	-714	-413	-126	177	358	264	79	-92	-198	-203	-158	-109	-85	-72	-50	22	131	243
325	241	40	-158	-360	-508	-441	-252	-61	99	91	-32	-156	-274	-347	-351	-237	-52	140	286
227	44	-68	-77	-43	31	143	269	337	265	151	81	21	-64	-167	-241	-205	-105	-8	30
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243	280	236	163	97	47	42	82	125	144	143	119	90	71	46	-6	-63	-90	-79	-52
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181	163	129	60	-17	-93	-167	-216	-230	-215	-174	-116	-56	3	31	25	14	5	-4	-13
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[illegible]

IIA011 56.601.0 EL ALAMO, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST EPICENTER 31 45 00N, 115 55 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT COMP S00W 32 47 43N, 115 32 55W
INSTR PERIOD = 0.0661 SEC DAMPING = 0.621 ACCELERUGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACN = 32.4 CM/SEC/SEC AT 10.16 SEC VELO = -4.0 CM/SEC AT 11.88 SEC DISP = -2.4 CM AT 30.90 SEC

INITIAL VELO = 0.45458 CM/SEC INITIAL DISP = 0.16755 CM

4502 INSTRUMENT AND BASELINE CORRECTED DATA IN		MM/SEC/SEC		AT EQUALLY-SPACED INTERVALS OF		0.02		SEC											
7	-20	-18	-23	-26	-24	-20	-17	-12	-1	14	21	19	10	-10	-31	-38	-34	-40	-57
-75	-83	-74	-62	-51	-40	-28	-23	-35	-52	-68	-81	-70	-43	-11	30	77	106	95	69
46	23	32	76	123	123	75	21	-18	-50	-68	-45	-4	36	72	76	57	38	20	2
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-52	-72	-98	-105	-72	-23	24	71	119	161	164	139	119	105	89	59	45	51	52	44
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IIA011 56.001.0 EL ALAMO, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST EPICENTER 31 45 00N, 115 55 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT COMP S90W 32 47 43N, 115 32 55W
INSTR PERIOD = 0.0655 SEC DAMPING = 0.621 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -50.1 CM/SEC/SEC AT 6.80 SEC VELO = -7.7 CM/SEC AT 24.06 SEC DISP = -4.1 CM AT 24.46 SEC

INITIAL VELO = 0.59679 CM/SEC INITIAL DISP = -0.21959 CM

4499 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-15	-41	-72	-95	-95	-84	-74	-47	10	46	56	52	26	3	5	21	33	59	114	181
214	183	132	91	75	75	67	56	45	34	23	20	20	20	20	7	-19	-37	-42	-32
-18	-5	-12	-40	-55	-59	-65	-65	-56	-46	-40	-38	-50	-84	-124	-162	-202	-217	-193	-158
-127	-105	-99	-79	-17	57	109	141	168	144	96	76	64	49	41	47	58	66	54	23
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-201	-204	-158	-107	-59	-12	27	35	25	41	79	116	152	189	226	255	233	181	140	105
71	60	73	88	103	102	65	17	-29	-79	-129	-180	-218	-213	-184	-162	-167	-188	-207	-206
-184	-162	-136	-95	-58	-38	-17	2	25	19	-47	-126	-141	-97	-45	3	50	68	52	33
29	38	46	63	107	149	148	127	109	127	180	238	294	350	359	304	248	220	183	126
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94	78	-2	-77	-133	-189	-246	-275	-248	-209	-152	-55	19	47	79	146	230	303	295	236
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IIA011 56.001.0 EL ALAMO, BAJA CALIFORNIA EARTHQUAKE FEB 9, 1956 - 0633 PST
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIG DISTRICT
INSTR PERIOD = 0.0646 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
EPICENTER 31 45 00N, 115 95 00W
COMP VERT 32 47 43N, 115 32 55W

DP	FAK	VALS	ACLN =	12.4	CM/SEC/SEC AT	9.48	SEC	VELD =	-2.9	CM/SEC AT	44.32	SEC	DISP =	-1.6	CM AT	44.94	SEC
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INITIAL VELO = 0.15046 CM/SEC INITIAL DISP = 0.07629 CM
INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-29	30	21	-16	-50	-48	-27	-7	0	-10	-24	-41	-59	-44	5	36	29	19	27	21
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111A012 56.002.0 EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST
 STATION NO. 117 FL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT
 INSTR PERIOD = 0.0661 SEC DAMPING = 0.621
 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
 EPICENTER 31 45 00N, 115 55 00W
 COMP S00W 32 47 43N, 115 32 55W

PEAK VALS ACIN = -11.8 CM/SEC/SEC AT 1.10 SEC VELO = 1.9 CM/SEC AT 0.92 SEC DISP = 1.7 CM AT 12.46 SEC

INITIAL VFLO = -0.22210 CM/SEC
INITIAL DISP = 0.27305 CM

4406 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

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IIA012 56.002.0 EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST EPICENTER 31 45 00N, 115 55 00W
 STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S90W 32 47 43N, 115 32 55W
 INSTR PERIOD = 0.0655 SEC DAMPING = 0.621 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACIN = -15.4 CM/SEC/SEC AT 0.66 SEC VELO = 2.7 CM/SEC AT 0.50 SEC DISP = -2.3 CM AT 51.28 SEC

INITIAL VELO = -0.39423 CM/SEC INITIAL DISP = -0.18479 CM

4405 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

0	42	62	77	81	77	72	69	69	69	69	70	72	72	72	72	77	83	87	87	83	69
46	30	25	22	16	6	-10	-33	-59	-82	-103	-123	-144	-154	-152	-147	-140	-123	-101	-76	-76	
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130	121	94	58	30	12	-5	-20	-30	-38	-36	-24	-8	5	13	27	50	73	83	81	81	
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[illegible]

IIA012 56.002.0 EL ALAMO, BAJA CALIFORNIA AFTERSHOCK FEB 9, 1956 - 0725 PST EPICENTER 31 45 00N, 115 55 00W
 STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT 32 47 43N, 115 32 55W
 INSTR PERIOD = 0.0646 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTRED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACLN = 3.7 CM/SEC/SEC AT 49.98 SEC VELO = 1.8 CM/SEC AT 53.20 SEC DISP = -2.9 CM AT 49.90 SEC

INITIAL VELO = -0.17322 CM/SEC INITIAL DISP = 0.23750 CM

4406 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

33	-8	1	-1	-10	-19	-19	-16	-13	-9	-6	-5	-7	-6	0	2	-3	-11	-17	-19
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17	12	0	-13	-19	-14	-8	-4	-6	-9	-7	-3	1	5	9	11	6	-3	-11	-11
-1	7	7	1	-5	-10	-12	-11	-10	-8	-8	-10	-12	-11	-9	-8	-10	-13	-11	-5
2	8	12	14	10	5	1	0	1	2	3	4	4	2	-1	-4	-6	-9	-7	-7
-6	-7	-10	-12	-14	-17	-19	-21	-24	-26	-23	-15	-7	-2	-1	-1	-1	-2	-2	-2
-1	1	4	6	9	11	14	14	10	3	-3	-9	-13	-15	-15	-11	-5	-2	-4	-7
-10	-14	-19	-24	-27	-20	-11	-1	3	-2	-10	-16	-21	-24	-21	-15	-10	-5	1	6
8	8	9	9	10	10	9	5	0	-5	-7	-1	5	11	10	6	2	-1	-5	-8
-6	-2	-3	-5	-4	-2	-2	-3	-4	-2	-1	-1	-3	-4	-4	-3	-1	5	13	17
15	11	8	9	11	13	12	7	3	5	8	10	9	8	6	5	5	7	5	-4
-9	-8	-5	-3	-4	-4	-5	-5	-4	-3	-3	-6	-6	-1	6	11	10	9	8	7
7	10	12	7	-2	-8	-6	-1	4	7	6	2	-1	-4	-7	-10	-12	-8	-3	0
-3	-8	-11	-9	-2	4	11	18	19	13	6	-1	-5	-7	-7	-7	-10	-5	-4	-4
-2	3	9	13	9	0	-9	-13	-11	-8	-5	-2	0	-1	-3	-5	-6	-5	-3	-1
0	-2	-4	-3	0	3	5	5	4	3	2	2	3	4	5	4	1	2	7	12
17	18	13	7	0	-6	-8	-6	-3	-1	2	4	2	-2	-5	-9	-9	-7	-3	-1
2	5	7	8	8	9	9	9	9	10	10	11	10	8	5	3	1	0	2	3
2	0	-2	-2	-2	-1	0	2	7	11	12	11	9	6	3	-1	-3	-2	3	7
9	7	3	-1	-5	-9	-12	-14	-13	-7	2	15	15	14	11	8	5	2	1	3
6	9	11	10	4	-3	-9	-10	-8	-8	-11	-15	-19	-22	-19	-14	-9	-7	-8	-7
-6	-5	-3	-2	1	4	5	5	5	5	5	5	5	5	5	5	5	5	5	5
5	5	3	2	3	6	10	13	16	15	10	4	0	-1	0	1	4	8	13	18
22	21	17	14	11	8	5	3	1	-1	-1	2	5	0	5	2	-1	-2	0	2
4	6	8	9	8	5	3	0	-2	-4	-2	2	2	0	-3	-5	-7	-10	-10	-5
0	2	0	-3	-6	-8	-6	-2	3	7	9	7	5	2	0	-3	-3	1	5	9

[illegible]

[illegible]

[illegible]

[illegible]

IIA013 57.002.0
STATION NO. 078

SAN FRANCISCO EARTHQUAKE
SAN FRANCISCO SOUTHERN PACIFIC
BUILDING BASEMENT

MAR 22, 1957 - 1144 PST
ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

EPICENTER 37 40 00N, 122 29 00W
COMP N45E 37 48 00N, 122 24 00W

INSTR PERIOD = 0.0668 SEC DAMPING = 0.592

PEAK VALS

ACLN = -45.9 CM/SEC/SEC AT 1.76 SEC

VELD = -2.9 CM/SEC AT 7.60 SEC

DISP = -1.1 CM AT 26.36 SEC

INITIAL VELO = 0.33423 CM/SEC
INITIAL DISP = -0.28461 CM

1948 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

9	68	78	62	26	-16	-44	-66	-80	-63	-18	9	-27	-91	-86	-30	26	57	66	73
80	83	58	32	7	-22	-54	-70	-55	-24	-24	-67	-106	-155	-198	-158	-73	11	44	26
-3	-10	42	128	135	54	-21	-23	13	48	83	80	31	0	-22	-95	-188	-173	-89	-14
72	161	208	208	158	104	56	-37	-157	-222	-170	-24	133	283	300	174	22	-83	-109	-107
-91	30	154	234	217	45	-167	-363	-459	-441	-314	-150	-14	123	226	195	115	84	126	211
249	165	41	-87	-161	-114	-14	31	-51	-151	-209	-230	-227	-162	-39	36	38	12	13	28
15	29	103	200	251	201	113	29	-46	-76	-54	26	138	246	305	298	216	97	-22	-85
-82	-67	-68	-111	-159	-162	-96	-20	1	-18	-77	-139	-149	-133	-116	-81	-26	33	79	100
103	77	17	-60	-103	-54	40	113	99	32	-32	-94	-138	-154	-147	-120	-72	-18	33	34
-21	-84	-138	-108	-14	85	133	92	26	-27	-24	14	62	115	144	156	158	143	123	107
94	82	69	57	43	20	-13	-45	-63	-71	-78	-87	-86	-67	-43	0	37	49	40	16
-12	-33	-41	-42	-31	-13	1	0	-12	-31	-60	-86	-110	-148	-182	-185	-141	-56	11	50
86	89	48	23	55	108	151	129	60	-4	-42	-67	-83	-74	-56	-36	-23	-27	-39	-50
-61	-66	-51	-28	-10	6	28	54	82	125	148	149	150	152	153	152	136	115	100	86
72	57	43	10	-38	-57	-61	-67	-78	-92	-103	-102	-96	-90	-84	-78	-66	-33	-7	-9
-20	-22	-10	10	16	-4	-32	-58	-83	-100	-111	-113	-110	-107	-104	-94	-76	-54	-27	-1
11	13	13	27	78	127	151	156	146	136	127	113	92	75	67	63	58	56	41	13
0	-5	-8	-1	8	-9	-43	-61	-56	-37	-13	13	24	-5	-52	-92	-111	-118	-118	-109
-101	-97	-96	-97	-93	-76	-49	-32	-37	-51	-60	-64	-66	-75	-52	-76	-51	-31	-16	-8
-3	7	43	98	151	184	206	215	199	179	171	167	164	150	114	85	75	68	62	46
11	-22	-39	-52	-65	-79	-87	-84	-77	-70	-63	-58	-67	-87	-105	-108	-107	-110	-110	-106
-106	-115	-126	-124	-97	-65	-49	-40	-27	-2	27	43	51	58	65	70	75	80	85	90
95	99	96	85	73	67	70	75	80	84	80	73	65	58	40	14	-2	-10	-15	-21
-27	-40	-56	-59	-46	-29	-12	0	1	-2	-3	-6	-7	-15	-38	-61	-73	-79	-83	-87
-90	-94	-98	-101	-95	-75	-52	-30	-10	-3	-3	0	5	10	10	8	10	18	40	63
71	65	46	36	54	83	108	126	131	129	127	130	128	116	87	52	34	31	33	27
7	-17	-34	-33	-23	-20	-38	-65	-84	-92	-90	-86	-85	-92	-97	-95	-91	-87	-83	-79
-70	-42	-4	24	35	33	28	30	56	92	110	104	74	41	24	17	10	3	-3	-5
-2	1	-3	-12	-21	-29	-29	-18	-5	9	12	-2	-21	-40	-58	-59	-45	-28	-13	1
10	12	13	16	23	42	75	110	145	173	179	154	109	74	50	28	6	-17	-39	-55
-65	-79	-104	-131	-141	-133	-124	-115	-107	-103	-100	-96	-88	-64	-36	-20	-10	1	17	37
51	55	52	40	28	21	31	49	55	46	35	33	34	35	42	51	60	69	73	69
64	54	37	22	18	21	22	15	5	-4	-14	-31	-55	-70	-75	-74	-63	-51	-42	-44
-50	-44	-31	-18	-7	-7	-15	-23	-27	-28	-28	-28	-29	-37	-49	-53	-46	-38	-28	-4
17	22	20	15	10	5	7	19	35	48	56	62	68	73	73	68	67	70	66	57
48	39	39	41	34	20	6	-8	-21	-26	-25	-23	-28	-41	-56	-66	-65	-60	-55	-50
-44	-28	-13	-18	-30	-32	-22	-10	0	4	4	5	5	6	8	11	9	2	-2	-4
-6	-8	-11	-16	-22	-17	-5	-8	20	33	46	59	67	61	50	44	39	33	29	27
22	12	5	4	6	7	10	12	5	-4	-3	0	3	6	4	0	-7	-14	-22	-30
-38	-45	-51	-52	-50	-48	-46	-41	-36	-31	-27	-17	2	19	25	27	29	27	20	13

6	-2	-8	-11	-13	-15	-17	-16	-8	-1	-2	-7	-7	-4	-1	2	6	10	15	20
25	28	28	27	28	32	38	43	49	54	60	62	56	48	38	27	15	3	-8	-19
-27	-31	-35	-37	-38	-38	-41	-49	-56	-56	-50	-44	-38	-32	-37	-50	-64	-71	-68	-57
-45	-34	-22	-16	-15	-15	-19	-23	-28	-32	-21	5	26	29	25	24	28	33	38	42
47	52	57	62	67	70	68	63	60	58	57	56	53	47	41	36	32	26	18	9
1	-8	-16	-25	-33	-42	-50	-59	-67	-76	-83	-83	-79	-76	-78	-82	-79	-72	-66	-57
-47	-37	-28	-21	-14	-6	6	20	31	38	44	51	57	63	68	67	63	60	58	54
46	33	23	19	18	14	9	3	0	5	12	19	26	26	21	15	9	3	-1	0
2	4	4	0	-7	-15	-22	-28	-30	-30	-31	-32	-33	-34	-35	-36	-36	-37	-37	-33
-27	-22	-21	-22	-22	-22	-21	-19	-14	-9	-5	-1	2	7	12	17	20	22	24	26
28	32	41	55	64	65	66	66	66	61	52	42	33	25	18	11	4	-2	-9	-15
-20	-24	-30	-37	-43	-43	-41	-38	-37	-40	-47	-52	-52	-47	-44	-42	-40	-39	-35	-26
-16	-4	7	19	29	36	37	33	31	34	38	42	44	40	34	28	22	16	10	4
1	2	5	7	7	3	-4	-11	-14	-14	-12	-9	-5	-2	-1	-1	-4	-10	-15	-21
-25	-24	-24	-23	-22	-21	-20	-19	-17	-15	-14	-12	-10	-7	-4	-1	2	5	7	10
14	18	22	27	31	35	35	31	27	22	18	15	11	8	5	2	-1	-5	-8	-11
-15	-20	-25	-29	-32	-31	-29	-27	-25	-25	-27	-29	-32	-32	-28	-23	-18	-14	-13	-12
-11	-9	-6	-3	0	3	6	9	11	14	18	27	36	37	35	33	30	28	26	23
21	18	16	14	11	9	5	-5	-5	-20	-19	-18	-21	-30	-38	-37	-33	-30	-33	-38
-36	-28	-20	-14	-11	-10	-8	-6	-3	1	5	9	12	16	20	24	25	20	13	10
12	14	11	5	0	-6	-11	-16	-22	-27	-30	-29	-28	-27	-26	-24	-19	-12	-7	-1
2	-2	-6	-4	0	5	10	15	18	20	22	23	17	10	5	4	4	2	-2	-7
-10	-12	-13	-14	-15	-15	-12	-9	-5	-2	1	4	6	6	4	3	3	4	6	4
9	10	12	11	7	1	-5	-10	-10	-4	2	8	11	10	7	5	4	-20	-18	-21
4	4	5	6	8	9	11	8	-2	-4	2	14	33	44	37	30	31	35	35	26
-17	-6	0	1	2	13	23	15	0	-3	4	-11	-11	-11	-11	-8	-1	6	13	20
15	7	4	5	5	6	7	8	7	1	-8	-11	5	-4	-13	-22	-21	-12	-2	6
23	20	16	13	9	5	2	-2	-4	-5	-2	5	27	19	15	15	15	15	16	19
4	-4	-11	-18	-21	-19	-16	-13	-6	3	13	24	27	19	15	15	12	10	7	5
20	13	2	-3	-1	3	5	4	0	-3	-7	-10	-9	1	12	15	12	10	7	5
5	7	9	11	8	0	-4	-5	-20	-47	-65	-60	-28	14	42	53	40	6	-23	-50
-65	-61	-43	-33	-18	106	132	114	58	-11	-67	-68	-42	-3	31	28	26	36	28	-5
-29	-35	-38	-22	-23	-22	-32	-30	-4	12	22	11	-8	-25	-42	-50	-32	-5	18	21
9	-2	-13	-22	-23	-22	-32	-30	-4	27	41	33	22	22	29	28	7	-18	-19	13
44	55	50	43	43	41	25	5	-14	-30	-31	-7	30	36	4	-29	-45	-44	-36	-27
-19	-15	-16	-23	-33	-45	-56	-62	-54	-22	25	50	31	-10	-37	-48	-43	-24	0	24
40	39	16	-13	-24	-8	23	53	64	56	29	1	-1	9	19	26	23	15	8	8
12	15	6	-9	-25	-32	-20	-3	15	21	6	-11	-20	-20	-19	-18	-20	-21	-16	-10
-4	-1	-7	-16	-25	-28	-21	-10	0	8	11	10	10	10	10	9	9	9	9	8
11	17	25	27	23	18	18	23	29	30	19	5	-7	-16	-20	-15	-9	-4	-8	-21
-33	-42	-44	-40	-32	-23	-16	-15	-17	-19	-21	-23	-19	-11	-2	0	-3	-6	-2	7
16	24	28	29	31	30	25	23	23	23	18	-18	3	-2	-6	-9	-16	-16	-16	3
0	-4	-6	-3	2	4	1	-5	-11	-16	-18	-18	-17	-17	-17	-17	-16	-16	-16	-15
-15	-15	-15	-14	-14	-14	-13	-13	-9	1	11	16	12	7	8	8	9	10	10	10
10	10	10	9	9	9	9	9	9	6	0	-7	-13	-15	-13	-12	-14	-17	-18	-16
-14	-12	-10	-8	-6	-4	-2	0	2	4	6	8	8	8	8	10	15	17	14	10
6	2	-1	-1	-1	2	4	5	7	8	8	4	-1	-7	-12	-14	-13	-13	-12	-13
-14	-15	-16	-16	-15	-14	-13	-14	-16	-13	-7	-3	-4	-8	-7	-1	4	10	12	14
15	16	14	10	6	2	-2	-7	-11	-15	-15	-11	-7	-7	-12	-16	-17	-15	-11	-8
-6	-3	0	3	6	9	7	0	-3	3	12	16	14	11	8	6	5	5	5	4

4	-9	5	8	12	16	20	19	16	12	9	6	3	0	-2	-3	-5	-6	-8	-9	-10
-17	-19	-18	-16	-8	-7	-8	-9	-10	-12	-12	-11	-11	-10	-10	-10	-10	-11	-12	-14	-15
28	32	32	26	18	0	8	14	16	16	18	23	29	34	38	35	30	25	20	20	24
-6	-11	-10	-7	-3	2	9	2	0	6	9	4	-2	-9	-11	-8	-3	1	5	8	4
-19	-13	-7	-1	5	11	9	11	13	15	16	-8	-11	-14	-17	-20	-23	-26	-29	-29	-25
20	17	13	12	12	12	12	12	10	8	5	18	20	21	23	27	33	36	34	28	23
-8	-8	-12	-16	-14	-7	-10	-7	-4			3	1	-1	-1	-1	-4	-10	-16	-18	-14

I1A013 57.002.0
 STATION NO. 078
 INSTR PERIOD = 0.0665 SEC DAMPING = 0.592
 SAN FRANCISCO EARTHQUAKE MAP 22, 1957 - 1144 PST
 SAN FRANCISCO SOUTHERN PACIFIC BUILDING BASEMENT
 ACCFLEROGAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
 EPICENTER 37 40 00N, 122 29 00W
 COMP N45W 37 48 00N, 122 24 00W

PEAK VALS ACIN = -44.9 CM/SEC/SEC AT 1.76 SEC VELQ = 5.0 CM/SEC AT 2.76 SEC DISP = 1.4 CM AT 4.10 SEC

1952 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC									
INITIAL VELQ = 0.21878 CM/SEC INITIAL DISP = -0.22902 CM									
12	-15	28	78	104	77	6	-56	-76	-72
94	62	15	-18	-50	-106	-141	-111	-55	-3
24	172	240	139	-20	-162	-150	22	197	253
-34	12	53	113	144	101	60	45	12	32
-159	-35	151	222	83	-111	-297	-428	-449	-400
256	331	223	54	-93	-166	-168	-123	-28	86
74	145	228	222	318	211	89	-25	-148	-206
-352	-384	-373	-347	-272	-165	-60	47	125	88
-90	-6	71	100	95	86	70	52	35	32
371	333	285	252	234	192	129	67	-9	-105
-55	-141	-226	-310	-169	-387	-368	-217	-253	-189
-22	-64	-82	-42	18	77	138	187	200	193
143	145	120	93	47	-23	-98	-166	-199	-209
31	-10	-51	-88	-100	-96	-91	-89	-95	-108
33	25	28	54	86	116	120	97	72	63
-21	-16	-7	0	-5	-17	-29	-41	-51	-60
4	8	12	16	20	24	29	36	45	42
23	33	29	13	8	11	15	22	47	69
-18	-17	-17	-15	-12	-11	-23	-42	-61	-77
-50	-28	6	40	64	72	82	100	118	136
-3	-7	-11	-15	-18	-20	-20	-24	-31	-36
-58	-77	-84	-81	-80	-95	-95	-105	-105	-98
5	26	48	70	92	107	113	117	121	124
-31	-42	-51	-57	-54	-48	-45	-46	-50	-50
-86	-78	-71	-57	-37	-15	3	12	16	21
54	48	47	45	44	43	40	20	-18	-38
-12	-13	-13	-6	10	31	40	24	0	-22
-11	-6	-1	4	6	14	19	24	23	17
19	23	22	19	16	12	13	19	28	31
-15	-19	-22	-11	9	30	52	67	63	50
-46	-44	-36	-27	-19	-11	-10	-18	-27	-32
55	38	20	3	-13	-28	-36	-37	-38	-39
30	20	19	23	27	29	22	11	-1	-12
-59	-60	-59	-54	-48	-42	-36	-30	-24	-17
68	61	55	49	42	34	26	18	11	3
-22	-26	-29	-22	-35	-37	-40	-42	-44	-44
-2	8	16	24	21	15	12	12	12	10
39	34	29	24	20	20	20	20	20	20
-6	-5	-4	-2	-5	-20	-37	-55	-72	-85
-2	14	28	40	52	64	76	88	99	111
-55	-22	-14	-2	-43	55	88	100	110	111
-41	-13	-24	-30	-41	8	14	29	34	29
-13	-14	-24	-30	-41	8	14	29	34	29
-92	-90	-83	-76	-69	87	77	56	56	77
64	75	86	91	86	-7	-1	-19	-28	-19
-10	-8	-3	-1	-3	-17	-43	-28	-28	-43
-17	-20	-20	-19	-17	-36	-21	-6	-6	-21
13	9	8	8	8	-36	-21	-6	-6	-21
-16	-24	-32	-38	-38	14	20	25	25	20
-40	-28	-13	2	-13	32	41	49	57	63
63	57	56	56	56	-58	-65	-72	-72	-65
-58	-57	-57	-57	-57	80	91	86	86	80
-17	-11	-6	-6	-6	5	5	-49	-49	-51
-12	-22	-32	-32	-32	-50	-50	13	13	13
41	37	31	25	25	19	19	8	8	11
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IIA014 57.003.0
STATION NO. 065
INSTR PERIOD = 0.0650 SEC DAMPING = 0.592
SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
SAN FRANCISCO ALEXANDER RLDG BASEMENT
ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
EPICENTER 37 40 00N, 122 29 00W
COMP NO9W 37 47 00N, 122 24 00W

PEAK VALS ACIN = 41.8 CM/SEC/SEC AT 2.68 SEC VELO = 2.9 CM/SEC AT 3.66 SEC DISP = -1.3 CM AT 2.08 SEC

INITIAL VELO = -0.82929 CM/SEC INITIAL DISP = -0.05220 CM

1985 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

13	68	87	85	84	100	105	51	7	-22	-66	-62	-49	-42	-8	12	-14	-10	14	-1
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-113	-112	-110	-100	-72	-42	-44	-88	-136	-159	-150	-82	8	53	80	118	140	116	72	19
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269	312	258	156	55	-27	-4	100	164	111	14	-31	-43	-76	-95	-130	-99	126	376	357
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51	165	196	164	148	151	127	45	-49	-143	-208	-183	-144	-152	-143	-58	68	180	272	320
313	233	88	-28	-76	-112	-152	-185	-221	-208	-108	41	142	133	49	-53	-116	-118	-76	-49
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IIAC16 57.067.0 STATION NO. 080 INSTR PERIOD = 0.0658 SEC DAMPING = 0.592
 SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST
 SAN FRANCISCO STATE BLDG BASEMENT
 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.
 EPICENTER 37 40' 00" N, 122 29' 00" W
 COMP SC9E 37 47' 00" N, 122 25' 00" W

PEAK VALS ACCLN = -83.8 CM/SEC/SEC AT 1.80 SEC VELO = -5.1 CM/SEC AT 1.88 SEC DISP = -1.1 CM AT 3.00 SEC

INITIAL VELO = -1.32605 CM/SEC INITIAL DISP = -0.06478 CM

2039 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

29	127	133	66	61	99	95	-18	-126	-153	-155	-98	48	143	172	137	59	61	128	178
146	64	39	82	137	164	167	108	-47	-142	-159	-177	-232	-298	-217	-36	141	257	318	278
125	-53	-210	-364	-420	-282	-85	83	208	314	316	184	25	-92	-101	-57	-47	-72	-89	20
183	102	-170	-415	-502	-483	-444	-176	154	261	376	375	108	-220	-346	-219	-32	101	92	23
94	266	438	517	463	393	251	-89	-529	-837	-838	-718	-611	-394	-10	415	803	826	525	219
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IIA016 57.007.0 SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST EPICENTER 37 40 00N, 122 29 00W
STATION NO. 080 SAN FRANCISCO STATE BLDG BASEMENT COMP VERT 37 47 00N, 122 25 00W
INST PERIOD = 0.0668 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -43.5 CM/SEC/SEC AT 1.62 SEC VELO = 2.3 CM/SEC AT 1.54 SEC DISP = 0.6 CM AT 17.66 SEC

INITIAL VELO = 0.08234 CM/SEC INITIAL DISP = -0.19076 CM

2033 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-125	83	115	54	-14	32	68	8	-70	-20	97	2	-140	-106	-56	-78	-42	79	114	21
-8	85	73	-78	-78	37	1	-154	-173	-17	109	135	85	-7	-19	42	90	71	8	-57
-11	-13	29	62	99	52	-44	-142	-191	-162	-77	71	164	169	144	38	-95	-83	36	62
-330	-435	-396	-246	-92	-366	-233	-93	-39	122	302	347	353	354	255	158	83	-25	-104	-205
66	126	231	344	271	134	51	31	-144	-211	-174	-162	-158	-21	197	-246	-234	-224	-188	-70
-9	-37	-101	-112	-73	-35	-59	-149	-157	-61	1	-23	8	79	104	312	332	240	0	-66
11	47	95	133	94	10	-67	-126	-164	-189	-229	-194	-54	93	101	128	102	-7	-48	-20
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0	-20	29	33	-6	-29	-38	-42	-40	-33	-16	33	53	16	24	-123	-53	61	122	88
-15	-10	-27	-7	39	88	115	81	54	78	55	-15	-57	-70	-71	-71	-72	-73	-70	-61
-22	40	59	43	26	18	33	61	73	36	-20	-49	-79	-132	-126	-56	6	43	73	96
100	83	42	-2	-9	5	-22	-39	-11	-14	-62	-77	0	17	17	0	-8	0	16	31
46	34	2	-6	7	19	31	28	8	-19	-37	-54	-30	22	52	51	33	12	3	24
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-5	-10	-8	-4	-1	2	5	7	6	4	4	8	16	22	20	12	3	-3	-5	-4
-3	-3	-3	-3	-1	1	4	6	8	11	10	6	1	-2	0	3	5	8	10	13
11	6	0	-6	-12	-13	-8	-1	1	-3	-10	-10	-4	3	10	16	12	1	-5	1
3	-3	-6	-2	3	3	-2	-5	-5	-3	-1	2	7	9	6	1	-1	-2	-4	-4
4	9	5	-1	-7	-10	-7	-4	0	3	6	10	11	7	1	2	9	12	8	2
-1	-4	-1	-1	4	3	-6	-5	4	2	-5	-8	-9	-10	-11	-12	-13	-13	-11	-7
-4	-4	-4	-6	-9	-10	-7	-2	2	5	8	12	12	6	-3	-6	-3	2	8	13
6	-7	-11	-5	-3	-4	-6	-7	-8	-9	-11	-12	-13	-14	-15	-15	-11	-1	4	1
-4	-7	-5	-2	-6	-13	-18	-17	-13	-8	-5	-9	-10	-13	-14	-16	-13	-16	-14	-10
-2	0	-4	-7	-7	-6	-2	2	6	4	-4	-4	-2	-4	-18	-16	-15	-5	-5	3
3	0	-2	-4	-2	-6	10	8	5	2	-1	-2	-8	-3	-3	-4	-5	-5	-5	-5
-4	-3	-2	-1	1	2	2	1	-1	-2	-5	-7	-8	-10	-11	-8	-11	-11	-13	-14
-13	-9	-7	-7	-8	-10	-11	-12	-13	-11	-6	0	5	10	11	8	5	2	-1	-4
-6	-8	-7	-7	-6	-6	-5	-5	-4	-4	-3	-3	-2	-2	-3	4	6	7	8	6
5	5	8	10	9	6	3	0	-3	-3	-3	-2	-2	-1	-1	0	1	1	2	2

IIA017 57.010.0 MAR 22, 1957 - 1144 PST EPICENTER 37 40 00N, 122 29 00W
STATION NO. 049 OAKLAND CITY HALL BASEMENT COMP S64E 37 48 00N, 122 16 00W
INSTR PERIOD = 0.0673 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 23.7 CM/SEC/SEC AT 1.26 SEC VELO = 1.2 CM/SEC AT 1.34 SEC DISP = -1.1 CM AT 8.88 SEC

INITIAL VELO = 0.31404 CM/SEC INITIAL DISP = -0.19916 CM

2005 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

72	-28	18	63	64	32	-4	-31	-56	-61	-10	63	80	48	9	-8	22	37	14	-28
-81	-142	-167	-116	-32	44	60	44	48	50	19	-9	-3	-1	-27	-47	5	83	97	84
113	113	12	-130	-234	-209	-114	-62	-44	-17	17	41	32	6	12	35	10	-47	-79	-92
-37	96	217	237	198	141	62	-6	-37	-44	-66	-92	-97	-113	-160	-152	-52	47	115	175
143	17	-57	-46	2	25	17	22	37	5	-49	-60	-15	69	106	42	-28	-83	-167	-208
-159	-89	-22	34	48	2	-62	-85	-46	17	82	119	86	53	58	75	72	28	-63	-131
-136	-94	-28	28	80	96	38	-23	-37	-41	-59	-51	-27	2	73	147	173	159	140	114
45	-47	-102	-92	-55	-17	1	-25	-40	-23	-7	-12	-22	-38	-19	60	125	127	66	-8
-15	43	68	54	34	-1	-30	-51	-76	-110	-119	-85	-62	-62	-70	-59	-28	-3	20	56
64	27	-4	-3	12	30	60	109	123	61	-3	-53	-103	-148	-135	-83	-44	-10	-6	-31
-33	-13	30	51	22	4	13	17	34	74	105	102	68	35	11	-17	-39	-41	-42	-62
-78	-67	-45	-23	-2	4	1	22	61	95	89	58	32	10	-5	-18	-35	-46	-43	-3
38	12	-34	-59	-82	-90	-60	-31	-18	-16	-29	-39	-23	-6	3	19	38	41	24	-6
-40	-31	0	-3	-17	-13	-1	11	24	16	-6	-24	-28	-1	45	44	7	-19	-19	0
19	12	-17	-34	-22	-4	5	12	31	42	46	55	56	34	18	21	32	44	54	37
2	-32	-43	-37	-33	-43	-58	-56	-48	-52	-53	-45	-44	-56	-44	1	39	40	22	7
9	21	19	2	-5	2	1	-10	-14	-6	-2	-7	-7	3	5	-6	-11	6	35	43
27	7	3	19	37	32	7	-19	-25	-18	-30	-50	-48	-31	-18	-15	-21	-6	42	70
67	57	41	9	-4	22	45	52	51	35	17	13	12	3	-13	-22	-17	-7	-6	-17
-31	-44	-47	-45	-46	-37	-31	-36	-31	-16	-7	1	17	35	52	46	16	-1	9	23
31	30	16	-5	-26	-33	-17	-10	-20	-32	-25	-5	19	29	12	-8	-22	-28	-26	-25
-23	-20	-11	8	46	11	16	20	14	0	-6	1	14	26	39	45	37	22	10	7
7	10	25	46	46	21	-5	-18	-16	-6	4	13	19	20	13	4	-6	-6	13	25
21	12	4	-3	-4	-2	1	4	9	12	12	10	5	-3	1	21	32	28	20	13
4	-5	3	30	37	22	10	6	5	5	3	6	11	2	-16	-32	-39	-32	-17	-3
-1	-5	-11	-22	-37	-36	-22	-13	-14	-15	-17	-18	-17	-1	23	44	46	36	25	14
1	-1	6	-1	-18	-22	-12	5	27	42	35	16	3	-3	-8	-10	-8	-7	0	11
18	19	19	18	13	-22	-1	-13	-25	-37	-50	-57	-50	-38	-28	-28	-34	-28	-7	9
21	30	28	22	16	11	5	3	10	16	13	14	21	29	29	22	12	3	-6	-16
-21	-18	-13	-6	9	26	34	38	38	25	8	-7	-15	-21	-26	-23	-18	-21	-29	-35
-36	-36	-35	-34	-34	-33	-32	-30	-27	-23	-18	-13	-6	4	16	25	26	21	21	21
18	14	12	16	25	32	32	26	20	14	8	2	-1	1	4	6	0	-9	-18	-24
-20	-6	4	2	-3	-1	8	10	6	2	-2	-6	-10	-17	-25	-24	-13	1	14	15
6	-2	-5	2	13	21	17	8	-2	-8	-8	-7	-9	-7	-5	-6	-11	-14	-14	-14
-13	-12	-12	-12	-11	-9	-2	5	12	19	27	30	27	22	18	18	18	19	19	19
21	24	28	32	27	14	1	-9	-16	-19	-19	-17	-16	-19	-23	-28	-29	-28	-26	-25
-25	-30	-36	-42	-41	-28	-14	-2	8	14	18	19	12	8	14	18	11	0	-7	-13
-14	-9	-3	3	8	-15	11	12	14	15	16	18	19	19	13	3	-3	0	6	11
9	3	-4	-10	-15	-15	-12	-10	-7	-5	-3	-1	1	4	7	9	8	4	1	-1
0	2	4	5	4	2	-1	-3	-6	-9	-11	-13	-12	-12	-13	-16	-19	-21	-18	-12

-5	-2	-3	-4	-5	-7	-12	-20	-23	-22	-19	-17	-14	-10	-6	-2	2	5	-14	5	5
5	5	5	5	4	4	4	4	5	8	11	9	4	-1	-6	-9	2	-11	-14	-14	-10
-5	-2	-3	-7	-9	-2	7	16	18	14	11	7	3	0	-4	-6	-7	-8	-9	-9	3
-7	-4	-2	-3	-5	-7	-9	-11	-11	-10	-9	-8	-8	-7	-5	-2	-1	0	0	3	2
4	4	1	-4	-7	-5	0	3	2	1	-13	-2	-3	-3	-2	-2	-7	-4	-1	-1	1
8	18	21	16	7	1	0	2	0	-6	14	15	13	-15	-12	-10	1	5	5	7	2
4	4	6	3	-1	-4	-4	2	8	12	14	15	13	9	4	1	2	-11	-11	-5	2
3	-2	-3	2	9	15	19	16	12	8	3	-1	-5	-8	-9	-10	-11	-14	8	3	3
10	13	4	-5	-8	-10	-13	-13	-11	-7	-3	0	4	7	11	14	17	14	14	8	2
-3	-7	-6	-5	-4	-2	-1	0	1	3	4	5	6	5	3	0	-2	0	0	3	6
9	12	16	19	18	13	8	4	2	2	2	2	2	2	2	2	2	2	2	3	10
17	22	25	26	25	22	16	10	14	2	5	8	8	-11	-1	-5	-8	-7	-4	-4	-2
-1	-2	-4	-5	-6	-2	4	11	14	11	5	0	-6	-11	-16	-21	-22	-22	-21	-21	-21
-19	-12	-4	3	6	6	6	7	7	8	8	9	9	8	7	6	5	3	3	3	4
5	4	-1	-6	-10	-9	-2	6	12	12	8	5	1	0	1	4	6	9	9	9	5
2	-2	-6	-10	-13	-12	-12	-11	-9	-9	-8	-8	-7	-7	-6	-5	-5	-4	-4	-4	-3
-3	-2	0	4	8	12	16	19	17	14	12	9	6	4	2	2	1	0	0	-1	-1
6	4	-4	-4	-5	-6	-7	5	-8	10	-9	-6	-3	1	7	12	13	11	9	9	7
-2	-3	2	0	-2	-2	1	5	8	10	8	7	4	2	1	0	-1	-2	-3	-3	-3
-3	-2	0	1	2	4	5	6	8	9	10	7	0	-4	-6	-7	-8	-4	2	2	9
9	2	-5	-13	-18	-17	-12	-8	-6	-10	-13	-13	-12	-11	-10	-9	-10	-11	-10	-10	-7
-3	1	5	5	1	-2	-2	0	2	4	3	1	-1	-3	-6	-4	3	10	13	13	10
6	2	-5	7	11	16	17	12	6	4	5	6	7	8	10	11	10	8	5	5	3
0	-2	-11	-7	-3	-9	-8	1	-7	-6	-1	-15	-2	-3	-4	-4	-5	-10	-12	-12	-14
-16	-15	-2	-1	-2	6	7	3	-3	-9	-14	-15	-2	-2	5	10	9	-5	-5	-4	-3
-3	-2	16	12	9	8	12	17	18	14	9	3	-2	-3	-2	-1	0	1	7	5	0
11	15	16	12	9	-4	-6	-8	-11	-13	-13	-10	-7	-8	-1	0	-3	-10	-17	-17	-22
-19	-2	-7	-2	-3	-4	-26	-22	-11	-10	-13	-10	12	8	4	0	20	19	10	10	1
-2	-1	1	4	8	2	-8	-6	2	2	-3	-1	10	14	6	-3	-4	4	7	7	5
6	11	14	12	9	7	10	13	4	1	5	2	-5	-5	3	10	7	-2	-9	-9	-9
-4	1	5	6	4	1	0	-1	-1	-2	-2	-2	-2	-3	-6	-12	-12	-2	2	2	-1
-6	-10	-14	-17	-13	-5	-4	10	-15	-14	-5	-10	-5	7	11	18	11	-3	-8	-13	-13
-18	-11	-1	-4	-9	-4	-16	-8	-2	-7	-5	-7	9	14	18	18	11	13	9	9	13
16	19	16	7	-2	-12	-16	-8	-6	-7	-6	-10	-3	-12	-11	-10	-9	-9	-8	-5	-10
-20	-18	-12	-5	0	-1	-2	-4	-6	-7	-9	-10	-12	-12	-11	-10	-9	-9	-8	-7	-7
-4	6	19	27	23	18	13	8	5	4	4	3	2	1	2	2	2	3	1	1	-5
-12	-15	-14	-11	-9	-7	-1	3	-2	-8	-13	-20	-23	-16	-4	6	5	-2	-9	-9	-9
4	6	-2	-2	7	14	18	18	14	9	4	3	8	-5	-4	-5	3	11	19	19	18
9	6	9	6	1	-5	-8	-11	-8	0	9	15	13	7	0	-5	-5	1	5	5	3
0	-3	-6	-10	-12	-9	-5	0	5	8	7	3	-1	-5	-9	-9	-5	0	4	4	8
12	16	17	11	2	-9	-13	-8	2	8	6	3	0	-3	-6	-8	-5	4	11	11	10
5	1	-4	-6	-3	3	7	5	1	-3	-6	-10	-12	-10	-6	-3	-5	-8	-6	-6	-1
5	10	15	17	13	7	2	0	-1	-2	3	12	13	7	0	-6	-7	-5	-4	-4	-2
-1	1	1	-1	-3	-4	-1	4	10	11	9	7	5	2	0	-2	-4	-7	-9	-9	-11
-13	-10	-6	-2	1	2	-17	-16	-15	-14	-14	-13	-12	-11	-9	-8	-6	-5	-4	-3	-2
1	-4	-9	-14	-18	-18	-3	-4	-4	-3	-1	-1	-2	-4	-3	-2	-6	-5	-3	-3	-2
0	1	3	4	3	-1	-4	-3	-1	1	3	5	7	9	7	-8	-6	-5	-3	-3	-2
13	10	8	6	3	1	0	5	12	14	14	13	12	12	11	10	8	6	3	3	1
-2	-5	-7	-10	-12	-9	-1	4	1	-3	-5	-7	-8	-10	-11	-13	-13	-10	-7	-7	-5

-3	7	0	1	2	3	4	6	8	11	13	11	8	4	3	4	5	6	7	8
7	-3	3	0	0	-5	-7	-4	-2	4	5	4	3	2	1	3	4	0	-2	-2
0	5	-5	-5	-6	-2	-3	1	4	2	4	5	4	3	3	3	2	-1	1	0
-2	-4	-1	-2	-5	-2	-2	-3	-6	-7	-9	-9	-4	-5	-6	-6	-3	1	2	2
2	2	2	2	-1	2	2	1	2	3	5	4	1	-1	-4	-7	3	0	0	1
-3	-4	-6	-5	-1	-5	-3	9	-2	3	5	6	7	-2	-2	-8	-8	1	-6	-5
11	10	8	7	6	4	4	2	1	3	2	3	1	7	8	9	9	10	11	11
-3	-3	-3	-3	-3	5	-3	-3	-3	-3	-2	-3	-3	-3	-3	-3	-3	-4	-3	-3
-7	-7	-6	-4	-2	-3	-3	3	11	9	8	6	11	12	13	12	10	8	6	4
2	0	-2	-2	-3	-2	0	5	6	6	8	3	8	4	3	4	5	6	7	8

IIA017 57.010.0 SAN FRANCISCO EARTHQUAKE MAR 22, 1957 - 1144 PST EPICENTER 37 40 00N, 122 29 00W
 STATION NO. 049 OAKLAND CITY HALL BASEMENT COMP VERT 37 48 00N, 122 16 00W
 INSTR PERIOD = 0.0668 SEC DAMPING = 0.607 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 15.3 CM/SEC/SEC AT 0.34 SEC VELO = 0.9 CM/SEC AT 22.38 SEC DISP = -1.3 CM AT 19.94 SEC

1998 INSTRUMENT AND BASELINE CORRECTED DATA IN										AT EQUALLY-SPACED INTERVALS OF 0.02 SEC									
INITIAL VELO = 0.11568 CM/SEC										INITIAL DISP = 0.19543 CM									
3	-56	-24	38	50	24	-12	-52	-39	36	48	-36	-66	-4	47	29	103	153	-40	-136
-24	11	-71	-68	2	38	44	37	51	74	71	14	-53	-91	-89	-30	-29	-39	31	83
24	-50	-10	59	-5	-109	-51	-1	-25	-22	5	25	27	4	-17	15	-19	-85	-13	62
-1	1	111	80	-24	-27	-16	-30	-18	22	32	-1	-15	1	-23	-58	-28	-27	-74	-74
-17	11	-15	-39	-12	73	133	46	-85	-20	58	-27	-47	34	96	116	96	-10	-93	-91
-75	-62	-32	5	18	-11	-28	-12	7	25	1	-51	-36	27	66	95	118	108	63	23
-48	-110	-73	11	71	49	-23	-38	-7	-22	-81	-75	-9	4	17	54	20	26	71	59
59	86	34	-36	-40	-9	15	23	22	18	38	38	2	-38	-62	-69	-73	-73	-27	16
16	8	-12	-56	-39	-20	-55	-19	66	76	39	47	54	28	18	-9	-34	-3	9	-11
-2	-6	-35	-38	-16	2	0	-27	-61	-51	-9	25	23	9	44	70	35	-23	-44	-15
3	13	18	-2	-3	17	19	-21	-34	-26	-33	-36	20	46	-6	-43	-48	-46	-26	3
11	4	-5	-2	8	12	22	35	19	-14	-1	27	17	-17	-5	26	12	-10	4	8
-29	-62	-70	-60	-29	-7	-9	2	5	-2	14	37	52	36	4	-9	-3	2	-10	-19
-1	10	-6	-17	-12	-20	-23	3	18	-6	-6	32	49	14	-11	19	38	3	-24	-28
-30	-8	6	-12	-5	2	-8	3	11	0	5	35	46	33	14	-11	-20	7	12	-6
-6	7	11	-2	-8	1	10	3	11	39	25	-21	-24	6	6	-24	0	13	7	10
18	-4	-18	1	13	13	13	15	26	23	4	-19	-29	-21	-10	-24	-47	-34	-2	9
10	28	28	-21	-40	-5	17	17	13	8	11	26	30	19	17	13	-3	-19	-25	-34
-45	-36	-24	-39	-46	-37	-34	-34	-15	8	19	38	52	51	48	44	41	40	47	47
34	20	9	0	9	17	-5	-30	-35	-31	-46	-54	-43	-37	-34	-15	-17	-28	7	39
27	25	31	30	39	52	44	17	-1	9	19	11	13	20	10	-8	-20	-26	-26	-20
-13	-4	3	-1	-1	8	-2	-21	-18	-5	4	7	-5	-17	-9	1	-8	-24	-20	-4
13	22	13	-1	-12	-21	-10	17	26	13	11	20	18	25	44	40	39	52	36	0
-7	1	0	-3	-6	-9	-5	4	10	7	-3	-13	-23	-19	-3	8	-1	-20	-21	-11
-7	-9	-10	-9	-6	-2	1	5	8	4	-7	-14	-10	2	15	18	11	2	-4	0
12	21	18	9	7	12	19	16	3	-9	-16	-20	-20	-11	-2	-3	-8	-3	12	11
-3	-5	4	8	10	12	9	-1	-9	-11	-14	-13	-6	-1	-4	-7	-8	-8	-6	-1
2	1	-1	-2	-3	-2	-1	-5	-13	-20	-21	-18	-16	-20	-20	-12	-5	1	6	9
7	5	9	16	22	22	17	11	7	4	3	2	0	-6	-13	-19	-20	-15	-11	-6
0	6	2	-1	12	27	22	7	-1	-2	-4	-6	-8	-10	-9	-3	-4	-12	-18	-21
-19	-10	-3	-8	-15	-14	-8	-1	4	8	7	0	-4	0	1	-6	-14	-15	-13	-8
-1	2	4	7	10	15	23	34	40	37	32	27	15	2	6	15	9	-6	-19	-29
-38	-40	-33	-25	-18	-19	-26	-25	-14	-3	-3	-11	-12	-3	6	12	12	6	3	4
4	-1	-6	-8	-4	-1	-4	-10	-13	-7	1	0	-7	-7	-3	1	8	22	23	13
5	3	3	5	12	18	12	-2	-9	-8	-9	-15	-21	-26	-21	-11	-2	-1	-1	1
5	8	9	9	8	8	8	4	-5	-12	-10	-6	-4	-2	-3	-10	-15	-11	-8	-7
-1	4	4	3	-1	-5	-4	2	9	12	6	1	3	7	8	6	4	3	1	-1
-3	-7	-12	-14	-12	-10	-9	-11	-13	-11	-6	-6	-13	-15	-9	-2	-3	-6	-6	-1
4	5	2	-1	0	8	7	-4	-6	-2	1	3	-1	-4	-7	-9	-9	-9	-10	-10
-10	-8	-6	-4	-2	-4	-3	2	4	0	-5	2	11	7	-3	-7	1	7	5	1

[illegible]

-8	-1	-7	-2	0	-1	-3	-5	-2	-4	-7	-8	-7	-8	-7	-10	-7	-6	-10	-6	-5	-4	-3	-2	-4	-4	-7	-7	-7	-6	-7	-5	-4	-3	-2	-1	0	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30	-31	-32	-33	-34	-35	-36	-37	-38	-39	-40	-41	-42	-43	-44	-45	-46	-47	-48	-49	-50	-51	-52	-53	-54	-55	-56	-57	-58	-59	-60	-61	-62	-63	-64	-65	-66	-67	-68	-69	-70	-71	-72	-73	-74	-75	-76	-77	-78	-79	-80	-81	-82	-83	-84	-85	-86	-87	-88	-89	-90	-91	-92	-93	-94	-95	-96	-97	-98	-99	-100	-101	-102	-103	-104	-105	-106	-107	-108	-109	-110	-111	-112	-113	-114	-115	-116	-117	-118	-119	-120	-121	-122	-123	-124	-125	-126	-127	-128	-129	-130	-131	-132	-133	-134	-135	-136	-137	-138	-139	-140	-141	-142	-143	-144	-145	-146	-147	-148	-149	-150	-151	-152	-153	-154	-155	-156	-157	-158	-159	-160	-161	-162	-163	-164	-165	-166	-167	-168	-169	-170	-171	-172	-173	-174	-175	-176	-177	-178	-179	-180	-181	-182	-183	-184	-185	-186	-187	-188	-189	-190	-191	-192	-193	-194	-195	-196	-197	-198	-199	-200	-201	-202	-203	-204	-205	-206	-207	-208	-209	-210	-211	-212	-213	-214	-215	-216	-217	-218	-219	-220	-221	-222	-223	-224	-225	-226	-227	-228	-229	-230	-231	-232	-233	-234	-235	-236	-237	-238	-239	-240	-241	-242	-243	-244	-245	-246	-247	-248	-249	-250	-251	-252	-253	-254	-255	-256	-257	-258	-259	-260	-261	-262	-263	-264	-265	-266	-267	-268	-269	-270	-271	-272	-273	-274	-275	-276	-277	-278	-279	-280	-281	-282	-283	-284	-285	-286	-287	-288	-289	-290	-291	-292	-293	-294	-295	-296	-297	-298	-299	-300	-301	-302	-303	-304	-305	-306	-307	-308	-309	-310	-311	-312	-313	-314	-315	-316	-317	-318	-319	-320	-321	-322	-323	-324	-325	-326	-327	-328	-329	-330	-331	-332	-333	-334	-335	-336	-337	-338	-339	-340	-341	-342	-343	-344	-345	-346	-347	-348	-349	-350	-351	-352	-353	-354	-355	-356	-357	-358	-359	-360	-361	-362	-363	-364	-365	-366	-367	-368	-369	-370	-371	-372	-373	-374	-375	-376	-377	-378	-379	-380	-381	-382	-383	-384	-385	-386	-387	-388	-389	-390	-391	-392	-393	-394	-395	-396	-397	-398	-399	-400	-401	-402	-403	-404	-405	-406	-407	-408	-409	-410	-411	-412	-413	-414	-415	-416	-417	-418	-419	-420	-421	-422	-423	-424	-425	-426	-427	-428	-429	-430	-431	-432	-433	-434	-435	-436	-437	-438	-439	-440	-441	-442	-443	-444	-445	-446	-447	-448	-449	-450	-451	-452	-453	-454	-455	-456	-457	-458	-459	-460	-461	-462	-463	-464	-465	-466	-467	-468	-469	-470	-471	-472	-473	-474	-475	-476	-477	-478	-479	-480	-481	-482	-483	-484	-485	-486	-487	-488	-489	-490	-491	-492	-493	-494	-495	-496	-497	-498	-499	-500	-501	-502	-503	-504	-505	-506	-507	-508	-509	-510	-511	-512	-513	-514	-515	-516	-517	-518	-519	-520	-521	-522	-523	-524	-525	-526	-527	-528	-529	-530	-531	-532	-533	-534	-535	-536	-537	-538	-539	-540	-541	-542	-543	-544	-545	-546	-547	-548	-549	-550	-551	-552	-553	-554	-555	-556	-557	-558	-559	-560	-561	-562	-563	-564	-565	-566	-567	-568	-569	-570	-571	-572	-573	-574	-575	-576	-577	-578	-579	-580	-581	-582	-583	-584	-585	-586	-587	-588	-589	-590	-591	-592	-593	-594	-595	-596	-597	-598	-599	-600	-601	-602	-603	-604	-605	-606	-607	-608	-609	-610	-611	-612	-613	-614	-615	-616	-617	-618	-619	-620	-621	-622	-623	-624	-625	-626	-627	-628	-629	-630	-631	-632	-633	-634	-635	-636	-637	-638	-639	-640	-641	-642	-643	-644	-645	-646	-647	-648	-649	-650	-651	-652	-653	-654	-655	-656	-657	-658	-659	-660	-661	-662	-663	-664	-665	-666	-667	-668	-669	-670	-671	-672	-673	-674	-675	-676	-677	-678	-679	-680	-681	-682	-683	-684	-685	-686	-687	-688	-689	-690	-691	-692	-693	-694	-695	-696	-697	-698	-699	-700	-701	-702	-703	-704	-705	-706	-707	-708	-709	-710	-711	-712	-713	-714	-715	-716	-717	-718	-719	-720	-721	-722	-723	-724	-725	-726	-727	-728	-729	-730	-731	-732	-733	-734	-735	-736	-737	-738	-739	-740	-741	-742	-743	-744	-745	-746	-747	-748	-749	-750	-751	-752	-753	-754	-755	-756	-757	-758	-759	-760	-761	-762	-763	-764	-765	-766	-767	-768	-769	-770	-771	-772	-773	-774	-775	-776	-777	-778	-779	-780	-781	-782	-783	-784	-785	-786	-787	-788	-789	-790	-791	-792	-793	-794	-795	-796	-797	-798	-799	-800	-801	-802	-803	-804	-805	-806	-807	-808	-809	-810	-811	-812	-813	-814	-815	-816	-817	-818	-819	-820	-821	-822	-823	-824	-825	-826	-827	-828	-829	-830	-831	-832	-833	-834	-835	-836	-837	-838	-839	-840	-841	-842	-843	-844	-845	-846	-847	-848	-849	-850	-851	-852	-853	-854	-855	-856	-857	-858	-859	-860	-861	-862	-863	-864	-865	-866	-867	-868	-869	-870	-871	-872	-873	-874	-875	-876	-877	-878	-879	-880	-881	-882	-883	-884	-885	-886	-887	-888	-889	-890	-891	-892	-893	-894	-895	-896	-897	-898	-899	-900	-901	-902	-903	-904	-905	-906	-907	-908	-909	-910	-911	-912	-913	-914	-915	-916	-917	-918	-919	-920	-921	-922	-923	-924	-925	-926	-927	-928	-929	-930	-931	-932	-933	-934	-935	-936	-937	-938	-939	-940	-941	-942	-943	-944	-945	-946	-947	-948	-949	-950	-951	-952	-953	-954	-955	-956	-957	-958	-959	-960	-961	-962	-963	-964	-965	-966	-967	-968	-969	-970	-971	-972	-973	-974	-975	-976	-977	-978	-979	-980	-981	-982	-983	-984	-985	-986	-987	-988	-989	-990	-991	-992	-993	-994	-995	-996	-997	-998	-999	-1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IIA018 61.001.0 HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST EPICENTER 36 40 00N, 121 18 00W
 STATION NO. 028 HOLLISTER CITY HALL COMP S01W 36 51 00N, 121 24 00W
 INSTR PERIOD = 0.0660 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -63.4 CM/SEC/SEC AT 1.04 SEC VELO = -7.8 CM/SEC AT 9.44 SEC DISP = -2.8 CM AT 9.70 SEC

INITIAL VELO = 1.11791 CM/SEC INITIAL DISP = 0.27354 CM

2024 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-273	160	85	12	-63	-99	-77	-48	-61	-106	-135	-80	29	134	240	274	186	65	-40	-58
-9	34	-10	-111	-203	-254	-179	-36	101	144	90	23	-10	2	25	46	65	81	97	114
135	211	293	193	-23	-210	-353	-385	-350	-310	-323	-450	-634	-622	-447	-253	-45	119	219	199
137	208	338	473	483	273	-14	-129	-50	64	184	203	99	-26	-146	-264	-313	-285	-241	-201
-149	-81	-45	-39	-21	30	81	85	60	60	151	319	482	556	518	411	141	-325	-586	-531
-377	-259	-172	-90	-20	47	98	80	16	11	75	174	247	128	-61	-179	-159	-39	99	250
335	364	350	278	218	189	144	60	-121	-357	-475	-448	-369	-228	-31	71	88	109	148	194
181	114	32	-60	-83	-44	-2	18	-16	-72	-120	-94	-12	81	138	126	122	149	130	58
-40	-136	-185	-188	-160	-103	-26	45	106	170	176	84	-32	-139	-220	-257	-248	-207	-147	-42
57	124	184	238	285	324	322	271	171	37	-74	-131	-155	-158	-137	-107	-75	-43	-11	13
34	28	-3	-60	-142	-200	-232	-265	-297	-321	-296	-225	-133	-27	87	206	274	254	215	196
184	174	161	129	76	65	110	165	228	286	248	142	33	-54	-87	-98	-110	-123	-135	-164
-218	-284	-361	-453	-491	-416	-307	-202	-106	-56	-30	-7	33	114	212	282	325	364	404	443
481	470	403	327	257	190	127	57	-47	-239	-396	-444	-453	-412	-344	-256	-132	-8	109	226
348	444	522	573	526	419	313	188	75	24	-3	-34	-107	-219	-337	-438	-450	-399	-346	-297
-254	-216	-166	-102	-13	128	255	331	339	270	184	105	39	-18	-51	-70	-84	-124	-216	-347
-455	-523	-533	-465	-379	-264	-96	72	210	329	407	465	484	413	306	178	39	-84	-165	-200
-227	-245	-224	-183	-141	-91	-32	24	79	107	54	-44	-142	-233	-243	-179	-111	-43	39	135
217	271	317	363	365	311	246	183	119	54	-13	-79	-156	-244	-337	-405	-394	-340	-286	-232
-182	-150	-128	-109	-70	16	118	214	270	291	308	311	294	273	253	221	168	110	52	-13
-86	-162	-222	-253	-275	-276	-249	-220	-183	-110	-11	73	136	189	223	242	263	274	262	243
224	203	170	130	71	-30	-127	-203	-263	-295	-320	-347	-380	-385	-330	-256	-185	-113	-38	38
104	146	156	148	142	153	181	209	239	248	219	178	139	100	57	3	-58	-120	-176	-219
-259	-298	-341	-389	-438	-480	-468	-414	-359	-305	-212	-74	47	149	236	298	342	369	383	383
368	349	332	314	297	281	265	249	232	218	209	207	194	160	119	80	42	5	-23	-37
-49	-57	-52	-41	-30	-19	-8	6	21	34	32	17	2	-13	-30	-51	-74	-99	-127	-156
-169	-163	-151	-141	-138	-139	-140	-127	-96	-63	-34	-25	-31	-37	-43	-49	-55	-61	-66	-73
-73	-62	-47	-33	-19	-4	17	48	81	114	170	239	279	302	326	354	392	417	397	355
315	261	173	75	-22	-116	-203	-262	-298	-332	-361	-385	-407	-430	-442	-429	-408	-387	-367	-341
-302	-259	-217	-169	-101	-26	83	246	347	389	434	478	514	524	485	422	355	281	189	86
-5	-83	-147	-189	-225	-262	-294	-318	-336	-338	-322	-306	-289	-266	-217	-165	-97	-11	7	-95
55	277	185	64	26	-3	-26	-39	-49	-47	-33	-7	7	51	99	147	194	202	236	267
293	218	245	294	229	155	103	59	14	-26	-69	-100	-120	-135	-148	-139	-117	-94	-72	-49
-29	-11	6	23	40	57	64	59	51	44	-37	30	18	-1	-22	-44	-62	-74	-84	-93
-96	-87	-76	-65	-53	-41	-28	-15	-5	-7	-17	-29	-40	-50	-61	-62	-52	-38	-26	-13
0	15	34	54	74	77	61	41	21	2	-18	-38	-56	-72	-87	-103	-118	-133	-145	-158
-170	-182	-191	-199	-201	-186	-159	-133	-107	-81	-44	4	52	97	141	185	231	256	240	212
186	159	133	106	76	44	14	-18	-38	-36	-28	-20	-13	-5	-3	-9	-17	-25	-34	-42
-50	-58	-66	-67	-61	-54	-47	-40	-34	-25	-12	5	22	33	34	33	31	30	29	27
29	34	41	48	55	62	68	72	71	70	70	69	68	67	66	63	61	58	55	53

50	47	48	52	57	62	67	71	77	83	90	96	103	106	99	87	76	65	54	42
-191	-172	-153	-134	-115	-96	-77	-58	-42	-33	-27	-20	-7	12	-190	-198	-207	-215	-220	-210
167	191	216	231	224	210	196	183	168	141	105	69	33	4	14	29	45	-60	-81	-105
-131	-155	-178	-201	-223	-245	-251	-234	-211	-190	-168	-146	-124	-101	-79	-56	-33	-14	1	15
29	44	60	77	94	112	129	146	164	181	198	203	193	180	167	155	142	130	117	101
82	63	45	19	-13	-48	-76	-94	-110	-126	-143	-158	-161	-153	-143	-134	-124	-115	-104	-85
-59	-32	-6	20	46	71	91	105	114	122	131	138	137	126	113	101	88	76	58	27
-8	-36	-55	-71	-88	-105	-121	-133	-134	-131	-128	-125	-122	-119	-112	-104	-96	-87	-79	-70
-54	-33	-11	11	33	54	75	95	116	136	156	175	190	205	219	216	199	181	163	145
127	109	91	72	48	21	-5	-31	-54	-66	-72	-77	-82	-88	-92	-89	-84	-79	-74	-73
-75	-78	-81	-84	-86	-78	-92	-95	-96	-92	-87	-83	-78	-74	-69	-62	-49	-34	-19	-4
11	26	40	53	66	79	92	105	115	113	103	92	81	70	59	48	37	25	14	5
5	10	16	22	27	33	38	40	41	43	44	45	45	43	38	34	30	26	21	12
0	-11	-22	-33	-44	-55	-65	-74	-82	-90	-87	-71	-54	-37	-19	-3	9	19	29	39
50	56	53	47	41	35	29	23	17	11	5	-1	-6	-8	-8	-7	-7	-6	-9	-17
-28	-38	-48	-59	-69	-79	-90	-95	-89	-79	-70	-60	-51	-41	-32	-23	-16	-10	-4	3
9	15	19	22	26	29	33	36	39	38	35	33	30	27	25	22	20	17	14	12
9	7	5	2	0	-3	-5	-8	-12	-16	-15	-9	-2	4	11	17	24	30	33	29
24	19	14	9	3	-2	-7	-12	-17	-22	-27	-29	-26	-22	-18	-14	-10	-6	-3	1
5	7	9	12	14	16	18	20	23	25	26	21	13	6	-2	-10	-17	-25	-33	-41
-51	-62	-73	-84	-95	-106	-117	-128	-130	-122	-112	-102	-91	-81	-71	-61	-51	-40	-30	-19
-5	9	23	37	52	66	80	92	101	109	118	126	134	143	150	149	140	132	124	115
107	99	91	82	71	57	43	28	14	-1	-17	-34	-50	-67	-84	-99	-100	-90	-80	-69
-59	-49	-39	-29	-21	-16	-10	-5	1	6	12	18	22	20	12	4	-4	-12	-20	-28
-34	-40	-46	-52	-58	-61	-60	-57	-54	-51	-48	-45	-36	-11	18	46	72	86	93	100
100	87	71	55	39	25	14	4	-6	-16	-24	-26	-26	-26	-26	-25	-25	-25	-25	-25
-25	-24	-23	-18	-12	-7	-1	5	11	17	23	28	34	40	46	48	42	32	22	13
3	-6	-17	-33	-52	-70	-89	-104	-112	-118	-123	-129	-134	-130	-120	-110	-100	-90	-80	-69
-50	-27	-4	16	35	53	72	90	101	106	111	116	122	127	132	136	133	126	120	113
106	99	92	81	69	57	44	33	26	23	21	18	16	14	11	9	5	-2	-10	-17
-25	-32	-40	-45	-49	-54	-58	-62	-66	-71	-75	-79	-80	-78	-74	-70	-66	-62	-59	-55
-51	-47	-43	-37	-31	-25	-19	-14	-8	-4	-4	-6	-6	-7	-8	-9	-10	-11	-12	-12
-10	-6	-3	1	4	8	11	15	18	22	25	28	32	35	38	41	44	47	50	49
45	41	38	34	30	27	23	19	16	12	9	9	12	14	17	19	22	24	27	29
31	33	36	35	32	29	26	22	19	16	12	9	8	8	10	11	12	13	15	16
17	18	20	18	12	5	-3	-10	-18	-25	-32	-40	-47	-54	-62	-69	-76	-84	-86	-82
-78	-74	-70	-66	-63	-59	-55	-49	-43	-36	-30	-23	-17	-11	-5	0	5	9	14	18
23	27	29	30	31	32	34	38	43	52	59	66	72	79	86	92	98	96	84	72
60	48	36	21	5	-12	-28	-42	-56	-64	-68	-71	-74	-78	-80	-82	-84	-82	-74	-63
-49	-36	-27	-21	-14	-7	-1	6	13	18	21	23	25	27	29	31	31	29	27	24
22	19	17	14	12	9	7	4	2	0	-3	-5	-7	-10	-12	-14	-17	-21	-25	-28
-32	-31	-29	-27	-25	-23	-20	-18	-16	-14	-12	-9	-5	-2	1	5	8	11	15	18
21	24	24	22	21	19	17	16	14	12	10	9	7	7	8	10	12	14	15	17
16	13	11	8	5	2	-1	-4	-6	-9	-10	-12	-14	-16	-18	-19	-22	-25	-28	-32
-35	-39	-42	-46	-49	-48	-42	-35	-28	-21	-15	-8	-1	6	13	19	23	27	30	34
38	42	46	50	53	50	44	38	32	26	20	13	7	1	-5	-11	-17	-23	-29	-36
-42	-48	-54	-60	-62	-56	-49	-43	-36	-29	-22	-15	-9	-2	6	13	20	28	35	43
50	58	65	67	63	58	53	48	43	38	33	28	22	17	12	7	2	-4	-10	-17
-23	-29	-35	-41	-47	-53	-59	-65	-71	-78	-81	-76	-66	-55	-45	-35	-25	-15	-5	6

16	26	34	35	33	31	30	28	27	25	23	22	20	19	17	15	14	12	11	10
-12	-9	-6	-3	0	3	6	10	12	11	9	7	5	3	1	-1	-1	-1	-1	-1
-2	-5	-2	1																
-10	-6	-3	0	4	7	10	14	17	19	17	14	10	7	4	0	-3	-6	-10	-13
-16	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	-15
-19	-22	-25	-28	-31	-34	-37	-40	-42	-42	-39	-36	-33	-30	-27	-24	-21	-19	-16	-16
8	10	11	12	12	11	9	8	6	4	2	1	-1	-3	-5	-6	-8	-10	-13	-16
15	13	12	10	8	6	4	3	1	-1	-2	-2	-1	0	2	3	4	5	6	7
15	-10	-15	-20	-25	-30	-32	-28	-22	-16	-10	-3	3	9	15	21	22	21	19	17
36	39	42	45	48	51	50	47	43	40	36	32	28	25	21	17	14	9	4	-1
-16	-20	-25	-26	-23	-19	-15	-11	-7	-3	2	6	10	14	18	21	24	27	30	33
-10	11	11	11	12	12	12	12	13	13	13	13	14	13	10	6	1	-3	-7	-12
16	10	11	11	12	12	12	12	13	13	13	13	14	13	10	6	1	-3	-7	-12

IIA018 61.001.0 HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST EPICENTER 36 40 00N, 121 18 00W
 STATION NO. 028 CITY HALL COMP N89W 36 51 00N, 121 24 00W
 INSTR PERIOD = 0.0659 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACIN = -175.7 CM/SEC/SEC AT 1.20 SEC VELU = 17.1 CM/SEC AT 1.12 SEC DISP = 3.8 CM AT 1.26 SEC

INITIAL VELO = -1.5271 CM/SEC INITIAL DISP = -0.82583 CM
 2025 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

-28	66	87	107	128	148	169	189	210	230	256	297	327	300	241	153	-32	-274	-398	-426
-445	-408	-307	-191	-57	87	252	403	410	321	231	141	58	42	83	126	151	73	-83	-288
-444	-538	-563	-445	-271	-73	214	639	942	1095	1127	1116	1048	991	891	778	370	-423	-1131	-1634
-1757	-1621	-1467	-1224	-939	-630	-348	-150	121	510	806	1023	1001	572	120	-705	-962	-931	-695	-411
-116	180	356	305	135	-51	-241	-459	-548	-625	-540	-360	-154	108	361	518	517	413	310	226
161	130	129	140	149	178	233	385	552	638	547	298	7	-273	-477	-547	-558	-531	-487	-421
-299	-162	-18	115	177	184	236	284	407	569	726	692	506	314	159	83	59	19	-26	-46
-78	-145	-246	-371	-453	-523	-519	-472	-395	-320	-216	-56	100	185	201	180	141	86	26	-5
5	27	47	74	115	183	235	296	294	181	94	31	-22	-24	-4	37	77	56	-2	-79
-157	-193	-222	-283	-346	-368	-370	-348	-287	-165	-65	31	90	122	128	106	77	38	-1	0
26	49	68	110	184	258	317	348	370	379	323	222	77	-88	-204	-289	-372	-408	-391	-364
-331	-292	-262	-269	-300	-326	-346	-359	-359	-341	-305	-252	-152	-23	111	252	449	665	806	884
98	164	197	216	212	213	64	-80	-259	-294	-341	-371	-400	-442	-460	-412	-339	-267	-184	-35
15	57	113	190	265	321	325	285	242	197	100	-53	-199	-285	-327	-192	-170	-110	-53	-18
19	141	226	285	345	415	479	524	553	543	510	466	383	300	252	218	199	192	184	160
119	72	19	-38	-104	-174	-222	-252	-280	-305	-327	-353	-388	-425	-432	-394	-348	-298	-239	-172
-127	-129	-145	-142	-119	-93	-65	-31	-2	3	-4	-3	7	19	24	0	-28	-63	-80	-92
-83	-61	-39	-15	54	159	252	331	399	435	455	440	382	292	164	62	-19	-102	-169	-214
-242	-262	-273	-264	-245	-225	-167	-70	25	106	160	185	183	160	116	40	-41	-95	-123	-122
-102	-81	-60	-38	-13	11	26	34	42	48	52	54	56	59	54	20	-28	-89	-139	-165
-163	-108	-36	52	147	214	265	306	330	341	350	357	354	337	323	288	234	102	-73	-155
-192	-225	-252	-277	-264	-221	-166	-96	-37	4	16	-19	-66	-123	-193	-232	-244	-255	-266	-278
-296	-320	-345	-369	-394	-417	-440	-457	-483	-406	-369	-330	-270	-189	-103	-36	5	28	45	57
49	27	5	-16	-28	-12	15	65	152	237	317	393	460	518	568	615	632	615	590	535
450	340	203	83	-20	-93	-115	-122	-130	-138	-152	-200	-268	-331	-373	-390	-377	-344	-310	-261
-188	-126	-89	-55	-22	19	76	135	179	204	219	211	185	157	117	64	19	-14	-41	-61
-79	-85	-74	-59	-44	-30	-13	12	32	36	35	48	77	109	139	167	189	207	224	225
206	177	130	81	50	27	5	-12	-14	-6	2	11	18	20	18	10	0	-10	-20	-35
-56	-73	-82	-88	-94	-100	-99	-89	-76	-65	-46	-8	37	82	119	141	158	176	193	211
228	246	249	230	205	180	140	86	38	1	-33	-52	-48	-39	-30	-22	-13	-3	11	27
42	58	70	53	14	-25	-64	-105	-174	-264	-323	-362	-399	-409	-398	-387	-377	-355	-304	-239
-174	-101	-25	53	128	179	208	235	266	302	341	376	369	327	285	236	169	97	28	-27
-74	-120	-167	-214	-263	-303	-324	-318	-295	-270	-246	-221	-194	-165	-137	-108	-78	-44	-9	26
60	93	124	156	178	187	191	196	193	183	173	162	152	141	130	112	92	72	52	32
10	-30	-82	-134	-172	-193	-210	-228	-246	-264	-277	-282	-286	-291	-291	-275	-251	-227	-204	-174
-124	-65	-20	11	40	68	79	80	81	81	79	81	94	110	125	141	156	173	192	211
230	250	268	265	247	226	200	170	141	91	23	-23	-49	-75	-98	-115	-130	-145	-162	-184
-206	-216	-217	-205	-181	-155	-129	-95	-53	-11	28	58	82	107	131	155	173	184	195	206
218	229	245	266	287	290	266	236	207	177	148	117	83	49	15	-13	-36	-59	-81	-104

[illegible]

IIA018 61.001.0 HOLLISTER EARTHQUAKE APR 8, 1961 - 2323 PST EPICENTER 36 43 00N, 121 18 00W
 STATION NO. 028 HOLLISTER CITY HALL COMP VERT 36 51 00N, 121 24 00W
 INSTR PERIOD = 0.0671 SEC DAMPING = 0.592 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 49.1 CM/SEC/SEC AT 1.28 SEC VELO = 4.7 CM/SEC AT 9.32 SEC DISP = 2.2 CM AT 10.00 SEC

INITIAL VELO = 1.20054 CM/SEC INITIAL DISP = 0.32095 CM

2032 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

15	-14	-14	-14	-15	-14	-15	-15	-15	-15	-29	-66	-107	-149	-186	-164	-86	-9	-3	-70
-90	-21	67	143	230	-15	-29	-88	-105	-105	-145	-148	-94	-22	41	57	66	100	58	-48
-159	-196	-140	-56	61	160	108	-19	-93	-117	-123	-138	-171	-209	-220	-184	-143	-125	-122	-82
13	126	248	396	491	436	310	196	154	169	207	180	31	-145	-272	-257	-152	-56	19	89
134	161	165	102	-30	-191	-272	-253	-231	-218	-170	-106	-24	85	167	212	273	274	179	45
-11	7	46	56	-14	-76	-86	-84	-96	-135	-168	-143	-80	-28	11	36	44	49	55	89
126	60	-72	-100	-40	30	100	134	133	99	45	-9	-53	-69	-125	-249	-262	-169	-72	19
81	116	121	96	67	50	24	-25	-47	-23	24	89	82	15	-18	-31	-31	-18	-8	-21
-49	-51	-14	31	74	81	46	3	-46	-111	-143	-128	-105	-87	-76	-51	16	91	127	141
127	90	65	54	35	3	-31	-24	16	47	68	89	133	195	217	158	19	-115	-183	-180
-140	-98	-69	-56	-46	-38	-40	-48	-56	-71	-82	-83	-79	-77	-66	-45	-14	38	93	91
42	40	86	139	172	150	104	78	76	79	76	59	31	14	22	40	59	94	111	62
-16	-85	-148	-209	-266	-262	-208	-150	-93	-25	29	54	73	91	138	110	77	33	-15	-35
-14	16	19	-5	-34	-41	-19	10	39	57	27	-14	-76	-33	-31	-15	-37	-72	-98	-77
-28	24	75	128	154	131	95	61	26	0	-8	-9	-15	-33	-57	-72	-81	-90	-79	-51
-20	11	38	45	38	39	33	71	81	64	45	56	76	96	93	33	-33	-81	-102	-90
-72	-80	-106	-115	-98	-77	-55	-42	-49	-60	-36	12	61	108	135	148	161	174	188	199
185	139	92	25	-74	-131	-163	-197	-198	-167	-132	-100	-96	-119	-146	-160	-133	-83	-32	8
7	-11	-10	4	17	30	42	39	20	1	-19	-40	-62	-82	-97	-94	-76	-57	-38	-18
9	38	68	85	73	52	32	7	-34	-82	-127	-137	-118	-97	-80	-76	-77	-78	-80	-76
-47	-4	38	79	116	137	144	147	146	143	141	138	139	146	156	166	177	174	140	98
59	44	55	69	82	84	76	68	59	46	30	15	-5	-35	-43	-33	-23	-12	-8	-18
-33	-47	-59	-69	-75	-58	-27	3	33	61	89	116	145	151	125	91	70	77	96	108
103	86	70	57	60	53	16	-29	-57	-70	-82	-95	-114	-137	-152	-157	-161	-155	-137	-116
-94	-72	-50	-27	-3	21	46	69	95	97	57	6	-45	-85	-98	-100	-102	-106	-131	-170
-209	-245	-241	-205	-168	-131	-94	-56	-19	12	43	59	36	-6	-48	-78	-81	-73	-67	-60
-53	-43	-29	-14	1	16	32	47	62	78	84	78	69	60	51	42	34	27	23	18
13	14	20	26	32	37	44	56	71	85	97	108	118	122	122	121	121	108	78	44
16	-4	-24	-43	-57	-67	-78	-87	-87	-80	-72	-65	-57	-49	-41	-33	-24	-15	-5	4
17	32	48	64	80	93	104	115	126	136	132	111	88	66	43	18	-17	-54	-92	-128
-147	-149	-149	-149	-149	-151	-153	-154	-147	-134	-119	-106	-86	-58	-28	-3	13	23	33	33
28	22	20	25	37	48	60	71	79	23	18	118	156	79	36	123	178	120	144	102
109	78	52	57	28	12	-14	-79	-85	-93	-127	-155	-173	-181	-172	-156	-140	-121	-100	-78
-66	-78	-59	20	51	36	22	25	48	74	101	119	125	121	105	81	57	17	-32	-71
-100	-129	-151	-163	-174	-180	-163	-131	-99	-66	-32	2	36	70	101	131	161	191	217	238
246	232	211	192	176	162	148	135	115	86	54	23	-8	-38	-67	-91	-111	-121	-116	-107
-99	-89	-76	-60	-44	-28	-15	-4	6	17	28	40	52	61	69	76	84	88	78	59
40	22	0	-28	-48	-48	-41	-35	-30	-24	-25	-34	-45	-55	-63	-69	-75	-81	-81	-75
-69	-62	-55	-48	-32	-10	12	43	82	108	120	131	134	121	104	88	73	59	47	34
22	7	-10	-27	-44	-62	-79	-98	-114	-126	-135	-145	-152	-157	-162	-168	-170	-165	-157	-150

-140	-118	-87	-55	-21	10	29	42	56	70	84	101	117	134	140	133	122	113	103	94
83	72	61	51	27	5	1	0	-2	-3	-5	-10	-18	-26	-34	-42	-47	-51	-54	-52
-46	-39	-32	-23	-11	3	17	25	27	28	31	37	43	49	51	51	50	50	49	49
47	39	28	16	4	-4	-9	-14	-19	-24	-28	-31	-35	-38	-41	-45	-50	-55	-60	-65
-72	-81	-90	-98	-106	-139	-122	-93	-84	-74	-60	-42	-23	-2	21	41	58	75	85	92
99	106	108	106	102	98	95	92	93	88	86	85	83	80	77	74	68	50	28	5
-10	-15	-18	-21	-24	-27	-30	-35	-40	-45	-50	-55	-59	-62	-66	-67	-63	-57	-51	-46
-40	-34	-27	-21	-14	-8	-9	-14	-19	-25	-26	-23	-19	-15	-12	-17	-28	-40	-50	-51
-39	-25	-12	1	16	33	52	71	86	98	109	111	104	95	87	78	73	70	68	65
63	60	52	41	31	20	11	1	-7	-7	-1	7	14	20	27	33	40	42	39	34
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29	33	38	41	46	50	55	60	69	62	55	47	38	28	18	9	1	16	20	24

I1A019 68.005.0 BORRERO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST EPICENTER 33 09 00N, 116 08 00W
STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP S90W 32 47 43N, 115 32 55W
INSTR PERIOD = 0.0670 SEC DAMPING = 0.570 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.07C AND 25 CYC/SEC.

PEAK VALS ACCLN = -56.3 CM/SEC/SEC AT 15.00 SEC VELO = -14.7 CM/SEC AT 28.86 SEC DISP = -11.0 CM AT 20.54 SEC

INITIAL VELO = 1.21809 CM/SEC INITIAL DISP = -0.72730 CM

4361 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

18	38	48	42	31	21	12	9	12	2	-3	3	14	27	12	-48	-75	-45	-12	10	30	47
30	-9	-19	-7	5	17	9	11	35	-17	-19	0	12	6	-6	-17	-21	17	-15	-14	-19	-26
-32	-36	-37	-32	-23	-8	11	41	41	35	34	-24	-63	-46	-22	-7	13	17	-16	-39	-31	-8
13	30	42	48	10	-38	-42	-30	-31	-41	-41	-48	-52	-46	-22	5	17	15	10	6	2	-5
-27	-33	-8	17	36	33	-5	-44	-54	-48	-54	-59	-40	-31	3	22	-10	-17	12	45	54	16
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-102	-52	-28	-79	-136	-156	-98	-51	-28	-14	-22	-64	-80	-74	-80	-74	-66	-89	-80	17	79	82
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[illegible]

IIAC19 68,005.0 BORREGO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST EPICENTER 33 09 01N, 116 08 00W
 STATION NO. 117 EL CENTRO SITE IMPERIAL VALLEY IRRIGATION DISTRICT COMP VERT 32 47 43N, 115 32 55W
 INSTR PERIOD = 0.0670 SEC DAMPING = 0.503 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -29.7 CM/SEC/SEC AT 7.56 SEC VELO = 3.4 CM/SEC AT 71.20 SEC DISP = -3.9 CM AT 70.50 SEC

4357 INSTRUMENT AND BASELINE CORRECTED DATA IN										AT EQUALLY-SPACED INTERVALS OF									
INITIAL VELO = 0.81829 CM/SEC										INITIAL DISP = -0.05023 CM									
MM/SEC/SEC										CM									
4357 INSTRUMENT AND BASELINE CORRECTED DATA IN										AT EQUALLY-SPACED INTERVALS OF									
INITIAL VELO = 0.81829 CM/SEC										INITIAL DISP = -0.05023 CM									
MM/SEC/SEC										CM									
4357 INSTRUMENT AND BASELINE CORRECTED DATA IN										AT EQUALLY-SPACED INTERVALS OF									
INITIAL VELO = 0.81829 CM/SEC										INITIAL DISP = -0.05023 CM									
MM/SEC/SEC										CM									
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11A220 68.007.0 BORRERO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST EPICENTER 33 09 00N, 116 08 00W
STATION NO. 277 SAN DIEGO LIGHT AND POWER BLDG COMP SCLM 32 42 25N, 117 09 18W
INSTR PERIOD = 0.080 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = 29.5 CM/SEC/SEC AT 8.54 SEC VELO = 6.0 CM/SEC AT 10.32 SEC DISP = -4.4 CM AT 8.64 SEC

3960 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC																			
INITIAL VELO = 0.06509 CM/SEC										INITIAL DISP = -0.17554 CM									
-2	-16	-22	-27	-14	4	3	-2	-9	-16	-15	-5	6	18	23	14	4	-3	-9	-15
-15	-8	-11	-17	-26	-30	-21	-9	-4	-4	-5	-5	1	12	23	37	47	55	49	39
28	19	11	5	-7	-24	-40	-40	-26	-12	5	13	8	0	-2	12	30	43	42	41
37	35	30	24	15	13	20	28	14	-7	-28	-31	-25	-17	-20	-28	-36	-46	-46	-29
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9	11	7	3	-1	5	10	4	-5	-7	-2	0	-3	-7	-10	-4	1	-4	-11	-20
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13	23	19	9	-3	-15	-26	-17	2	12	2	-12	-22	-25	-27	-23	-11	-11	-26	-44
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IIAC20 68.007.0 BORRERO MOUNTAIN EARTHQUAKE APR 8, 1968 - 1830 PST EPICENTER 33 09 00N, 116 08 00W
STATION NO. 277 SAN DIEGO LIGHT AND POWER BLDG COMP VERT 32 42 25N, 117 09 18W
INSTR PERIOD = 0.081 SEC DAMPING = 0.574 ACCELEROGRAM IS BAND-PASS FILTERED BETWEEN 0.070 AND 25 CYC/SEC.

PEAK VALS ACCLN = -12.7 CM/SEC/SEC AT 10.90 SEC VELO = -1.9 CM/SEC AT 16.06 SEC DISP = 1.3 CM AT 36.20 SEC

INITIAL VELO = 0.10610 CM/SEC INITIAL DISP = -0.00179 CM

3963 INSTRUMENT AND BASELINE CORRECTED DATA IN MM/SEC/SEC AT EQUALLY-SPACED INTERVALS OF 0.02 SEC

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